

the Contact Reliability Analysis of Gear Rack Based on the Kriging and RSM Method

Hui Liu ^{1,a}, Wei-Min Cui ^{2,b}, Bo He ^{3,c}, Xiang-Rui Gong ^{4,d}

¹ Northwestern Polytechnical University, Xi'an, China

² Northwestern Polytechnical University, Xi'an, China

³ Northwestern Polytechnical University, Xi'an, China

⁴ Northwestern Polytechnical University, Xi'an, China

^aliuhui-1991@163.com, ^bcuiwm.nwpu.edu.cn, ^chebo2009@126.com, ^dgxru1991@163.com

Keywords: gear rack; Kriging; response surface method

Abstract. Obtaining the performance function of gear contact is difficult, and this paper founded the response surface model and the Kriging model with the usage of response surface and Kriging method. Then the reliability was calculated by the founded metamodel using Monte Carlo method. The result shows the kriging method owns a better accuracy than response surface method in numerical fitting.

Introduction

The gear rack is widely used in engineering, including steering mechanism, feeding mechanism of machine tool, wing flap, etc. It usually bears vast loads, causing failure modes of gear teeth snap, tooth surface wear, teeth surface pitting and tooth face agglutination. Accordingly, it is of high engineering usage value to analyze loading conditions of gear rack, check the strength of contact area, and propose a reliability assessment method.

The traditional designing method has been used until now but it can not actually reflect the objective situation without considering the uncertainty of the item. There are lots of blindness and experience in it.

This paper will redesign the variable and change them into random variables, which will obey the probability distribution. Then the model of gear rack was established and performance function was founded by surrogate model of Kriging method and response surface method. The results were compared after reliability was calculated by Monte Carlo method and referential experiences were concluded.

1 Finite Element Analysis of Gear Pair

1.1 Geometry Model of Gear Pair

The material of gear rack is isotropic material of 20CrMnTi with the yield strength of 835MPa, elasticity modulus of 207GPa, and the Poisson ratio of 0.3. The parameters of gear rack are shown in Table 1.

Table 1 the parameters of gear rack

	module[m]	number of teeth	Pressure angle[o]
gear	6	24	20
rack	6	23	20

1.2 The Finite Element Model of Gear Pair

The net is divided in Abaqus using C3D10. The net of contact area is specially intense, which is shown in Fig. 1.

