

Vanadium Extraction from Molten Vanadium Slag with High Ca and P Contents by Direct Oxidation-acid Leaching Method

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ABSTRACT: A novel method of extracting vanadium from molten vanadium slag was developed to process vanadium slag with high Ca and P contents. The mineral phases of the clinker obtained after oxidizing the molten vanadium slag with high Ca and P contents (10.71 wt. % V_2O_3 , 19.20 wt. % CaO, 1.03 wt. % P_2O_5) were analyzed by X-ray diffraction (XRD) to fully comprehend the compositions of the clinker. The leaching conditions of extracting vanadium from the clinker and the kinetics during the leaching process were also investigated in this paper in order to obtain a better leaching rate of vanadium. The results indicate that most of V in the clinker exists in the form of calcium orthovanadate ($Ca_3V_2O_8$), and the rest turns into the vanadate with low valence state of V. Silicates mainly include pyroxene ($Ca(Mg/Fe/Ca)Si_2O_6$), calcium silicoaluminate ($CaAl_2Si_2O_8$) and calcium orthosilicate (Ca_2SiO_4). P exists in the form of calcium phosphate ($Ca_3(PO_4)_2$). The leaching rate of vanadium can reach 95% under the conditions: sulfuric acid concentration of 15%, liquid to solid ratio of 5:1 mL/g, leaching temperature of 90°C, leaching time of 40 min, stirring rate of 240 r/min. Kinetic analysis results show that the acid leaching process of the clinker can be well interpreted by the unreacted shrinking core model under internal diffusion control, and the apparent activation energy is 8.36 kJ/mol.

KEYWORD: Molten vanadium slag with high Ca and P contents; vanadium extraction; phase; leaching; kinetics

1 INTRODUCTION

At present, vanadium extraction from vanadium containing hot metal is mainly accomplished in the converter process in China (Fu, 2011). During the process, vanadium is oxidized and enriched in the slag. After that, semi-steel and vanadium slag are obtained, then the vanadium slag as raw materials for vanadium extraction is processed through hydrometallurgical method to recover vanadium. At the end of the converter process, an acid slag system with complicated multi-component is formed (Zhang et al., 2011), which is not favorable for dephosphorization from vanadium containing hot metal. In addition, the work of removing phosphorus also could not be finished effectively during the following semi-steel blowing process (Dong, 1997). In order to settle this problem, a method of adding CaO containing materials to form basic slag to extract vanadium and remove phosphorus simultaneously from vanadium containing hot metal is put forward, and a better outcome of phosphorus removal in the previous experiment has been achieved. In this case, a new kind of vanadium slag

that contains more CaO and P_2O_5 contents is obtained, and such type slag is defined as vanadium slag with high Ca and P contents for the following discussion.

The V_2O_3 content in the vanadium slag with high Ca and P is generally 9.0 wt. %~13.0 wt. %, between the content in the original vanadium slag (15.0 wt. %~20.0 wt. %) and that in the vanadium bearing steel slag (about 3.0 wt. %). The CaO and P_2O_5 contents in the vanadium slag with high Ca and P are approximately 8.0 wt. %~28.0 wt. % and 0.6 wt. %~1.3 wt. %, respectively, and much higher than their contents in the original vanadium slag (3.0 wt. % CaO and 0.2 wt. % P_2O_5). “A method of dealing with vanadium slag with energy conservation and emission reduction” was proposed by University of Science and Technology Beijing (Li et al., 2012; Song et al., 2013, 2014; Li et al., 2013) considering the fact that the current roasting process for vanadium extraction is not suitable for dealing with such type vanadium slag. The main phases of the clinker and the acid leaching conditions of vanadium extraction were investigated, and the kinetics analysis was also performed in this paper

2 EXPERIMENTAL

The vanadium slag with high CaO and P contents was prepared by mixing the original slag and analytical reagents of CaO and P₂O₅. The chemical

composition, which is listed in Table 1, was determined by the slag composition acquired from the previous experiments.

