

Design for Reactive Power Compensator Based on Buck-Boost AC/AC Chopper

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Abstract: Aiming at the problem of voltage reduction and voltage distortion due to the extensive use of inductive loads, and some shortcomings of existing reactive power compensation devices, a new AC-AC chopper based on compensator is proposed. The basic principles, compensation characteristics and topology of the Buck-Boost AC-AC chopper based var compensator are described, the mathematical model of Buck-Boost based on state-space equation is established, the relationship between duty ratio and compensation current is derived. The instantaneous reactive power theory and direct current control method are adopted to build a MATLAB model. The results indicate that the real-time compensation of reactive power in grid side can be realized by this var compensator based on a direct controlled Buck-Boost AC—AC chopper, it has potential application value.

Introduction

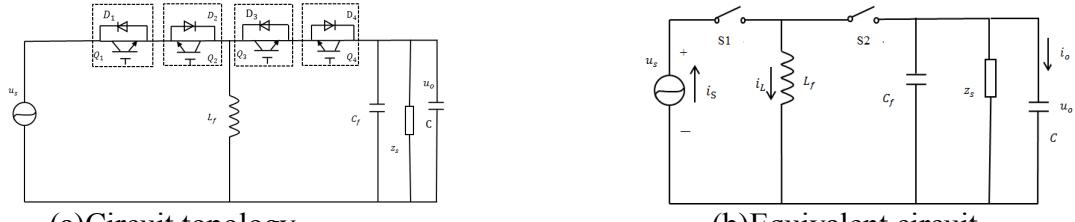
With the rapid development of industrial processes, power grid demands change drastically, especially the growing of impact load (such as a large rolling mill, electric tram, power converter device). Generally speaking, the booting process of those electrical equipment is short, during the booting process frequency keep a high level, large amounts of dynamic reactive power was absorbed frequently, those factor cause rapid bus voltage fluctuation, bringing power grid stability a negative impact. It is urgent to resolve the problem such as how to improve the power factor of the power system, how to improve voltage stability of user and the grid, how to balanced three-phase active and reactive loads have become a serious problem [1].

The basic principles of the Buck-Boost AC-AC chopper based var compensator

Buck-Boost AC-AC chopper based var compensator consists of Filter in grid side, AC/AC Chopper and Compensation capacitor. Filter is mainly used to eliminate the interference of multiple frequency harmonics and edge frequency harmonic component of breaker to power grid.

If a Buck-Boost AC-AC chopper based var compensator is added between grid and capacitor, by controlling switch status of chopper circuit, we can get a capacitive current whose angle 90 degrees ahead of the grid voltage [2]. The amplitude of the current is adjustable. This capacitive current can continuously and dynamically compensate reactive power of AC side, and finally make the power factor of grid is 1.

The Figure 1 shows the reactive power compensator principle diagram based on Buck-boost AC/AC chopper, Q1, Q2 and Q3, Q4 are two bidirectional switch respectively consisting of two IGBT series reversely [3]. These two switches complementary closing. Inductor L_f is used to storage. Capacitor C_f is used to eliminate the higher harmonic components of switching frequency and its multiples frequency. C is reactive power compensation capacitor. The two switchs, s1 and s2, works as complementary roles. For purposes of analysis, Figure 2(a) equivalent circuit can be simplified as shown in Figure 2(b).



(a)Circuit topology

(b)Equivalent circuit

Fig.1 Reactive power compensator principle diagram based on Buck-boost AC/AC chopper

Under the conditions of all the components in circuit is ideal devices. The input voltage is expressed as u_s , dealing with the chopper circuit, then obtained a voltage expressed as u_0 . Switching frequency is f_s . Switching cycle $T_s = 1/f_s$. Duty-cycle of S1 is D ($0 < D < 1$). Define a functions $\xi(t)$ 、 $\delta(t)$. When S1 is turned on, S2 turned off, $\xi(t)=1$ 、 $\delta(t)=0$, When S2 is turned on, S1 turned off, $\xi(t)=0$ 、 $\delta(t)=1$ [4]. That is:

$$\xi(t)=\begin{cases} 1(0 \leq t \leq DT_s) \\ 0(DT_s \leq t \leq T_s) \end{cases} \quad (1)$$

$$\delta(t)=\begin{cases} 0(0 \leq t \leq DT_s) \\ 1(DT_s \leq t \leq T_s) \end{cases} \quad (2)$$