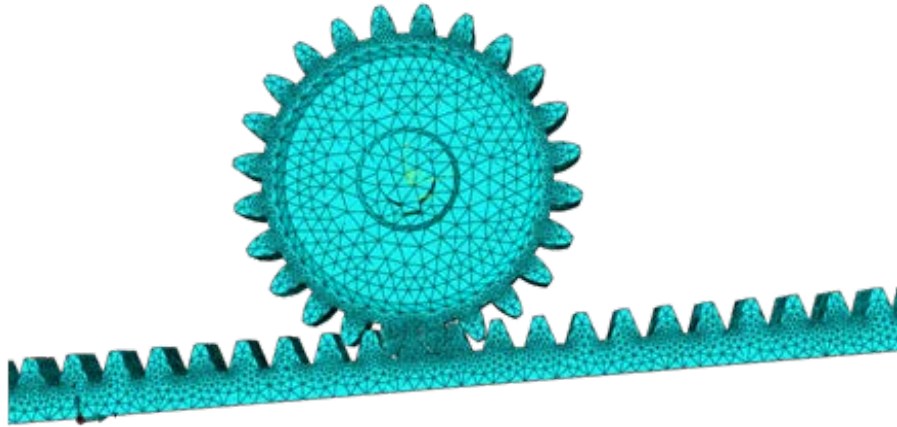


Figure 1 gear rack net division

The Mises stress nephogram is shown in Fig. 2

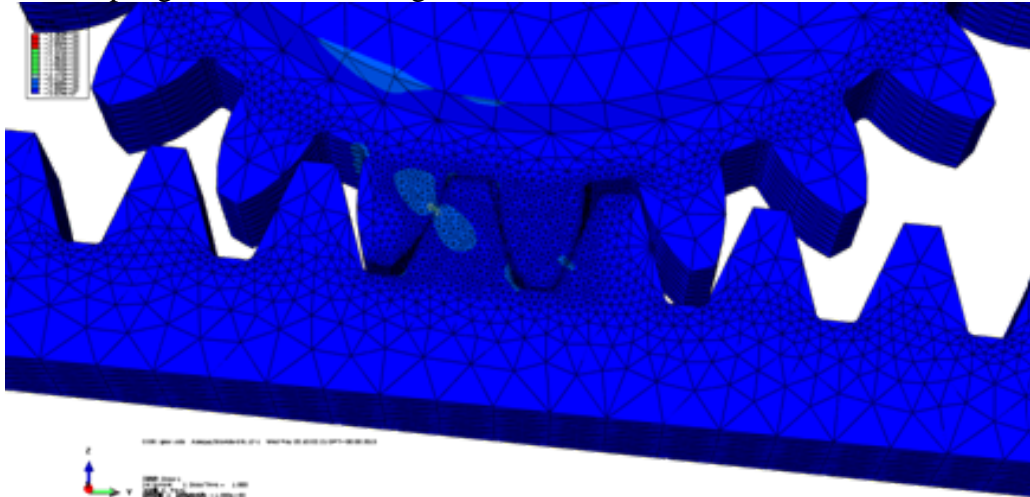


Figure 2 the Mises stress nephogram of gear rack

From the Mises stress nephogram we can see the biggest stress is generated in the contact surface and the root of tooth being 730.2MPa, which is less than the finite stress of 835MPa. It is convincing that the contact surface bears high stress and the root of the tooth is bearing high bending load, easily causing the fatigue and spalling of contact surface. According to this, it is necessary to perform an analysis of reliability.

2 Establishment of Surrogate Model by Kriging Method

2.1 Introduction of Kriging Method

The Kriging method is developed by Matheron[1] based on the achievement of Krige, with a high accuracy in nonlinearity. Giunta[2] studied the problem of multi-disciplinary design optimization using the Kriging method. Kaymaz[3] introduced the Kriging method into reliability analysis.

The Kriging method is composed of two parts: polynomial and random distribution.

The specific model is:

$$y(x) = F(\beta, x) + z(x) = f^T(x)\beta + z(x) \quad (1)$$

The β is regression coefficient, $f(x)$ is polynomial. In design space, $f(x)$ offers global approximate, namely mathematical expectation; While $z(x)$ offers local deflection approximate, namely local variation of $y(x)$.

2.2 Random Variable and Performance Function

There is no analytical expression of limit state function for the gear rack contact problem, which means the limit state function is implicit. The performance function is shown as follows based on the stress-intensity interference theory:

$$\sigma_s - G(D, E, T) = \begin{cases} < 0 \text{ failure} \\ = 0 \text{ limit} \\ > 0 \text{ reliable} \end{cases} \quad (2)$$

Where D is distance between reference circle of gear rack (mm), E is elasticity modulus (GPa), T is torque (NM) and σ_s is yield strength (MPa).

The four variables are chosen as random variables, and obeys normal distribution, the distribution is shown as follows:

$$D \sim N(0, 0.17) \quad E \sim N(207, 6.9) \quad T \sim N(200, 6.67) \quad \sigma_s \sim N(835, 28.33)$$

Normally, the fitting precision will grow with the number of sample points but the calculation cost will grow simultaneously. This paper chooses 18 groups of sample points.

2.3 Calculation of Stress Response

This paper performs an analysis of gear rack using Abaqus after sample points are obtained. FEA results of 18 groups of sample points are obtained by changing the parameters of variables, which is shown in Table 2:

Table 2 variables and response value

D[mm]	E[GPa]	T[NM]	stress[MPa]
0.0991	211.5900	199.79	736.101
-0.0447	198.1300	202.39	745.677
0.1527	198.3800	198.5475	731.521
0.0886	210.3000	189.255	697.289
-0.1905	212.3000	220.98	814.168
-0.0043	207.9300	194.3725	716.142
0.1466	198.5200	194.23	715.614
-0.0379	212.3800	198.605	731.736
0.0221	214.3100	191.4025	705.201
0.0313	202.1800	203.7425	750.66
-0.1797	204.7600	196.7375	724.553
-0.1207	201.7500	189.07	696.605
0.2764	193.9700	198.6775	731.998
0.5020	201.6700	204.0275	751.71
-0.0453	210.3800	200.8075	739.85
-0.1357	206.9500	204.4525	753.277
0.2175	207.4700	204.8975	754.917
-0.2177	203.1100	187.2	689.716

2.4 Establishment of Kriging Model

Choose the 18 groups of sample points and the FEA response as basic information. Because of the minor impact of polynomial $f(x)$ to the accuracy of Kriging model, the regressor is selected as 1.

Relevant equation is determined factor to the accuracy of model, so this paper chooses the good-performed Gaussian correlation equation.

2.5 The Verification of Kriging Model

It is necessary to compare the FEA results with the Kriging model results after the Kriging model is established. 10 groups of sample points is selected in the value space, and the results are shown in Table 3 and Fig. 3.

