# A new matrix decomposition method for estimating the position of prism based stereovision 

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#### Abstract

In this paper, a new matrix decomposition method was proposed for estimating the position of prism based stereovision. The prism was considered as a single optical system composed of few refractive planes. A transformation matrix which relates the coordinates of an object point to its coordinates on the image plane through the refraction of the prism was derived based on geometrical optics. A matrix decomposition method which is able to calculate the position of an arbitrary faces prism was introduced. This model further extends the application of the single-lens stereovision system using a prism to other areas. Experimentation results are presented to prove the effectiveness and robustness of our proposed model.


## Introduction

Stereovision, an important field in computer vision, aims to recover the shape, size or location of an object from two or more images taken from different viewpoints. According to the number of cameras used, it can be divided into multi-camera based method and single-camera based method.

Multi-camera based method employs two or more cameras to capture images from different views. It is currently used for space exploration [1], panoramic reconstruction [2], robot navigation or other volume static target measurements and surface reconstruction [3]. Yet such measurement system has some known issues: 1) It is expensive due to the use of multiple cameras; 2) In order to obtain a high accuracy, the distance of baseline must be long enough, resulting in large system size; 3) the working condition between multiple cameras cannot be completely consistent, thus affecting the measurement accuracy; 4) cameras capture time cannot be synchronized accurately, which will cause the errors in dynamic target measurement. To overcome these limitations, the concept of single-camera stereo vision has been proposed and attracted great research interests.

The single-camera stereovision system can be classified into two categories. One is depth recovery by exploiting some known cues such as the environment or the movement of the camera [4-6]. The second is depth recovery by the reflective or refractive properties of optical devices such as mirrors [7] or prisms. Among these methods, prism-based stereovision may have the simplest system structure. With the use of only one camera, it could reduce the cost and eliminate the multi-camera synchronization problem. In addition, the system is more compact which has the potential for wide range of applications having space constraints.

In this paper, a new matrix decomposition method was proposed for estimating the position of prism based stereovision system, this new method can improve the 3D reconstruction with high precision for speed control and high dynamic quality.

## Refraction of an Arbitrary Plane

The refraction of prism can be regarded as a ray refracted by two planes with inverse refractive index respectively. Thus, we will start from the virtual point formed by the refraction of an arbitrary plane, and the imaging model of prism can be acquired simply by combine the twice refractions. As shown in Fig.1, $\Pi$ is an arbitrary plane with equation $n_{x} \cdot x+n_{y} \cdot y+n_{z} \cdot z+d=0$ in 3D space with surface normal $N=\left[n_{x}, n_{y}, n_{z}\right]^{T}$. $A=\left[x_{0}, y_{0}, z_{0}\right]^{T}$ is a point in front of this plane. PB is a line segment which is perpendicular to plane $\Pi$. $P C$ is an incident ray intersecting $\Pi$ at point $C$, and the back extension line of its refracted ray intersects $P B$ at point $P^{\prime}=\left[x^{\prime}, y^{\prime}, z^{\prime}\right]^{T}$. According to Shell's law, it is clear that $\alpha$ is equal to the incident angle, and $\alpha^{\prime}$ is equal to the angle of refraction. Then, the relationship between point $P$ and $P^{\prime}$ can be expressed as below:

$$
\left[\begin{array}{l}
x^{\prime}  \tag{1}\\
y^{\prime} \\
z^{\prime}
\end{array}\right]=\left[\begin{array}{ccc}
q n_{x}^{2}+1 & q n_{x} n_{y} & q n_{x} n_{z} \\
q n_{x} n_{y} & q n_{y}^{2}+1 & q n_{y} n_{z} \\
q n_{x} n_{z} & q n_{y} n_{z} & q n_{z}^{2}+1
\end{array}\right]\left[\begin{array}{c}
x_{0} \\
y_{0} \\
z_{0}
\end{array}\right]+q d\left[\begin{array}{l}
n_{x} \\
n_{y} \\
n_{z}
\end{array}\right]
$$

where $q=\tan \alpha / \tan \alpha^{\prime}-1$. From Eq. (1) we can see that the transformation from a 3D point $P$ to its virtual image point $P^{\prime}$ ' is the combination of a scale transformation (with scale factor: $\tan \alpha / \tan \alpha$ ') and a translation in the direction of $N$. When using the algebraic form, Eq. (1) can be rewritten as:

$$
\begin{equation*}
P^{\prime}=A P+t \tag{2}
\end{equation*}
$$

where $A=q N N^{T}+I, t=q d N$, and $I$ is unit vector. Moreover, $A$ also can be regarded as an affine transformation matrix, which is determined by $q$ and $N$. Thus it has four degree of freedom (DOF) which denotes that the refraction of a plane is not a rigid transformation. According to Snell’ law, $q$ can be converted to:

$$
\begin{equation*}
q=\frac{n \cos \alpha^{\prime}}{\cos \alpha}-1 \tag{3}
\end{equation*}
$$

where $n$ is the refractive index. If we use unit vector $V$ and $V$ ' to express the direction vector of $C P$ and CP' respectively, another form of Eq. (3) is

$$
\begin{equation*}
q=n \frac{V^{\prime} \cdot N}{V \cdot N}-1 \tag{4}
\end{equation*}
$$

Since $V^{\prime}$ also can be calculated from $V$, thus, when the material of the plane is determined, the $q$ can only be influenced by the direction vector of incident ray $V$.