Table 1. Chemical composition of vanadium slag with high Ca and P contents wt. %.

V ₂ O ₅	CaO	SiO ₂	FeO	TiO ₂	MnO	Al ₂ O ₃	MgO	P ₂ O ₅	else
10.71	19.20	12.80	30.06	10.03	7.47	2.55	2.50	1.03	3.65

It was found from the preliminary experiments that the slag melted when the temperature approached 1400°C. Hence, the temperature of 1400°C was selected as the beginning temperature of blowing oxygen. The experiment was conducted in a vertical high-temperature furnace. Before heating, 80 g of synthetic slag materials were kept in an alumina crucible and placed at the center of the furnace. The slag materials were heated to 1400°C over a period of time. Then, the temperature was held for 5 min before turning off the power. After that, oxygen was blown immediately into the molten slag at a flow rate of 2 L/min through a quartz tube (outer diameter: 8 mm, inner diameter: 4 mm). The quartz tube was near but above the slag surface, and oxygen blowing was lasted for 20 min. The clinker was cooled to the room temperature in the furnace.

The clinker was crushed and ground to < 0.074 mm. Some of them were used for XRD analysis, and the rest were applied for acid leaching. During the leaching process, the slurry was separated via vacuum filtration, and the residues were washed several times by distilled water. All the filtrates were merged. The potassium permanganate oxidation-ammonium ferrous sulfate titration method was used to measure the concentration of vanadium in the filtrate (YB/T 5328-2006, 2006). The leaching rate of vanadium is expressed as equation (1).

$$\eta_V = m_1/m \times 100 \quad (1)$$

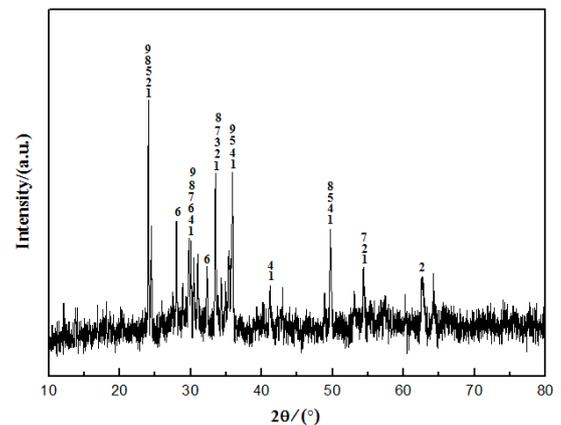
Where η_V is the leaching rate of vanadium, %; m_1 is vanadium content in the filtrate, g; m is vanadium content in the vanadium slag clinker, g.

3 RESULTS AND DISCUSSION

3.1 Mineral phase analysis of the clinker of vanadium slag with high Ca and P contents

As shown in Figure 1, the phases of the clinker mainly include vanadates, silicates, phosphates, titanates and ferric oxides. Most of V exists in the form of Ca₃V₂O₈, and the rest turns into Ca_{0.17}V₂O₅ and CaV₂O₅. Silicates have many types, mainly including pyroxene phase (Ca(Mg/Fe/Ca)Si₂O₆), calcium silicoaluminate phase (CaAl₂Si₂O₈) and calcium orthosilicate phase (Ca₂SiO₄). Some of them crystalize later, and the crystal shape is restricted by

the space. So, the silicate phases present an irregular particle shape filling the space between other phases and even enwrap other phases. In the subsequent leaching process, those silicates can react with the acid to form colloids which prevent vanadium leaching and result in vanadium loss (Li et al., 2011, 2012; Bie et al., 2010). P in the clinker exists in the form of Ca₃(PO₄)₂. Thus, P can dissolve into the filtrate together with V in the leaching process, which can have a disadvantage to purification.



