

Numerical simulation of stress relieving and analysis of influencing factors on geostress measurement

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Abstract

At present, over coring method by using hollow inclusion strain cells are applied widely for geostress measurement. But there are some errors in measurement accuracy. In order to improve the measurement precision and reliability of stress relief method, the paper analyzed the influence of drilling aperture ratio on stress. Studies shows that drill holes will cause the loss of displacement and change the aperture ratio of the drilling will cause variation of losing displacement and correction coefficient K_1 . The equation of losing displacement and drilling ratio is $\beta = 0.5546r^{(-1.856)} + 0.06$. Finally, using simulated conclusions analyzed geostress measurement data of Datai mine and verified the validity and feasibility of the formula, It can provides reference for field measurement precision.

Keywords: Stress relief Method; Drilling aperture ratio; geostress measurement; Numerical simulation

1. Introduction

Geostress is the natural stress deposited in the rock strata of the earth's crust and is the important influencing factor for the rock mass deformation and failure in mine, water conservancy, hydropower, civil construction and other kinds of projects. In addition, it use to determine rock mechanics parameters ,analyze rock mass stress and design supporting^[1-2] .In engineering, generally through on-site measurements to get the size and direction of geostress^[3]. At present, stress relief method is widely used to measure

geostress .The method is simple, adaptable. It can determine the three-dimensional stress state of the measuring point. But stress relief method still exist errors in the measurement accuracy, many scholars studied the factors affecting the precision of the measurement^[4-7]. But the strain gauge position and drilling aperture ratio's impact on measurement accuracy is not perfect. In this paper will research the numerical simulation method for stress relief process and analyze the impact of different aperture ratio, then will analyze stress measurement results of Datai mine with the conclusion.

2. The principle of geostress measurement by hollow inclusion strain cells

The method of hollow inclusion strain cells is widely used among stress relief methods, which is shown in Fig.1. This kind of strain gauge is recommended by ISRM, and is designed for monitoring during the core stress release process. Its principle is that in rock mass's(having a 3-D ground stress) drilling hole wall of adhesive elastic circle layer, assuming the rock mass is linear elastic. When the surrounding rock is cut by overcoming, geostress is calculated by using elastic recovery^[8], as shown in Fig.2.



Fig.1 Hollow Inclusion Strain Cells

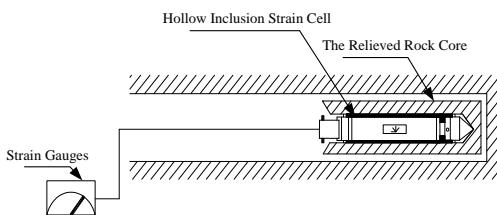


Fig.2 Stress Relief Process of Hollow Inclusion Strain Cell

The hollow inclusion stresses relieve strain gauges measured during the stress-strain data to calculate the formula are:

$$\begin{aligned}\varepsilon_\theta &= \frac{1}{E} \{ (\sigma_x + \sigma_y) k_1 + 2(1 - \nu^2) [(\sigma_y - \sigma_x) \cos 2\theta \\ &\quad - 2\tau_{xy} \sin 2\theta] k_2 - \nu \sigma_z k_4 \} \quad (1)\end{aligned}$$

$$\varepsilon_z = \frac{1}{E} [\sigma_z - \nu(\sigma_x + \sigma_y)] \quad (2)$$

$$\gamma_{\theta z} = \frac{4}{E} (1 + \nu) (\tau_{yz} \cos \theta - \tau_{zx} \sin \theta) k_3 \quad (3)$$

Where, $\varepsilon_\theta, \varepsilon_z, \gamma_{\theta z}$ is respectively the hollow inclusion strain gauge measured hoop strain, axial strain and shear strain value; $K1 \sim K4$ are the correction coefficient. Equations for the calculation of K are:

$$k_1 = d_1 (1 - \nu_1 \nu_2) [1 - 2\nu_1 + \frac{R_1^2}{\rho^2}] + \nu_1 \nu_2;$$

$$k_2 = (1 - \nu_1) d_2 \rho^2 + d_3 + \nu_1 \frac{d_4}{\rho_2} + \frac{d_5}{\rho^4};$$

$$k_3 = d_6 (1 + \frac{R_1^2}{\rho^2});$$

$$k_4 = (\nu_2 - \nu_1) d_1 (1 - 2\nu_1 + \frac{R_1^2}{\rho^2}) \nu_2 + \frac{\nu_1}{\nu_2};$$