Fig.1. Ray refraction of an arbitrary plane

## Perspective Projection Model

A 3D point is denoted by $P=[X, Y, Z]^{T}$. A 2D point is denoted by. $p=[u, v]^{T}$. If we use $\tilde{p}$ and $\tilde{P}$ to denote the homogeneous coordinates: $P=[X, Y, Z, 1]^{T}$ and $p=[u, v, 1]^{T}$ the relationship between a 3D point $P$ and its image projection $p$ is given by

$$
s \tilde{p}=M_{\mathrm{int}}\left[\begin{array}{ll}
R_{e} & \mathrm{t}_{e} \tag{5}
\end{array}\right] \tilde{\mathrm{P}}
$$

where $s$ is an arbitrary scale factor, [ $R_{e} t_{e}$ ], termed the extrinsic parameters, $R_{e}$ is the $3 \times 3$ rotation matrix and $t_{e}$ is the $3 \times 1$ translational vector which relate the world coordinate system to the camera coordinate system, and $M_{\text {int }}$ is the $3 \times 3$ camera intrinsic matrix. If we use superscript $P^{C}$ to denote the point in camera coordinate system, then the object point in camera coordinates can be expressed as

$$
\tilde{P}^{C}=\left[\begin{array}{cc}
R_{e} & t_{e}  \tag{6}\\
0^{T} & 1
\end{array}\right] \tilde{P}=M_{e x t} \tilde{P}
$$

The perspective projection model of bi-prism based stereovision system is

$$
\left\{\begin{array}{c}
s \tilde{p}_{l}=M_{\mathrm{int}} M_{L B} M_{e x t} \tilde{P}  \tag{7}\\
s^{\prime} \tilde{p}_{r}=M_{\mathrm{int}} M_{R B} M_{e x t} \tilde{P}
\end{array}\right.
$$

Thus, the projection model of prism based stereovision is the combination of an intrinsic matrix, a scale-translate matrix and a rotate-translate matrix.

## Parameters Estimation

The projection process from an object point to the image plane by prism can be formulated as the combination of an intrinsic matrix, an affine matrix and an extrinsic matrix. Since the intrinsic matrix of the camera can be calculated by single camera calibration, the calibration problem becomes to find the affine matrix and the extrinsic matrix. In Euclidean coordinates, the projection model of bi-prism based stereovision system can be written as

$$
\left\{\begin{array}{c}
s \tilde{p}_{l}=M_{L} \tilde{P}  \tag{8}\\
s^{\prime} \tilde{p}_{r}=M_{R} \tilde{P}
\end{array}\right.
$$

where $M_{L}$ and $M_{R}$ denote the perspective projection transformation of $P$ with left and right views, which can be calculated by normal single camera calibration method, such as Direct Linear Transformation. We decompose the extrinsic matrix and acquire the following equations:

$$
\left\{\begin{array}{l}
H_{L}=M_{\mathrm{int}}^{-1} M_{L}=M_{L B} M_{e x t}  \tag{9}\\
H_{R}=M_{\mathrm{int}}^{-1} M_{R}=M_{R B} M_{e x t}
\end{array}\right.
$$

If we use $N_{r 0}, N_{l 0}$ and $N_{b 0}$ to express the three surface normal of the prism with no offsets, then, the surface normal of the prism can be written as

$$
\left\{\begin{array}{c}
N_{r 0}=(-\sin \theta, 0, \cos \theta)^{T}  \tag{10}\\
N_{l 0}=(\sin \theta, 0, \cos \theta)^{T} \\
N_{b 0}=(0,0,1)^{T}
\end{array}\right.
$$

In most cases, these conditions are hardly achieved in practical applications. There would be some alignment errors and the results would not be accurate if the above assumptions were used. If we use a rotation matrix R to denote the skewing of prism, then the real surface normal of each plane is

$$
\left\{\begin{array}{l}
N_{l}=R N_{l 0}  \tag{11}\\
N_{r}=R N_{r 0} \\
N_{b}=R N_{b 0}
\end{array}\right.
$$

According to Eq. (9), let $E_{R}$ express the first three rows of $H_{R}$, then

$$
\begin{equation*}
E_{R}=A_{R} A_{B} R_{e} \tag{12}
\end{equation*}
$$

It could also be acquired that

$$
\begin{equation*}
E_{R} E_{R}^{T}=\left(A_{R} A_{B} R_{e}\right)\left(A_{R} A_{B} R_{e}\right)^{T}=R A_{R B R} R^{T} \tag{13}
\end{equation*}
$$

Since $R$ is an orthogonal matrix, so $E_{R} E_{R}{ }^{T}$ and $A_{R B R}$ are similar matrices, then they have the same eigenvalue. Let

$$
\left\{\begin{array}{c}
E_{R} E_{R}^{T}=U V U^{T}  \tag{14}\\
A_{R B R}=D V D^{T}
\end{array}\right.
$$

then the rotation matrix R can be solved by

$$
\begin{equation*}
R=U D^{-1} \tag{15}
\end{equation*}
$$

## Experiments and Results

The original and rectified image pairs with different offset of prism were shown in Figure 2 for visual comparison, where (a) was the original image pair, and (b) was the rectified results of the method proposed. The rotation matrix which be calculated from this three system configurations were

$$
R_{\text {sce }}=\left[\begin{array}{ccc}
0.9990 & -0.0392 & 0.0226 \\
0.0365 & 0.9932 & 0.1107 \\
-0.0268 & -0.1098 & 0.9936
\end{array}\right]
$$


(a)

(b)

Fig.2. The experimental results
As shown in these figures, the epipolar lines of original image pairs were misaligned respectively. After rectification all the re-sampled image pairs were properly rectified by the proposed method with minimal geometric distortions.

## Conclusion

Prism based single-lens stereovision systems have many advantages compared with traditional two or more cameras' system. In this research, we presented a new way for calculating the position of prism, which leads to a new approach of projective rectification for stereo images. It can greatly simplify the stereo correspondence search for a bi-prism based single-lens stereovision system.

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