1-Fe₂O₃; 2-Fe₉TiO₁₅; 3-Ca₃(PO₄)₂; 4-Ca(Mg/Fe/Ca)Si₂O₆; 5-CaAl₂Si₂O₈; 6- Ca₂SiO₄; 7-Ca₃V₂O₈; 8- CaV₂O₅; 9- Ca_{0.17}V₂O₅

Figure 1. XRD patterns of the clinker.

3.2 Effect of acid leaching conditions on vanadium extraction

3.2.1 Effect of sulfuric acid concentration

Calcium vanadate is hardly soluble in water, but it can be easily dissolved in dilute acid. Sulfuric acid is generally chosen as the leaching agent. The leaching conditions are presented in Figure 2. It is apparent that η_V increases significantly when the sulfuric acid concentration increases ranging from 5% to 15%. η_V tends to be slightly changed when the sulfuric acid concentration is higher than 15%. Under the circumstance of keeping the ratio of liquid to solid constant, higher acid concentration means more H⁺ reacting with calcium vanadate, which facilitates vanadium dissolution. However, when the sulfuric acid concentration is too high, excess H⁺ can react with some undesired substances, leading more impurities into the leach liquor, which is detrimental

to purification. Therefore, the sulfuric acid concentration of 15% is chosen for further studies.

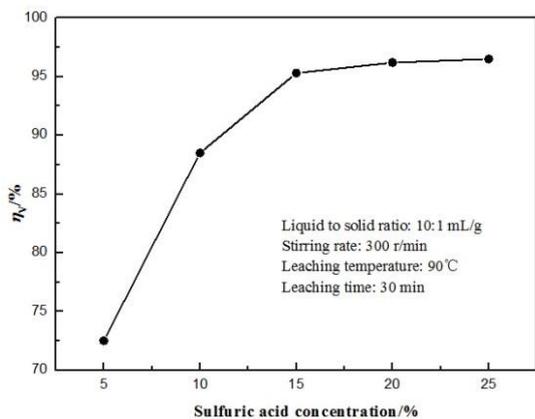


Figure 2. Effect of sulfuric acid concentration on η_V .

3.2.2 Effect of liquid to solid ratio

The relation between η_V and liquid to solid ratio and the leaching conditions are all illustrated in Figure 3. A small liquid to solid ratio will lead to a result that the amount of H^+ is insufficient to fully dissolve calcium vanadate on the condition that the acid concentration is invariant. Besides, the viscosity of the leach liquor becomes high due to the small liquid to solid ratio, which will give rise to a great resistance to the external diffusion of soluble vanadium. Both of them can cause the reduction of η_V . Figure 3 reveals that η_V increases rapidly when the liquid to solid ratio is varied from 2:1 mL/g to 5:1 mL/g, but η_V has no obvious change with a further increase in the liquid to solid ratio. In addition, a high liquid to solid ratio can dilute the concentration of vanadium, which generates adverse effects on precipitation of vanadium. The liquid to solid ratio is commonly controlled at (3~5):1 mL/g in practice production. Considering the discussion above, the ratio of 5:1 mL/g is recommended for the following experiments.

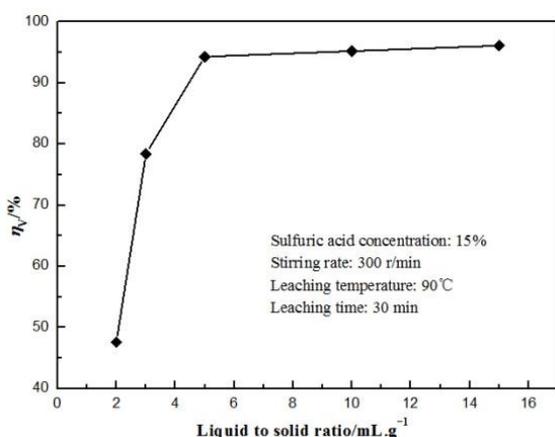


Figure 3. Effect of liquid to solid ratio on η_V .