Table 3 comparison between Kriging and FEA

D[mm]	E[GPa]	T[NM]	Kriging[MPa]	FEA[MPa]	error
-0.1341	198.8998	193.9470	714.3263929	714.572	3.44E-4
0.0718	211.3788	198.1070	729.9031455	729.946	5.87E-5
0.0110	201.0746	195.5445	720.4001554	720.458	8.03E-5
0.1601	209.9278	196.4487	723.7733095	723.791	2.44E-5
0.1555	215.9429	209.2762	770.6955268	771.051	4.61E-4
0.1538	212.3869	198.8159	732.4670427	732.513	6.27E-5
0.0670	197.5341	209.4386	771.6474246	771.644	4.44E-6
0.0420	215.8056	198.8815	732.6486995	732.755	1.45E-4
0.0495	205.2421	205.6488	757.7143054	757.684	4.00E-5
0.0490	207.8876	198.2804	730.5523406	730.539	1.83E-5

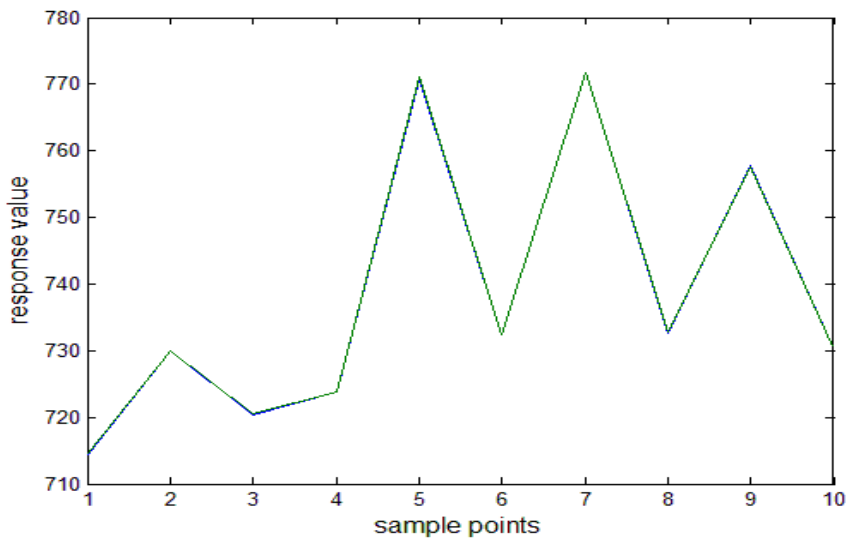


Figure 3 comparison between Kriging and FEA

The relative error between Kriging and the FEA results is in a minor scale judged From Table 3. So it is convincible that the founded Kriging model is of high accuracy.

2.6 the Reliability Calculation of Gear Rack Contact

Select 10000000 groups of samples to calculate the failure probability by Monte Carlo method. The failure probability is 0.004433 and the reliability is 0.995567.

3 Surrogate Model Establishment by Response Surface Method

3.1 Introduction of RSM

The basic idea of response surface method is to approximate implicit limit state function by polynomial. The polynomial function will converge in probability to actual implicit limit state function by rational sample points and iteration strategy[4]. The weighted least-squares method can raise the effect of the ideal points while reduce the effect of the non-ideal points[5]. This paper utilize the nonlinear weighted response surface method to reflect the effect of nonlinearity, which is shown as follows:

$$g(x) = b_0 + \sum_{i=n+1}^n b_i x_{i-n}^2 + \sum_{i=n+1}^{2n} b_i x_{i-n}^2 \quad (3)$$

Where $b = (b_0, b_1, \dots, b_{2n})^T$ is undetermined coefficient
The foundation of weight is:

$$\begin{cases} g_{best} = \min_{i=1}^m |g(x_i)| \\ w_i = \frac{g_{best}}{|g(x_i)|} \end{cases} \quad i = 1, 2, \dots, m \quad (4)$$

$$b = (a^T W a)^{-1} \times a^T W y \quad (5)$$

Where n is the variable number;w is the weight matrix.

3.2 the establishment of the response surface method

Choose the 18 groups of sample points and the FEA response as basic information to calculate the coefficients of the fitting function. Then 8 groups of sample are selected to compare the relative error between the value of response surface method(RSM) and finite element analysis, which is shown in Table 4 and Fig. 4.

