

Making of Free Cutting Austenitic Stainless Steels with Additions of Sulfur, Rare Earth and Bismuth

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Abstract. Making of free cutting austenitic stainless steels with additions of sulfur, rare earth and bismuth were investigated through comparing to the metallurgical properties and machinabilities. The results have shown that free-machining additives exhibit the characteristic shape of spindle shaped sulphides and rounded, globular shaped inclusions. The cutting forces of free cutting austenitic stainless steel were lower than those of an austenite stainless steel 1Cr-18Ni-9Ti at three cutting speeds. The machinability of austenitic stainless steel was visibly improved by adding free-cutting additives, such as sulfur, rare earth and bismuth.

Introduction

In machining metals profound knowledge about the wear behaviour of the cutting tool is essential [1]. Machinability is an important criterion in materials selection and design for many applications [2]. The adhesion properties between work material and tool material in the secondary shear zone are of significant importance both regarding the energy spent in the cutting process and the performance of the cutting process itself [3].

Austenitic stainless steels are generally known to be more demanding to machine than plain carbon steels [3]. There is an important question for the machinist because of its poor machinability [4, 5]. The machinability of the steels can be improved by adding free-machining elements, such as sulfur, lead, selenium, tellurium, etc. [6]. Steelmakers have set out the reduction of environmentally harmful substances such as lead [6].

This paper reports on several aspects of the machinability by adding sulfur, RE (rare earth) and bismuth in two different austenitic stainless steels. Metallurgical properties of free cutting austenitic stainless steels were analyzed. Making of free cutting austenitic stainless steels with additions of sulfur, rare earth and bismuth were investigated through comparing to the metallurgical properties and machinabilities.

Experimental

Materials

The ingots were prepared by using a 150 kg induction vacuum furnace. Specimens were 100 mm diameter rods which were produced by hot forging and solution treating at 1100°C. The tool material was cemented carbide K30 tool containing WC and Co. The chemical composition of specimens for cutting test is given in Table 1.

Table 1 Chemical compositions (wt %) of the experimental steels

Steel	C	Si	Mn	S	P	Ni	Cr	Ti	RE	Bi
A	0.11	0.09	0.50	0.02	0.02	10.15	17.87	0.55	-	-
B	0.09	0.07	1.470	0.12	0.01	9.49	18.34	0.37	0.04	0.11

Machinability test

Cutting tests were performed in a CA6161A lathe under the dry cutting condition. The cutting speed was a range of 120-130 m/min. The feed rate was 0.2 mm/rev, and the depth of cut was 0.5 mm. An optical measuring microscope and a scanning electron microscope (SEM) were used for evaluation of the morphology and quantity of the inclusions.

Results

Microstructures

The inclusions can not be found in steel A. And there are a lot of inclusions in steel B. The shape and size of the inclusions in polished specimen for steel B is shown in Fig. 1. In Fig. 1, free-machining additives exhibit the characteristic shape of punctuation and chain.

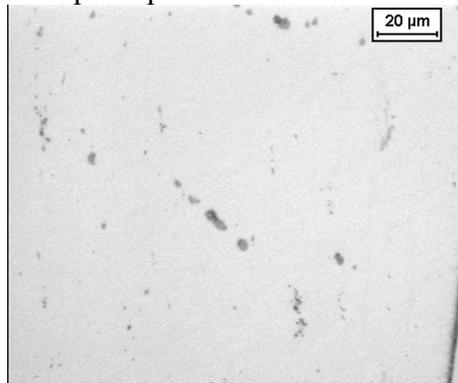


Fig.1 Optical micrographs of steel B

Fig. 2 shows a SEM micrograph of steel B. In Fig. 2, spindle shaped sulphides were observed. Sulphides appear grey. Rounded, globular shaped inclusions should be attributed to the addition of rare earth.

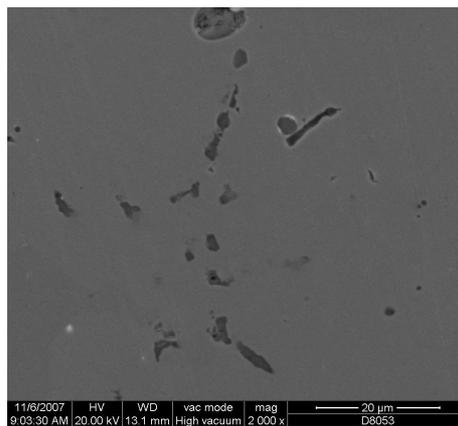


Fig. 2 SEM micrograph of steel B

Machinability

In order to measure the average abrasion depth of the flank of the tool for steel A and B, tool wear for both steels was examined using two new tools keeping the same cutting output at a cutting speed range of 120-130 m/min, feed and depth of cut of 0.2 mm/rev and 0.5 mm, respectively. The results of flank wear tests for both steels are presented in Fig. 3.

In Fig. 3, the tool after turning free cutting Pb-free austenitic stainless steel showed obviously smaller flank wear than that of after turning an austenite stainless steel 1Cr-18Ni-9Ti during 20 min. That is, the progression speed of the tool wear for steel B was less than that of steel A.