3.2.3 Effect of leaching temperature

The results shown in Figure 4 suggest that η_V increases with an increase in the leaching

temperature. One of the reasons is that high temperature can improve the reaction rate. The other is the viscosity of the leach liquor becomes low at high temperature, which can accelerate the diffusion of vanadium. Therefore, the leaching temperature should be as high as possible in practice. But η_V negligibly increases with the leaching temperature exceeding 90°C, furthermore, water is evaporated severely. Hence, 90°C is the choice of the leaching temperature.

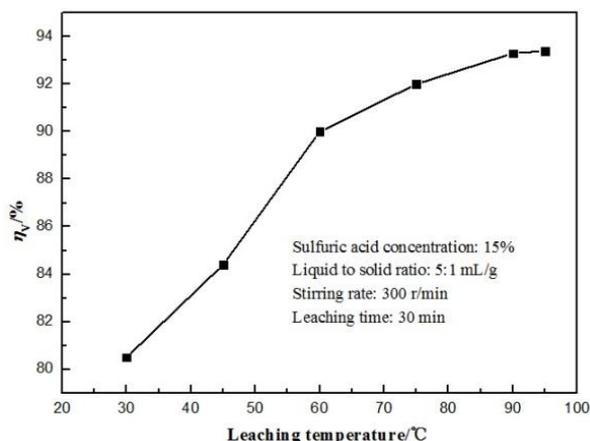


Figure 4. Effect of leaching temperature on η_V .

3.2.4 Effect of leaching time

Figure 5 demonstrates that η_V markedly increases with the leaching time from 5 min up to 40 min. This is because prolonging the leaching time can be of benefit for complete reactions and diffusions occurring in the leaching process. But, with a longer leaching time, η_V barely changes observed from Figure 5. So 40 min is selected as the leaching time.

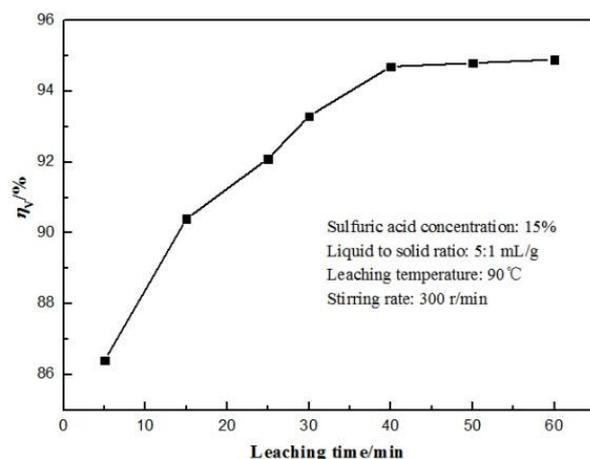


Figure 5. Effect of leaching time on η_V .

3.2.5 Effect of stirring rate

It can be observed from Figure 6 that increasing the stirring rate is beneficial for η_V . Because stirring can decrease the thickness of the liquid layer on the surface of vanadium slag particle so as to diminish the diffusion resistance. η_V nearly increases by 17% when the stirring rate is varied from 0 r/min to 240 r/min, but η_V has slight increase with the stirring rate

above 240 r/min. Thus, the optimum stirring rate under the leaching conditions presented in Figure 6 is 240 r/min.

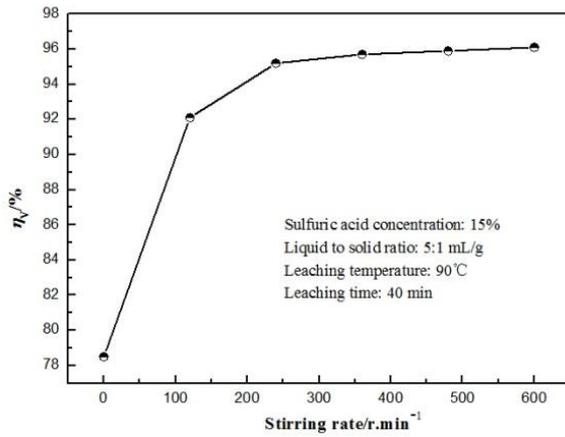


Figure 6. Effect of stirring rate on η_V .