Table 4 comparison between RSM and FEA

D[mm]	E[GPa]	T[NM]	RSM[MPa]	FEA[MPa]	error
0.0718	211.3788	198.1070	729.7984832	729.946	-1.43E-04
0.0110	201.0746	195.5445	720.3467979	720.458	-7.41E-05
0.1601	209.9278	196.4487	723.7099703	723.791	-8.75E-05
0.1555	215.9429	209.2762	770.9768998	771.051	3.65E-04
0.1538	212.3869	198.8159	732.4226522	732.513	-6.06E-05
0.0670	197.5341	209.4386	771.5600156	771.644	-1.13E-04
0.0420	215.8056	198.8815	732.6364468	732.755	-1.67E-05
0.0495	205.2421	205.6488	757.5844784	757.684	-1.71E-04
0.0490	207.8876	198.2804	730.4329559	730.539	-1.63E-04
-0.1341	198.899	193.9470	714.4021337	714.572	1.06E-04

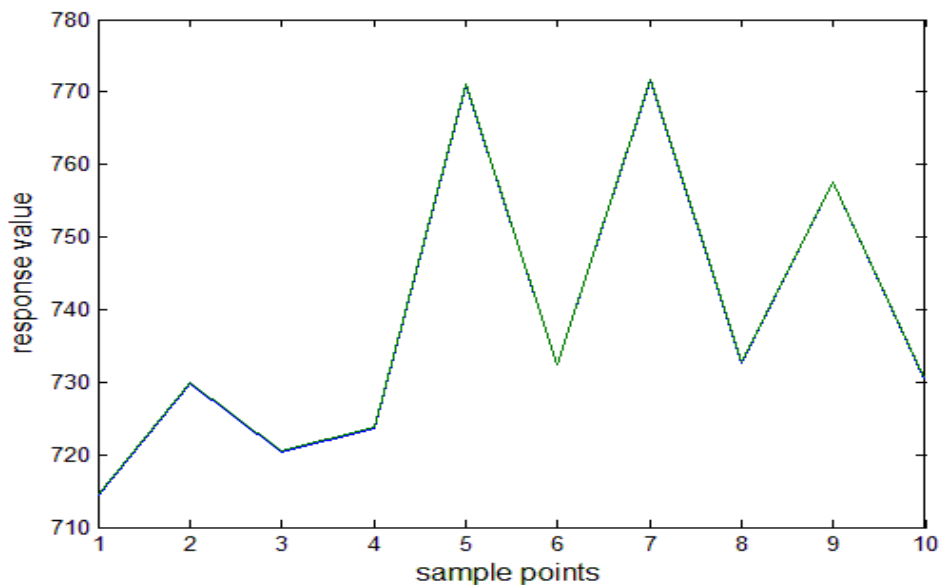


Figure 4 comparison between RSM and FEA

The relative error between RSM and the FEA results is in a minor scale judged From Table 4. So it is convincible that the founded RSM model is of high accuracy.

3.3 the reliability calculation of gear rack contact

Select 10000000 groups of samples to calculate the failure probability by Monte Carlo method. The failure probability is 0.004302 and the reliability is 0.995698.

4 Comparison between Kriging method and RSM

Compared to the response surface method, the Kriging method is of higher accuracy when fitting the input-output function of gear rack contact judged by the former results. Accordingly, Kriging method is more convincing when calculating the gear rack contact reliability.

The reason lies in the high nonlinearity, in which situation the Kriging method is more likely to obtain an accurate results, and owns good adaptation.

Conclusions

This paper analyzed the gear rack contact reliability by surrogate model. The main work is as follows:

- (1) The contact stress under certain working condition is analyzed in abaqus.
- (2) The surrogate model is founded utilizing the Kriging method and response surface method. Then the reliability is respectively calculated by Monte Carlo method.
- (3) The accuracy of two surrogate models is compared and the Kriging method can reach a higher accuracy in the issue of gear rack contact.

References

- [1] DU De-wen, MA Shu-zhen, CHEN Yong-liang. Overview of the methods in geology statistics [J]. Journal of World Geology, 1995, 14(4):79 -84.
- [2] Giunta A A. Aircraft multidisciplinary design optimization using design of experiments theory and response surface modeling [D]. Blacksburg, Virginia: Virginia Polytechnic Institute and State University, 1997.
- [3] Kaymaz I. Application of kriging method to structural reliability problems [J]. Structural Safety, 2005, 27(2):133 -151.
- [4] Lv Zhen zhou. Reliability and sensitivity analysis of structure and mechanism [M]. Beijing: Science Press. 2009.
- [5] Zhao Jie. Study of response surface method in mechanism reliability analysis [D]. Xi'an: Northwest Polytechnical University. 2006