In order to facilitate analysis, consider voltage at the end of the inductor. When the high-frequency switch S1 is turned on, S2 turned off, voltage of inductor $u_L = u_s$. When S1 is turned off, S2 turned on, $u_L = u_0$. That is:

$$0 \leq t \leq DT_s \text{ 时}, u_L = u_s ;$$

$$DT_s \leq t \leq T_s \text{ 时} u_L = u_0$$

So, that: $u_L = \xi(t)u_s + \delta(t)u_0$

According the formula to Fourier series expansion:

$$\xi(t)=D+\frac{2}{\pi}\sum_{K=1}^{\infty}\frac{1}{K}\sin\Phi_K\cos(k\omega_0-\Phi_K) \quad (3)$$

$$\delta(t)=1-D+\frac{2}{\pi}\sum_{K=1}^{\infty}\frac{1}{K}\sin\Phi_K\cos(k\omega_0-\Phi_K) \quad (4)$$

Fundamental frequency of $\xi(t)$ 、 $\delta(t)$ is ω_0 , $\omega_0 = 2\pi/T_s$. The initial phase angle $\Phi_K = k\pi D$. Because the average value of u_L is 0, $\xi(t)u_s + \delta(t)u_0 = 0$. If $u_s = U_s \sin\omega_s$:

$$u_o=\frac{D+\frac{2}{\pi}\sum_{K=1}^{\infty}\frac{1}{K}\sin\Phi_K\cos(k\omega_0-\Phi_K)}{-\left[1-D+\frac{2}{\pi}\sum_{K=1}^{\infty}\frac{1}{K}\sin\Phi_K\cos(k\omega_0-\Phi_K)\right]}U_s\sin\omega_s \quad (5)$$

After ignoring latter part of $\delta(t)$, the formula changed:

$$u_o=-\frac{D}{1-D}U_s\sin\omega_s-\frac{2U_s}{(1-D)\pi}\sum_{K=1}^{\infty}\frac{1}{K}-\sin\Phi_K * \{ \sin[(k\omega_0+\omega_s)t-\Phi_K]-\sin[(k\omega_0-\omega_s)t-\Phi_K] \} \quad (6)$$

Analysis of the formula (6), in addition to containing the fundamental frequency components, there are higher harmonic components, high-frequency part can be filtered out by the low-pass filter, so get the following equation:

$$u_o=-\frac{D}{1-D}U_s\sin\omega_s=-\frac{D}{1-D}u_s \quad (7)$$

$$i_o = \frac{u_o}{-j \frac{1}{\omega_s c}} = j\omega_c u_o = -\frac{\omega_s C D}{(1-D)} U_s \cos \omega_s t \quad (8)$$

Formula (8) showed that, Buck-Boost AC-AC chopper based var compensator can be viewed as a capacitor whose capacitance value can be adjusted continuously. We can complete reactive power dynamic compensation of the grid by controlling the duty-cycle of the switch.[5].

Simulation and experimental verification

To verify the rationality and right of reactive power compensation feature and direct current control strategy mentioned in this paper, we use the Simulink component library of MATLAB to build the simulation model of Buck-Boost AC-AC chopper based var compensator whose line voltage is 220V/50Hz. Reactive power of load Q=3kvar; Switching frequency =10kHz; Inductor =10H; Filter capacitor=20uF; Compensation capacitor C=2mF.