In summary, the leaching rate of vanadium η_V can reach up to 95% under the optimum leaching conditions: sulfuric acid concentration 15%, liquid to solid ratio 5:1 mL/g, leaching temperature 90°C, leaching time 40 min, stirring rate 240 r/min.

3.3 Kinetic analysis of leaching process

The reactions occurring in the acid leaching process of vanadium slag belong to the typical solid-liquid reaction with a solid product layer formed. The leaching process can be interpreted by the unreacted shrinking core model under the assumption that vanadium slag particle is homogeneously spherical solid phase (Liu et al., 2013). Three established rate-controlling steps are usually used, and the according equations are expressed as follows (Li, 2005; Yang and Qiu, 1998).

1) Surface reaction control

$$1 - (1 - \eta_V)^{1/3} = k_1 t \quad (2)$$

2) Internal diffusion control (Solid product layer control)

$$1 - 2/3\eta_V - (1 - \eta_V)^{2/3} = k_2 t \quad (3)$$

3) External diffusion control (Liquid boundary layer diffusion control)

$$\eta_V = k_3 t \quad (4)$$

Where k_1 , k_2 and k_3 are the rate constants, min^{-1} ; t is the leaching time, min.

In order to determine the controlling step in the leaching process of vanadium slag, the data of η_V at different leaching temperatures were fitted using equations (2), (3) and (4), and the corresponding results are given in Figure 7, Figure 8 and Figure 9, respectively. The slopes of the fitted lines are the numerical values of k_1 , k_2 , k_3 , respectively, as shown in Table 2.

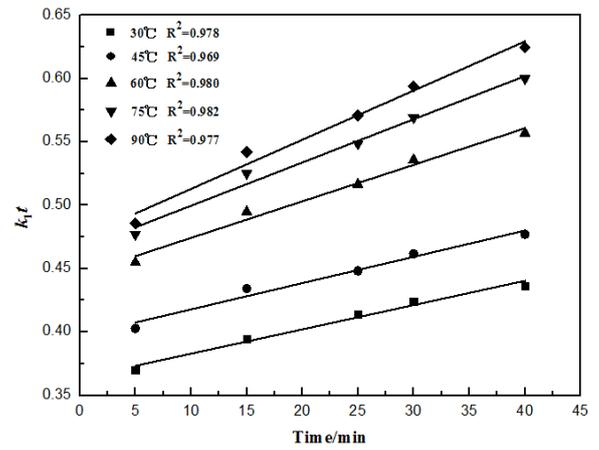


Figure 7. Fitted results of η_V data by equation of surface reaction control at different temperatures.

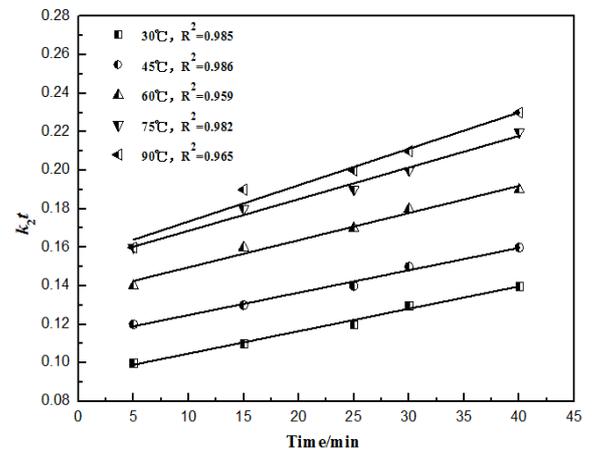


Figure 8. Fitted results of η_V data by equation of internal diffusion control at different temperatures.