$$\text{Where } d_1 = \frac{1}{1 - 2\nu_1 + m^2 + n(1 - m^2)};$$

$$d_2 = \frac{12(1 - n)m^2(1 - m^2)}{R_2^2 D};$$

$$d_3 = \frac{1}{D} [m^4(4m^2 - 3)(1 - n) + x_1 + n];$$

$$d_4 = \frac{-4R_1^2}{D} [m^6(1 - n) + x_1 + n];$$

$$d_5 = \frac{3R_1^4}{D} [m^4(1 - n) + x_1 + n];$$

$$d_6 = \frac{1}{1 + m^2 + n(1 - m^2)};$$

$$n = G_1/G_2; \quad m = R_1/R_2;$$

$$\begin{aligned}D &= (1 + x_2 n)[x_1 + n + (1 - n) \\ &\quad (3m^2 - 6m^4 + 4m^6)] + (x_1 - x_2 n)m^2 \\ &\quad [(1 - n)m^6 + (x_1 + n)]\end{aligned}$$

$$x_1 = 3 - 4\nu_1; \quad x_2 = 3 - 4\nu_2.$$

Where R_1 is the hollow package radius in the body; R_2 is the installation of the pore radius; G_1 is the hollow inclusion material shear modulus of epoxy resin; G_2 is the shear modulus of the rock; ν_1 is the hollow inclusion material Poisson's ratio of epoxy resin; ν_2 is the Poisson's ratio of the rock and ρ is the resistance strain gauge in the hollow inclusion of radial distance. This method can be operated easily and adapt to poor integrity rock mass, and has a high success ratio. But there are still errors on the accuracy. Studies show that the precision of ground stress measurement is influenced not only by the drilling sites, rock mechanics properties, drillings speed, temperature, but also by the structure of strain gauge itself. Strain gauge are built-in epoxy resin layer, its feeling of the strain of drilling rock will go through the epoxy resin layer. Thus, the accuracy depends on the radius of drilling hole, strain gauge radius, the radius of the strain gauge's built-in parts and the elastic constants of surrounding rock and epoxy resin layer, namely the correction coefficients in the formula $K_i (i=1 \sim 4)$. Reference [9] pointed out that the error of stress component, which is main caused by the value K_1 , and radius of drilling hole R has a comprehensive effect on K_1 , but it did not explain the influence degree of drilling hole radius to K_1 and the final results. In order to definite the influence degree, improving the accuracy and the reliability of stress

relief method, this paper will research the process of stress relief by numerical simulation method.

3 The research on hollow inclusion stress relief process with numerical simulation

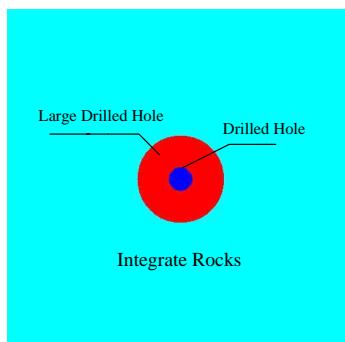
3.1 Establishment of numerical model

Utilizing the calculation software of FLAC3D to simulate and discuss the influence degree of the drilling aperture ratio on the measuring accuracy. The size of the model is $53.2cm \times 300cm \times 53.2cm$, the rock formation is linear elastic, homogeneous and isotropic, and the needing mechanical parameters are shown in table 1.

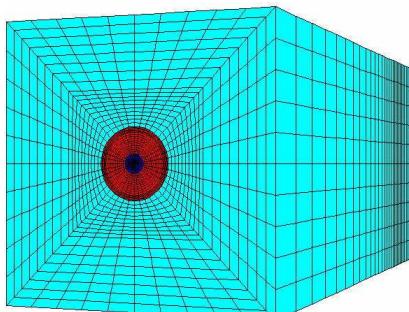
Table 1 Mechanical Parameters

Mechanical Parameters	Rock	Epoxy resin layer
E/GPa	22.350	3
μ	0.27	0.36

The bottom, left and right of the model is fixed, the drilling side is free surface, and applying 25MPa pressure on the top(Fig.3 is the model). The parameters remain unchanged, except the radius of holes.