Figure 2(a),(b),(c) shows the compensation current waveform of grid getting from the output voltage and Buck-Boost AC-AC chopper based var compensator when duty-cycle is 0.2, 0.5, 0.8. Simulation result shows that compensation current is the capacitive current whose frequency is the same as output voltage and ahead of phase angle of output voltage , which can compensate grid reactive power. From the experimental results, we know that we can control the size of compensation current by regulating the duty-cycle of Buck-Boost AC-AC chopper based var compensator. As the picture shows, when duty-cycle changes from 0.2 to 0.8, compensation current changes from 34.4A to 550A at the same time, which shows that Buck-Boost AC-AC chopper based var compensator has a bigger adjusting range. Figure 4(d), (e) shows the waveform of grid voltage and current before and after using the Var compensator. From the simulation result, we can know that before using the Var compensator, Power factor angle of system $\alpha=52^\circ$, Power factor $\lambda=0.62$. After using the Buck-Boost AC-AC chopper based var compensator, Power factor angle $\alpha=9^\circ$. Grid voltage and current in frequency and phase is almost synchronization and the power factor is approximately 1, which verifies the veracity and feasibility of control strategy and the effectiveness of Buck-Boost AC-AC chopper based var compensator.

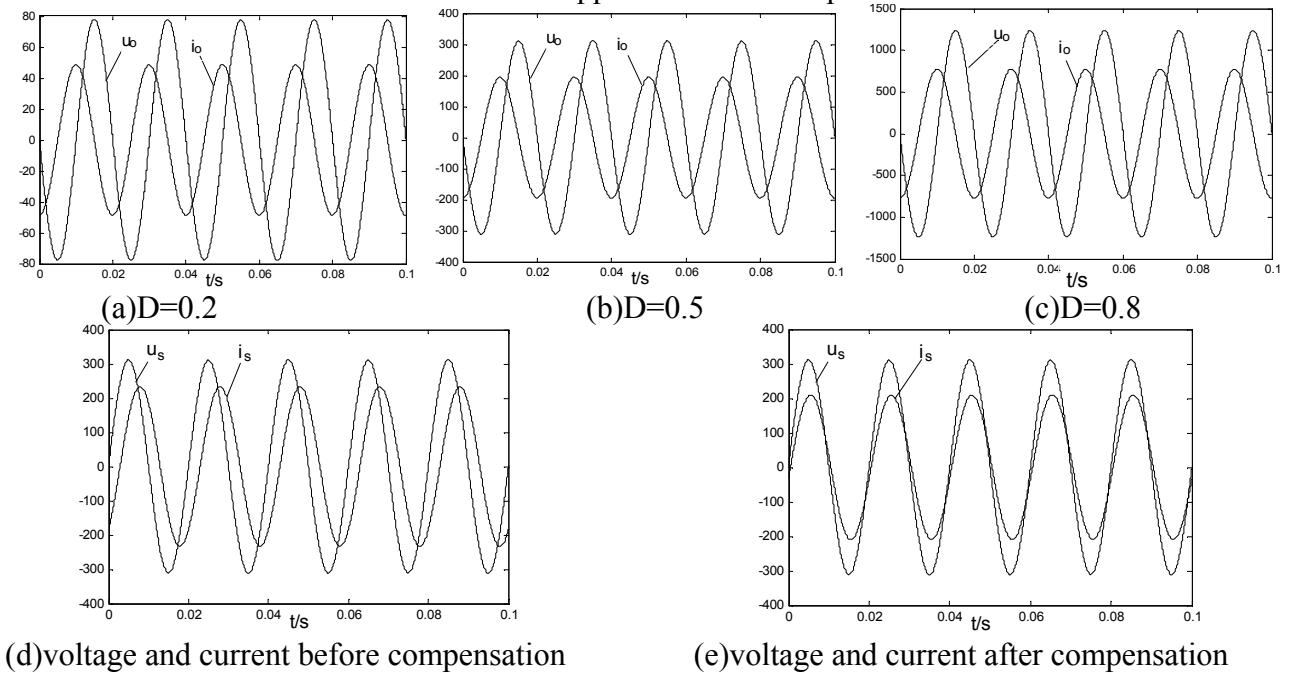


Fig.2 The results of simulation diagram

Conclusion

According to the analysis of the basic principles and topology of the Buck-Boost AC-AC

chopper based var compensator, we get the relationship between compensation current and duty-cycle. Using PWM technology to control the compensator and simulation results of MATLAB software show that: Buck-Boost AC-AC chopper based var compensator can real-time and tracking compensating to reactive power frequency.

References

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