The Effect of Forming Speed on Cold Roll Forming of the Rocket Frame

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Abstract. Aiming at the forming speed of sheet metal, this paper discusses the influence of technological parameters on the quality of the rocket frame. Using 3D software SolidWorks to establish the geometric model of the plate and the upper and lower rolls required in the cold roll forming process, and introduced it into the finite element analysis software ANSYS/LS-DYNA to analyze the change of stress and strain of the plate during the forming process. By comparing the stress-strain nephograms of sheet metal at different forming speeds, it can be seen that with the increasing of forming speed, the maximum Mises stress of the sheet is gradually increasing, and the maximum strain of the sheet is gradually decreasing.

Introduction

During the cold roll forming process, the selection of process parameters plays a crucial role in the molding quality of the final product [1,2]. The deformation and stress of the sheet during the cold roll forming process are very complicated and belong to the nonlinear deformation process [3,4]. At present, many domestic enterprises are relying on experience in the cold roll forming processes. Before actual production, a large number of experiments are often performed, which will generate a large amount of waste products, increase production costs, and waste resources. Aiming at this phenomenon, this paper uses the LS-DYNA analysis module of the finite element analysis software ANSYS to investigate the influence of process parameters on the quality of the frame of the rocket frame by taking the forming speed, forming angle and thickness of the sheet as examples.

The Rocket Frame and Roll Parameters

In this paper, the simulation analysis of the cold roll forming process of the rocket frame is carried out. Figure 1 is a specification of the rocket frame.

Figure 1. Parameters of the rocket frame

The material of the rocket frame is 7A09, which is a hard aluminum alloy with a tensile strength of 490 MPa, a yield strength of 370 MPa [5], and the roll material is Cr12MoV. Table 1 and table 2 are their specific parameters.
Table 1. Material parameters of rocket frame

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<tbody>
<tr>
<td>2700</td>
<td>7e10</td>
<td>0.3</td>
<td>3.7e8</td>
<td>1.714e9</td>
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Table 2. Material parameters of upper and lower rolls

<table>
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<tr>
<th>Density [kg/m³]</th>
<th>Elastic Modulus [Pa]</th>
<th>Poisson Ratio</th>
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<tr>
<td>7850</td>
<td>2.06e11</td>
<td>0.28</td>
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After analysis, six molding passes were finally selected to complete the molding of the model. The forming angles of the six passes are 10°, 25°, 45°, 65°, 80°, 90°.

Simulation Analysis Pre-processing

Model Establishment and Meshing

This article uses SolidWorks to create 3D model drawings of the plate, the upper rolls and lower rolls, then save the files into x-t format and import them into the LS-DYNA module. SOLID164 solid unit was used in the plate, upper rolls and lower rolls during forming process, which contains 8 nodes, supports the simultaneous application of multiple types of loads, provides a variety of unit algorithms, and accelerates unit calculations by integrating and viscous hourglass control. It is suitable for handling most nonlinear problems. Since the plate, the upper rolls and lower rolls are not very complicated, the sweeping method is used to mesh models. Taking the first pass as an example, the size of the plate unit is controlled to 5mm×5mm×2mm, and the number of units obtained after the division is completed is 5760. For the upper and lower rolls, the unit size is controlled to 5mm×5mm×1mm, and the division is completed. After getting the upper roller, there are 8692 grid units, and the lower roller has 7791 grid units. Their meshing is shown in the figure 2.

![Figure 2. Mesh division of plate, upper roll and lower roll](image)

Contact and Restraint Loads

The upper surface of the plate is in contact with the outer surface of the upper roll, and the lower surface of the plate is in contact with the outer surface of the lower roll. Therefore, the contact type belongs to surface to surface contact. The cold roll forming design manual shows that the static friction coefficient of the plate and the upper and lower rolls is 0.61. The dynamic friction coefficient is 0.47.

For the plate, according to its force characteristics during the cold roll forming process, it is only necessary to limit the movement constraint in the X direction of the plate to prevent lateral slippage during the simulation process. For the upper and lower rolls, it is necessary to limit the movement constraints in the X, Y, and Z directions and the rotation constraints in the Y and Z directions, and release the rotation constraint in the X direction. After several simulations and simulations, the forming speed of the plate was finally selected to be 1 m/s, and the upper and lower rolls were rotated at the corresponding initial speed.
Simulation Results Analysis

In this paper, taking the first pass as an example, in the case of ensuring that other parameters are unchanged, the forming speed of the plates is set to 1m/s, 1.5m/s, 2m/s, 2.5m/s and 3m/s. Simulation analysis shows that the stress at each speed is shown in figure 3 to figure 7.

![Stress nephogram of 1 m/s at velocity](image)

![Stress nephogram of 1.5 m/s at velocity](image)

![Stress nephogram of 2 m/s at velocity](image)

![Stress nephogram of 2.5 m/s at velocity](image)

![Stress nephogram of 3 m/s at velocity](image)

It can be seen from figure 3 to figure 7 that the maximum Mises stress value of the sheet is 371.9 MPa at a speed of 1 m/s, the maximum Mises stress value of the sheet is 374.7 MPa a speed of 1.5 m/s, the maximum Mises stress value of the sheet is 375.8 MPa at a speed of 2/s, the maximum Mises stress value of the sheet is 377.7 MPa when the speed is 2.5 m/s, and the maximum Mises stress value...
of the sheet is 378.5 MPa when the speed is 3 m/s. It is concluded that as the forming speed increases during the cold forming process, the maximum Mises stress on the sheet is also increased, and the increased amplitude is not fixed, the increasing slope is different.

Figure 8. Strain nephogram of 1 m/s at velocity
Figure 9. Strain nephogram of 1.5 m/s at velocity
Figure 10. Strain nephogram of 2 m/s at velocity
Figure 11. Strain nephogram of 2.5 m/s at velocity
Figure 12. Strain nephogram of 3 m/s at velocity

Figure 5.6 to figure 5.10 show the strain of the plates at different speeds. It can be seen from Figure 8 to Figure 12 that the maximum strain value of the sheet is 1.074e-2 at a speed of 1 m/s, the maximum strain value of the sheet is 1.058e-2 at a speed of 1.5 m/s, the maximum strain value of the plate is 9.905e-3 when the speed is 2m/s, the maximum strain value of the plate is 9.892e-3 when the speed is 2.5m/s, and the maximum strain value of the plate is 9.634e-3 when the speed is 3m/s. It is
concluded that as the forming speed increases during the cold forming process, the maximum plasticity of the sheet gradually decreases.

![Graph showing Maximum stress and strain at various forming speeds]

Figure 13. Maximum stress and strain at various forming speeds

The maximum stress and the maximum strain at various forming speeds is as shown in figure 13. After analysis, it can be seen from figure 13 that the forming speed of the sheet has a great influence on the forming result. With the increasing of forming speed, the maximum Mises stress of the sheet is gradually increasing, while the maximum strain tends to decrease gradually.

**Summary**

In this paper, the influence of process parameters on the quality of cold-formed products was discussed by changing the forming speed. Through the simulation analysis of different forming speeds, it is found that with the gradual increasing of forming speed, the maximum Mises stress of the sheet is gradually increasing, and the maximum plasticity of the sheet is gradually decreasing. This is the effect of forming speed accelerating sheet metal can not recrystallize in time.

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**References**