Fig. 4 shows the principal force against different speed ratios for both steels. From Fig. 4, it is clear that the cutting forces generally decreased with increasing of cutting speed in the range 50-100 m/min. They were reached 349N and 272N at 50 m/min cutting speed, respectively, for steel A and B. And at

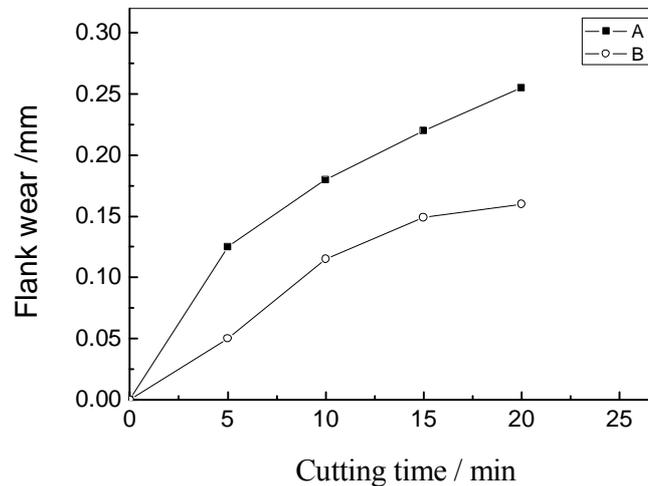


Fig. 3 The flank wear curves of tools for both steels

100 m/min cutting speed, principal force were 343N and 262N, respectively, for steel A and B. It was evident that the cutting forces for free cutting austenitic stainless steel were lower than those of an austenite stainless steel 1Cr-18Ni-9Ti at three cutting speeds.

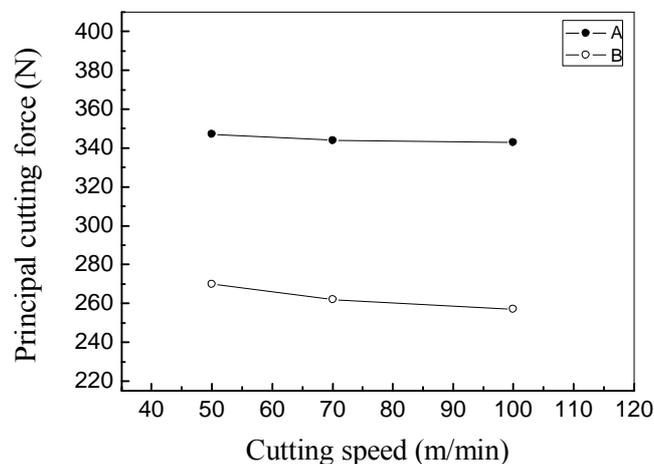


Fig. 4 Effect of cutting speed on principal force

Discussion

A significant aspect in design of cutting tools is cutting forces and should be considered in machining furthermore minimizing cutting forces affect machine component and workpiece distortion [7]. As mentioned above, the cutting forces for steel B were lower than those of steel A at three cutting speeds (Fig. 4). That is, Tool life for free cutting austenitic stainless steel was superior to that of an austenite stainless steel 1Cr-18Ni-9Ti (Fig. 3). However, Patra and his co-workers [8] found that there are only minor effects from cutting speed, square of cutting speed, square of feed and product of speed, and feed on the cutting forces. Controlled oxide inclusions contribute to the improvement of the

machinability of austenitic stainless steels. It is expedient to add various free-machining elements, such as sulfur, rare earth and bismuth in the steel. A lot of oval inclusions were found in the surface of the specimen (Figs. 1, 2).

The inclusions are mainly composed of MnS (Figs. 1, 2). The beneficial effect of sulphur on machinability has been known now for over one hundred years. Manganese sulfide inclusion in the steel results in the formation of MnS films on the rake faces of the tools, and cutting force decreases because of the lubricating action of the MnS film. Sulphides are very beneficial to machining. Sulfur forms manganese sulfide, which at a certain size of the inclusions facilitates shearing and easy detachment of turnings.

RE element is also an important one because it can improve the machinability of austenitic stainless steels. Rare earth elements include 15 elements in the Periodic Table, also known as lanthanides, plus yttrium (Y) and scandium (Sc), that share chemical properties related to a similar external electronic configuration [Effect of some rare earth elements on the growth and lanthanide accumulation in different *Trichoderma* strains]. The S-RE-Ca system free-cutting steel exhibited the best machinability at high cutting speeds. Therefore, the S-RE system free-cutting steel had better machinability than the others in the low cutting speed range.

The addition of bismuth is a key element. It is well known that the leaded steel is currently the most common. However, lead is considered to enhance the machinability with some adverse environmental effects. Bismuth can also improve machinability of steels because it is a soft metal, like lead, with a low melting point, has a very limited solubility in solid iron, and like tellurium, is known to segregate readily to surfaces and cause embrittlement. It is considered to be distinct advantage over lead.

Conclusions

(1) A lot of inclusions in steel were observed in free cutting austenitic stainless steel. free-machining additives exhibit the characteristic shape of spindle shaped sulphides and rounded, globular shaped inclusions.

(2) The cutting forces for free cutting austenitic stainless steel were lower than those of an austenite stainless steel 1Cr-18Ni-9Ti at three cutting speeds. The machinability of austenitic stainless steel was visibly improved by adding free-cutting additives, such as sulfur, rare earth and bismuth.

(3) Sulphides are very beneficial to machining. The RE elements improved the machinability of austenitic stainless steel. The addition of bismuth is a key element for improving machining characteristics of austenitic stainless steels.

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