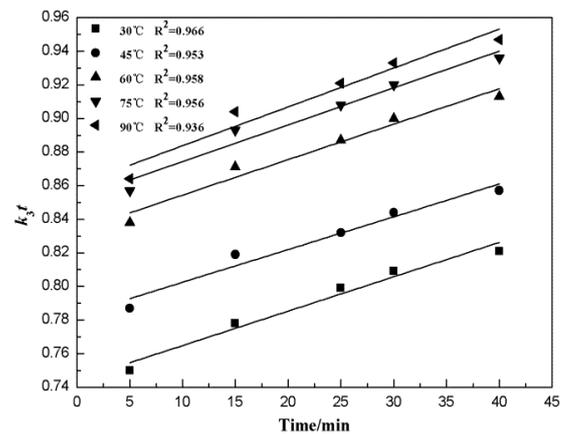


Figure 9 Fitted results of η_V data by equation of external diffusion control at different temperatures

The apparent activation energy can be calculated based on the Arrhenius equation which is expressed as follow. The relation between natural logarithm of the rate constant ($\ln k$) and the leaching temperature (T) is obtained as a function of Table 2, as plotted in Figure 10.

$$\ln k = \ln A - Ea/RT \quad (5)$$

Where k is the rate constant; A is the pre-exponential factor; E_a is the apparent activation

energy, J/mol; R is the molar gas constant, J/(mol K); T is the leaching temperature, K.

Table 2. Results of k_1 , k_2 , k_3 and $\ln k_1$, $\ln k_2$, $\ln k_3$.

$1/T \times 10^3 / K^{-1}$	k_1	$\ln k_1$	k_2	$\ln k_2$	k_3	$\ln k_3$
3.300	0.0019	-6.266	0.0011	-6.812	0.0021	-6.166
3.145	0.0021	-6.166	0.0012	-6.725	0.0020	-6.215
3.003	0.0029	-5.843	0.0014	-6.571	0.0021	-6.166
2.874	0.0034	-5.684	0.0016	-6.438	0.0022	-6.119
2.755	0.0039	-5.547	0.0019	-6.266	0.0023	-6.075

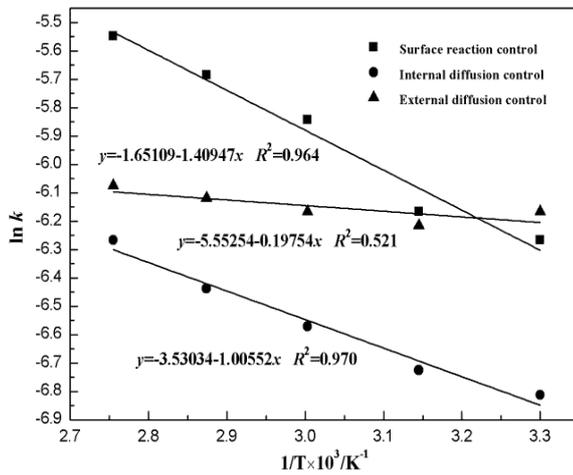


Figure 10. The relation between $\ln k$ and T .

It can be calculated from Figure 10 that the apparent activation energies are 11.72kJ/mol, 8.36kJ/mol and 1.64kJ/mol when the rate-controlling steps are surface reaction step, internal diffusion step and external diffusion step, respectively. However, the apparent activation energy should be greater than 41.8 kJ/mol when surface reaction step is the rate-controlling step, and the apparent activation energy should be 4~12 kJ/mol when diffusion step is the rate-controlling step. Therefore, the possibilities that the rate-controlling step is surface reaction step or external diffusion step are excluded. In view of the discussion above, the rate-controlling step in the acid leaching process of vanadium slag is internal diffusion, and the apparent activation energy is 8.36 kJ/mol.