(a) Sectional View of The Model



(b) Model of Computing Grid

Fig.3 Three - dimensional Calculation Model for Stress Relief

3.2 The process of stress relief simulation

According to the field measurements, the simulation process is divided into five steps, including: 1) Drilling the large hole, its radius is 133mm and the depth is 130cm; 2) Drilling the small hole, the depth is 40cm and its radius is changed under different circumstances; 3) Setting the hollow inclusion strain cells, the reference [6] shows that the ring compress of CSIRO cells' resin layer, supporting the hole wall, should be considered, the shell structure is used to simulate the resistance of resin layer; 4) Stress relief, the stress is relieved along the direction of the large hole, calculating balance every 2cm, and recording the displacement of the measuring point until it has not obvious change. Along the depth of the small hole, measuring points for monitoring displacement is arranged every 5cm, points' arrangements are shown in Fig.4.

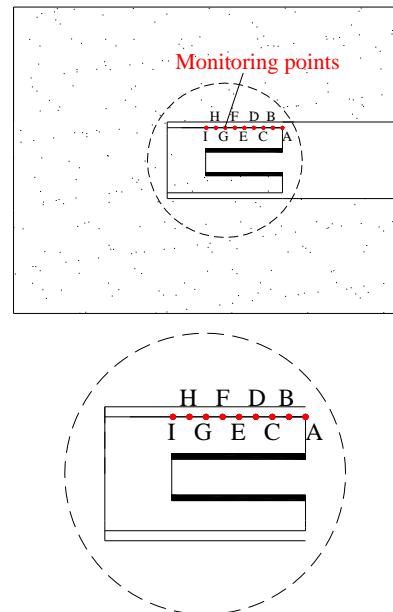


Fig.4 Layout of Monitoring Points

3.3 Measuring points' simulation results

In the second step of the simulation to change the radius of the hole, respectively took 0mm (that is, no drill holes), 10mm, 12mm, 14mm, 16mm, 18mm, 20mm, 22mm, 24mm, 26mm. Fig.5 is the 9 point circumferential displacement curve when the radius is 26mm, the trends of circumferential displacement are similar when radius changed, they are not listed subject to the length.

Using α presents the ratio between the distance from the hole and the hole radius ratio. Analyzed the data, the detail is shown in table 2 and Fig.6. It can be seen that the trend of displacement measuring point is hardly affected by the drilling radius; on the whole, the measured displacements near the hole are changed

largely. With increasing depth of the measuring point, the displacement difference gradually reduced small and stabilizes. In actual measurement, strain gauges should make the work area in the stable area of displacement as much as possible and ensure data more accurate.

Table 2 The Ratio of The Distance Measuring Point With The Holes' Radius

Distance form the hole/cm	0	5	10	15	20	25	30	35	40
α	0	0.125	0.25	0.375	0.5	0.625	0.75	0.875	1
Measuring displacement $/ \times 10^{-2} \text{ mm}$	10.4	7.63	5.14	4.4	3.83	3.65	3.61	3.66	4.29

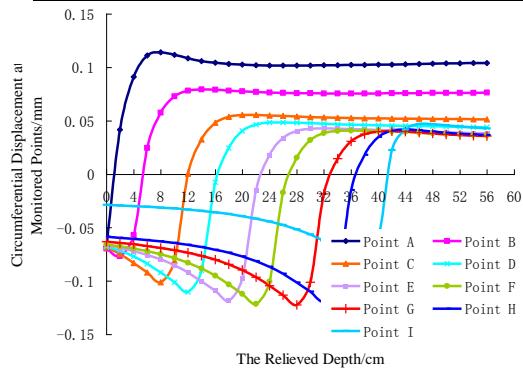


Fig.5 Measuring Displacement of Different point

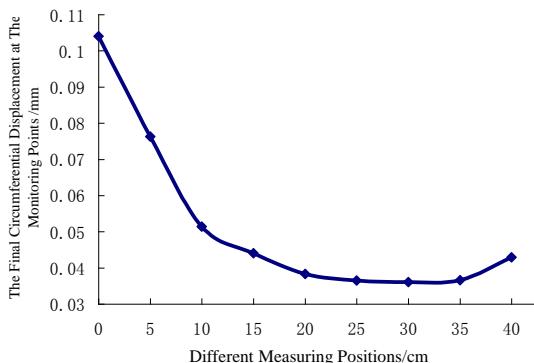


Fig.6 Variation of Circumferential Displacement With Measuring Point

3.4 Aperture ratio analysis of simulation results

In order to define the drilling aperture ratio on the measurement results and seek the most reasonable way of measuring, measuring point displacements under different aperture ratio is analyzed. Fig.7 reflects the changed trend of monitoring displacement under

different aperture ratio during the stress relieving process.

