

## A continuum model in traffic flow considering the jerk effect

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**Abstract:** Based on the optimal velocity model, a new continuum model considering the jerk term is mentioned in this paper. Then, the critical condition for the steady traffic flow is deduced. Near the neutral stability line, nonlinear analysis is taken to derive the KdV-Burgers equation for describing the traffic density and one of the solutions is given.

### The continuum model

Based on the OVM model[1], the jerk term is added to the dynamic equation, which is

$$\begin{cases} \frac{dv_n(t)}{dt} = a[V(\Delta x_n(t)) - v_n(t)] - \lambda J_n(t) \\ J_n(t) = \frac{dv_n(t)}{dt} - \frac{dv_n(t-1)}{dt} \end{cases} \quad (1)$$

in which  $V$  means the optimal velocity given by Bando and the  $\lambda$  is the jerk parameter.

Considering the headway - density formula given by Berg et al. [2]

$$\Delta x \approx \frac{1}{\rho} - \frac{\rho_x}{2\rho^3} - \frac{\rho_{xx}}{6\rho^4} \quad (2)$$

and the relationship transferring microscopic variables in Eq.(1) into the macroscopic ones as below

$$\begin{aligned} v_n(t) &\rightarrow v(x, t), v_{n+1}(t) \rightarrow v(x + \Delta, t), \\ V\left(\frac{1}{\rho}\right) &\rightarrow V_e(\rho), V'\left(\frac{1}{\rho}\right) \rightarrow -\rho^2 V'_e(\rho) \end{aligned} \quad (3)$$

and the Taylor expansions, Eq.(1) is rewritten as follows

$$\frac{\partial v}{\partial t} + v \frac{\partial v}{\partial x} = a[V_e(\rho) - v] - \lambda v v_{xt} + a V'_e(\rho) \left( \frac{\rho_x}{2\rho} + \frac{\rho_{xx}}{6\rho^2} \right) \quad (4)$$

Including the following continuity equation,

$$\frac{\partial v}{\partial t} + \frac{\partial(\rho v)}{\partial x} = 0 \quad (5)$$

We obtain the new model described by Eqs. (4)-(5).

### Stability analysis

For the convenience of analysis, we rewrite the Eqs. (4) and (5) as follow:

$$\frac{\partial \vec{U}}{\partial t} + \vec{A} \frac{\partial \vec{U}}{\partial x} = \vec{E} \quad (6)$$

The eigenvalues of the matrix  $\vec{A}$  are obtained as follows

$$\lambda_1 = \lambda_2 = v \quad (7)$$

From Eq.(7), we can see that the characteristic speeds  $dx/dt$  are equal to the macroscopic flow speed  $v$ , which demonstrates the fundamental principle that vehicle flows are anisotropic and response only to frontal stimuli.

Then, we use linear stability method to analyze the qualitative properties of this new model. Considering that the system is a uniform flow, and we apply a infinitesimally perturbation to the homogenous flow

$$\begin{pmatrix} \rho(x, t) \\ v(x, t) \end{pmatrix} = \begin{pmatrix} \rho_0 \\ v_0 \end{pmatrix} + \sum_k \begin{pmatrix} \hat{\rho}_k \\ \hat{v}_k \end{pmatrix} \exp(ikx + \sigma_k t) \quad (8)$$

With the replacement of  $\rho$  and  $v$ , the Eqs.(6) and (5) will be rewrite without the nonlinear higher-order terms as follows

$$\begin{cases} (\sigma_k + ik v_0) \hat{\rho}_k + ik \rho_0 \hat{v}_k = 0 \\ \sigma_k \hat{v}_k + v_0 \hat{v}_k ik = a \left[ \hat{\rho}_k V'_e(\rho_0) - \hat{v}_k \right] - \lambda v_0 \hat{v}_k ik \sigma_k \\ + a \hat{\rho}_k \left( \frac{V'_e(\rho_0)}{2\rho_0} ik + \frac{V''_e(\rho_0)}{6\rho_0^2} (ik)^2 \right) \end{cases} \quad (9)$$

Taking  $\hat{\rho}_k$  and  $\hat{v}_k$  as the unknown quantities of the equations, we can obtain that the unknown quantity  $\sigma_k$  satisfies the following quadratic equation

$$\begin{aligned} (\sigma_k + ik v_0)^2 + (a + \lambda v_0 ik \sigma_k)(\sigma_k + ik v_0) + \\ ik \rho_0 a V'_e(\rho_0) \left[ 1 + \frac{ik}{2\rho_0} + \frac{(ik)^2}{6\rho_0^2} \right] = 0 \end{aligned} \quad (10)$$

In the state that both roots of  $\sigma_k$  have negative real parts the stable traffic flow will be obtained.

$$a_s = -2\rho_0^2 V'_e(\rho_0) \left[ 1 - \frac{k^2}{6\rho_0^2} \right]^2 \quad (11)$$

And

$$\text{Im}(\sigma_k) = -k[v_0 + \rho_0 V'_e(\rho_0)] + o(k^3) \quad (12)$$

Considering Eq.(12), the critical speed of disturbance propagation will be obtained as

$$c(\rho_0) = v_0 + \rho_0 V'_e(\rho_0) \quad (13)$$

which is mentioned in Ref.[3].