4 CONCLUSIONS

The main mineral phases of the clinker of vanadium slag with high Ca and P contents include vanadates, silicates, phosphates, titanates and ferric oxides. Most of V exists in the form of $Ca_3V_2O_8$, the rest changes into $Ca_{0.17}V_2O_5$ and CaV_2O_5 . Silicate phases mainly consist of pyroxene, calcium silicoaluminate and calcium orthosilicate, some of which will prevent vanadium leaching and result in vanadium loss in the subsequent leaching process. P in the clinker exists in the form of $Ca_3(PO_4)_2$, so P can

dissolve into the filtrate with V and generate a disadvantage to purification. The leaching rate of vanadium can reach up to 95% under the optimum leaching conditions: sulfuric acid concentration 15%, liquid to solid ratio 5:1mL/g, leaching temperature 90°C, leaching time 40min, stirring rate 240r/min. The rate-controlling step in the acid leaching process of vanadium slag is internal diffusion, and the corresponding apparent activation energy is 8.36kJ/mol.

5 ACKNOWLEDGMENTS

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REFERENCES

- [1] Bie, S., Wang, Z.J., Li, Q.H., Zhang, Y.G. 2010. Review of vanadium extraction from stone coal by roasting technique with sodium chloride and calcium oxide. *Chinese Journal of Rare Metals* 34(2): 291-297.
- [2] Dong, P.Q. 1997. Current situation of the converter semi-steel steelmaking technology in China. *Steelmaking* 13(2): 62-64.
- [3] Fu, Z.B. 2011. Development process and trends of vanadium extraction from vanadium-titanium magnetite ore. *China Nonferrous Metallurgy* 40(6): 29-33.
- [4] Li, H., Song, W.C., Niu, S.T., Niu, S.Z., Guo, L.F. 2012. A method of dealing with vanadium slag with energy conservation and emission reduction. Chinese Patent (ZL201110044380 .5).
- [5] Li, H.G. 2005. *Hydrometallurgy*. Changsha: Central South University Press, 74.
- [6] Li, K., Song, W.C., Zheng, Q., Li, H. 2013. Vanadium extraction by acid leaching after calcification of molten vanadium slag. *Iron Steel Vanadium Titanium* 34(5): 15-18.
- [7] Li, X.J., Xie, B., Diao, J., Zhang, C.Y., Wang, Y.H. 2011. Kinetic of isothermal growth of spinel in vanadium slag. *Chinese Journal of Rare Metals* 35(2): 281-285.
- [8] Li, X.J., Zhang, R.P., Xie, B. 2012. Effect of vanadium-containing slag calcium roasting conditions on leaching rate of vanadium. *The Chinese Journal of Process Engineering* 12(1): 54-58.

- [9] Liu, H.B., Du, H., Wang, D.W., Wang, S.N., Zheng, S.L., Zhang, Y. 2013. Kinetics analysis of decomposition of vanadium slag by KOH sub-molten salt method. *Transactions of Nonferrous Metals Society of China* 23(5): 1489-1500.
- [10] Song, W.C., Li, H., Li, K., Zheng, Q. 2013. New process of vanadium extraction from molten vanadium slag. *Nonferrous Metals (Extractive Metallurgy)* (7): 35-37.
- [11] Song, W.C., Li, K., Zheng, Q., Li, H. 2014. A novel process of vanadium extraction from molten vanadium bearing slag. *Waste and Biomass Valorization* 5(3): 327-332.
- [12] Yang, X.W., Qiu, D.F. 1988. *Hydrometallurgy*. Beijing: Metallurgical Industry Press, 174.
- [13] YB/T 5328-2006. 2006. *The potassium permanganate oxidation-ammonium ferrous sulfate titrimetric method for the determination of vanadium pentoxide content*. Beijing: Standards Press of China.
- [14] Zhang, Y.L., Zhao, F., Wang, Y.G. 2011. Effects of influencing factors on distribution behaviors of vanadium between hot metal and FeO-SiO₂-MgO (-TiO₂) slag system. *Steel Research International* 82(8): 940-950.