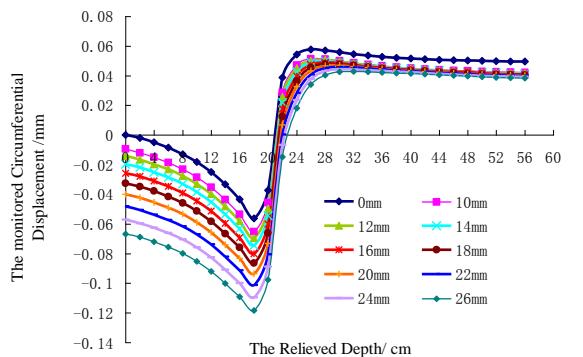


Fig.7 The Circumferential Displacement in The Different Aperture Ratio

As can be seen from the figure, the whole process of stress relief can be divided into three stages. When relieved depth did not reach monitoring, circumferential displacement moves along the radius direction to the center, which led by stress transfer, and it is equivalent to excavation effect. When relieved depth close to the monitoring point, along the circumferential displacement into the direction of the radius outward growth, the core outward expansion; and the third phase is when relieved depth reaches a certain value, displacement gradually stabilized, suggested that the stress on the core has been completely released.

Analysis the curve under the different aperture ratio , which can be found that part of the displacement in

the process of drilling had lost and could not be monitored by the strain gauge .Using β represents the losing displacement, then

$$\beta = \left(1 - \frac{u_i}{u_0} \right) \times 100\%$$

Where u_i is the displacement in different aperture ratio; u_0 is the displacement in no hole.

Analyzed the data and the results are shown in Table 3 and Fig.8. With the increase of r, the error caused by the drilling hole will decrease. Through the expression of K_1 , K_1 's value will decrease when r increases, then

Table 3 Displacement Error Caused by The Different Aperture Ratio

Radius/mm	0	10	12	14	16	18	20	22	24	26
Aperture Ratio	--	6.65	5.54	4.75	4.16	3.69	3.325	3.02	2.77	2.56
Stable Displacement / $\times 10^{-3}$ mm	5.02	4.65	4.59	4.55	4.51	4.47	4.42	4.37	4.30	4.22
β	--	7.4	8.6	9.4	10.2	11.0	11.6	0.129	14.4	16.0

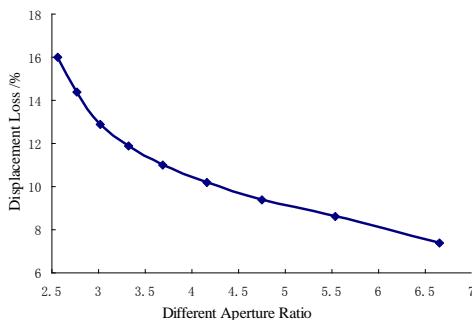


Fig.8 Effects of Different Aperture Ratio on Displacement

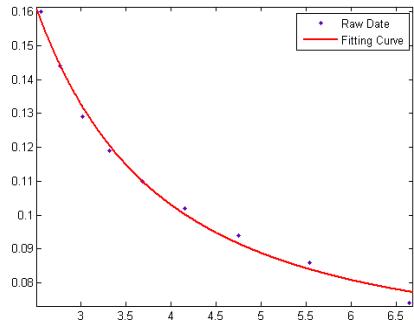


Fig9 Fitting Curve by Using Matlab

according to the formula (1) the calculation of the stress will increase accordingly. Therefore a direct result of stress measurement is lower when r smaller, also suggests that thick holes is conducive to improve the accuracy of measurement. To determine the loss of displacement by drilling holes, using Matlab to fit the curve, as shown in figure 9. After fitting, the curve equation is $\beta = 0.5546r^{(-1.856)} + 0.06$, When r is determined according to the equation the measured data can be corrected. It can make displacement closer to the actual displacement; thereby can increasing the measurement accuracy.

4 Analysis of geostress measurement results in the Datai mine

Information on stress measurement by Datai mine as an example of measurement error caused by drilling aperture ratio. The mine average surface elevation between 400 and 500m, geotress measurement level of observation point is located at -510m roadway, as shown in figure 10.