## Nonlinear analysis

The system behavior around the neutral stability condition attracts our attention. Then the role of time  $t$  and space  $x$  is concentrated in the variant  $z$  [4]

$$z = x - ct \quad (14)$$

So we can rewrite the Eqs. (4) and (5)

$$-c\rho_z + q_z = 0 \quad (15)$$

$$\begin{aligned} -c v_z + v v_z = a[V_e(\rho) - v] - \lambda v(-c v_{zz}) \\ + a V'_e(\rho) \left( \frac{\rho_x}{2\rho} + \frac{\rho_{xx}}{6\rho^2} \right) \end{aligned} \quad (16)$$

where  $q$  is the product of density and velocity. Also, we can get

$$v_z = \frac{c\rho_z}{\rho} - \frac{q\rho_z}{\rho^2} \quad (17)$$

We expand the flow  $q$  as

$$q = \rho V_e(\rho) + b_1 \rho_z + b_2 \rho_{zz} \quad (18)$$

which represents the flow  $q$  with the homogeneous, stability, and stable characters.

Combining the two equations above and introducing them in the Eq.(16), we can get

$$\begin{aligned} & -c \left( \frac{c\rho_z}{\rho} - \frac{q\rho_z}{\rho^2} \right) + \frac{q}{\rho} \left( \frac{c\rho_z}{\rho} - \frac{q\rho_z}{\rho^2} \right) = \\ & a \left[ V_e(\rho) - \frac{q}{\rho} \right] - \lambda \frac{q}{\rho} (-c) \\ & \left( \frac{c\rho_{zz}}{\rho} - \frac{c\rho_z^2}{\rho^2} - \frac{q\rho_{zz}}{\rho^2} - \frac{c\rho_z^2}{\rho^2} + \frac{2q\rho_z^2}{\rho^3} \right) \\ & + aV_e'(\rho) \left( \frac{\rho_z}{2\rho} + \frac{\rho_{zz}}{6\rho^2} \right) \end{aligned} \quad (19)$$

Balancing the coefficients of  $b_1$  and  $b_2$  in the both sides of Eq.(19), we can deduce

$$\begin{cases} b_1 = \frac{1}{2a} (V_e(\rho) - c)^2 + \frac{1}{2} V_e'(\rho) \\ b_2 = \frac{V_e'(\rho)}{6\rho} + \frac{c\lambda V_e(\rho)}{a} (c - V_e(\rho)) \end{cases} \quad (20)$$

With Taylor expansions, we rewrite Eq.(18) near the neutral stability condition

$$\rho V_e(\rho) \approx \rho_h V_e(\rho_h) + (\rho V_e)_\rho \Big|_{\rho=\rho_h} \hat{\rho} + \frac{1}{2} (\rho V_e)_{\rho\rho} \Big|_{\rho=\rho_h} \hat{\rho}^2 \quad (21)$$

With Eq. (18) and (21), another equation can be deduced

$$\begin{aligned} & -c\rho_z + \left[ (\rho V_e)_\rho + (\rho V_e)_{\rho\rho} \rho \right] \rho_z + b_1 \rho_{zz} + b_2 \rho_{zzz} \\ & = 0 \end{aligned} \quad (22)$$

To obtain a regular form, some variable substitutions are taken

$$U = - \left[ (\rho V_e)_\rho + (\rho V_e)_{\rho\rho} \rho \right] X = ms, \quad T = -mt \quad (23)$$

Hence, we can deduce the KdV-Burgers equation as follows

$$U_T + U_X - mb_1 U_{XX} - m^2 b_2 U_{XXX} = 0 \quad (25)$$

of which one of the solutions is

$$\begin{aligned} U = & - \frac{3(-mb_1)^2}{25(-m^2 b_2)} \\ & \left[ 1 + 2 \tanh \left( \pm \frac{-mb_1}{10m^2} \right) \left( X + \frac{6(-mb_1)^2}{25(-m^2 b_2)} T + \zeta_0 \right) + \right. \\ & \left. \tanh^2 \left( \pm \frac{-mb_1}{10m^2} \right) \left( X + \frac{6(-mb_1)^2}{25(-m^2 b_2)} T + \zeta_0 \right) \right] \end{aligned} \quad (27)$$

in which  $\zeta_0$  is an arbitrary constant.

## Summary

In this paper, the jerk term that indicates the sharp change of accelerated speed in the real traffic has been added to the traditional OVM model. Considering the jerk term, the stability condition of the new OVM model has been studied and then the KdV-Burgers equation has been derived and one of the solutions is given to describe the evolution of density wave happened in the traffic flow.

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