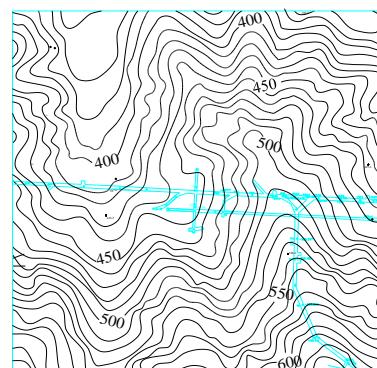


Fig10 Topographic Map About Datai Mine

The rock is diabase in geostress measurement section and is relatively hard. Measuring points are away from the stress concentrated area, mining - affected zone ,faults and other geological structure^[10], as shown in figure 11.Measuring method by using KX-81 hollow inclusion strain cells. Drilled large holes with a diameter of 133mm, the hole diameter is 36mm, the size of the hole radius ratio of 3.69.After installing the strain gauge about 24 hours for the curing of epoxy, stress relieving.

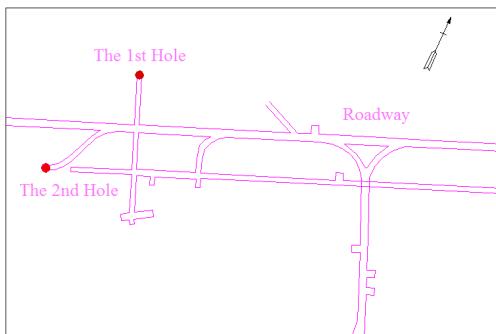


Fig11 Drill Hole Location

Table 4 The Stress Components of The Measuring Point

σ_x /MPa	σ_y /MPa	σ_z /MPa	τ_{xy} /MPa	τ_{yz} /MPa	τ_{xz} /MPa
22.32	42.47	24.46	-8.63	0.93	-0.24

Table 5 Comparison of Error

Theoretical Value/MPa	Measured Value/MPa	Measurement Error/%	Correction/MPa	Correction Factor/%
26.57	24.46	7.94	27.12	2.1

5. Conclusions

Using hollow inclusion strain cells to measure the size and direction of geostress is one of the general methods, it is simple and adaptable. However, there are still some errors on the measurement accuracy. There are many reasons affecting the measurement accuracy, this paper analyzed the influence on the measurement accuracy with the placement of sensor, drilling aperture ratio.

(1) Arrangements of measuring positions are hardly effected by aperture ratio. It related to the location of the hole's depth. As the depth of the measuring point increase, displacement will be smaller by the position. Displacement difference can be ignored after the

In this paper, the simulation analysis shows that the measurement of displacement is less than the actual value in ratio, which in turn caused the geostress smaller. According to the measured strain data, measuring points and geometrical parameters of rock mechanics parameters, calculated by the Institute of Geomechanics, Chinese Academy of Geological Sciences Stress of dedicated software, as shown in table 4. Using the modified formula correct measurement results , when $r = 3.69$, $\beta = 0.109$, then the result is 27.12MPa. According to the drilling of the mine area histogram and the rock density^[11], vertical stress and $\sigma_z = \gamma H$,the theoretical value is 26.57MPa. The measured and calculated values, are shown in table 5. The measured geostress is less than the theoretical value. It verified the correctness of simulation conclusions. Errors can be reduced by amending the measured results and improve the precision of measurement

midpoint of the hole, the sensor is suitable at that location.

(2) Drill holes will cause displacement damage, the displacement can not be record by the strain gauge. Drilling aperture ratio change will lead loss of displacement and correction coefficient K_1 to change, fitting the quantitative relationship between the displacement and loss of aperture ratio by the simulation results and the equation is $\beta = 0.5546r^{(-1.856)} + 0.06$.It can be verified by using measurement results to compare with theoretical value in Datai mine and can provide a reference for field measurements.

In addition, the analysis of the drilling aperture ratio on measurement accuracy of this paper is limited to numerical simulation .It needs further study.

6.Acknowledgements

This work is financially by the deep mining of coal mine ground pressure control in Heilongjiang Province and the opening of gas control key laboratory of fund projects(F2313-09);Shandong University of Science and Technology Science Fund for Distinguished Young(2011KYJQ106);Construction of Special Fund for “Taishan Scholars” in Shandong Province.

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