

Analysis on the Coupled System of Vibratory Roller Vibration Wheel and Soil

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Key Words: vibratory roller; wheel vibration; amplitude;

Abstract: In this paper, the intelligent vibration road roller system is simplified to three degrees of freedom dynamic system, the differences between the dynamics model with past is that we not only considering two degrees (vibration wheel, the soil or frame, wheels), But at the same time considering vibratory wheel, frame and the soil under the interaction of three degree of freedom vibration. In this text, Vibratory roller vibration system is mainly studied in the vertical direction vibration, by solving equations, obtaining the expression of the wheel vibration amplitude, the relationship between wheel vibration amplitude and the various soil parameters are studied by using numerical analysis method, the influence of various parameters on the amplitude is discussed. The results show that the parameters of soil have different degrees of influence on amplitude. Among them, the soil stiffness has the most effect on the amplitude. The results can provide the reference data for vibration system design and the real-time monitoring, control of the vibration response.

Introduction

From the early 1940s, the birth of the first self-propelled roller to the present, the vibratory roller has great changes in form and function, vibratory roller entered a new period of development. Intelligent vibratory roller becomes the new trend of development [1]. The amplitude of vibratory roller is the amount of roller wheel to move up and down, for compaction depth requirements of soil, the more amplitude of the roller, the more the quality of the material in vibration, increasing compaction influence depth or thickness [2-5]. consider only two degrees of freedom is the case in the past, In this paper, the intelligent vibration road roller system is simplified to three degrees of freedom dynamic system, but at the same time considering vibratory wheel, frame and the soil. Vibratory roller vibration system is mainly studied in the vertical direction vibration, by solving equations, obtaining the expression of the wheel vibration amplitude, the relationship between wheel vibration amplitude and the various soil parameters are studied by using numerical analysis method, the influence of various parameters on the amplitude is discussed. To provide the reference for the realization of intelligent control of roller design.

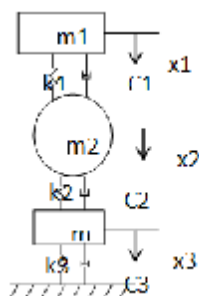


Fig. 1 the system dynamics model diagram

Formulation and solution of the coupled system of vibratory roller-vibration wheel and soil

Roller vibration system is mainly studied in the vertical direction vibration, roller-vibratory wheel-soil the system dynamics model diagram is shown in figure 1.

Vibration wheel and eccentric mass and main structure along the longitudinal axis symmetric, so system vibration model can be simplified as plane dynamic problems; The vibration of the vibrating road roller wheel, the quality of the frame is simplified to concentrated mass respectively, soil compaction, vibration wheel and frame together as a quality - spring - damper system, ignore the quality of spring and damping; Assuming that the soil is a certain stiffness of the elastomer, the roller's rigidity and damping and soil stiffness and damping into consideration; Only consider the degrees of freedom vertical direction vibration of the vibration wheel, and ignore the rotational degree of freedom. vibration wheel of Vibratory roller keep contact with the ground at any moment.

Fig.1

m_1 , m_2 , m_3 —the quality of the roller on the frame, the quality of the vibration and the soil;

c_1 , c_2 , c_3 —On the frame of vertical damping, vertical wheel and soil vertical damping;

k_1 , k_2 , k_3 —On the frame of vertical stiffness, Vibration wheel and soil vertical stiffness.

Vibration system dynamics model is shown in type (1).

$$\begin{cases} m_3 \ddot{x}_3 + (c_2 + c_3) \dot{x}_3 - c_2 \dot{x}_2 + (k_2 + k_3)x_3 - k_2 x_2 = 0 \\ m_2 \ddot{x}_2 + (c_1 + c_2) \dot{x}_2 - c_2 \dot{x}_3 - c_1 \dot{x}_1 + (k_1 + k_2)x_2 - k_2 x_3 - k_1 x_1 = -F_0 \sin wt \\ m_1 \ddot{x}_1 + c_1 \dot{x}_1 - c_1 \dot{x}_2 + k_1 x_1 - k_1 x_2 = 0 \end{cases} \quad (1)$$

$$\text{Among: } [k] = \begin{bmatrix} k_2 + k_3 & -k_2 & 0 \\ -k_2 & k_1 + k_2 & -k_1 \\ 0 & -k_1 & k_1 \end{bmatrix} \quad [c] = \begin{bmatrix} c_2 + c_3 & -c_2 & 0 \\ -c_2 & c_1 + c_2 & -c_1 \\ 0 & -c_1 & c_1 \end{bmatrix} \quad [x] = \begin{bmatrix} x_3 \\ x_2 \\ x_1 \end{bmatrix}$$

$$[F] = \begin{bmatrix} 0 \\ -F_0 \sin wt \\ 0 \end{bmatrix} \quad [m] = \begin{bmatrix} m_3 & 0 & 0 \\ 0 & m_2 & 0 \\ 0 & 0 & m_1 \end{bmatrix}$$

Because the model is a linear time invariant system, incentive is the resonant force, so the steady state response is also resonant displacement. For solving the dynamic equation (1), Use the plural vector representation, $F_0 e^{iwt}$ is vibration force, $x_1 = A_1 e^{i(wt-a_1)}$, $x_2 = A_2 e^{i(wt-a_2)}$, $x_3 = A_3 e^{i(wt-a_3)}$

A_1 , A_2 , A_3 —the amplitude of instantaneous displacement x_1 , x_2 , x_3 ;

a_1 , a_2 , a_3 — phase Angle of instantaneous displacement x_1 , x_2 , x_3 behind the exciting force F

Take $\dot{x}_1 = iw x_1$, $\ddot{x}_1 = -w^2 x_1$; $\dot{x}_2 = iw x_2$, $\ddot{x}_2 = -w^2 x_2$; $\dot{x}_3 = iw x_3$, $\ddot{x}_3 = -w^2 x_3$ to type (1):

$$\begin{aligned} [-m_3 w^2 + iw(c_2 + c_3) + k_2 + k_3] x_3 + (-iwc_2 - k_2) x_2 &= 0 \\ (-iwc_2 - k_2) x_3 + [-m_2 w^2 + iw(c_1 + c_2) + k_1 + k_2] x_2 + (-iwc_1 - k_1) x_1 &= -F_0 e^{iwt} \\ (-iwc_1 - k_1) x_2 + (-m_1 w^2 + iwc_1 + k_1) x_1 &= 0 \end{aligned} \quad (2)$$

Among, $M = [-m_3 w^2 + iw(c_2 + c_3) + k_2 + k_3]$, $N = (-iwc_2 - k_2)$, $P = (-iwc_2 - k_2)$

$Q = [-m_2 w^2 + iw(c_1 + c_2) + k_1 + k_2]$, $R = (-iwc_1 - k_1)$, $Z = (-iwc_1 - k_1)$,

$G = (-m_1 w^2 + iwc_1 + k_1)$

$x_2 = A_2 e^{i(wt-a_2)} = F_0 e^{iwt} \text{MGQ}/(\text{PNGQ}-Q^2\text{MG}+\text{ZRMQ})$

$A_2 e^{-ia_2} = F_0 \text{MGQ}/(\text{PNGQ}-Q^2\text{MG}+\text{ZRMQ}) = F_0 (a + bi) / (c + di)$

Among: $F_0 = w^2 M e$, $A_2 = F_0 \sqrt{(a^2 + b^2) / (c^2 + d^2)}$

This shows the vibration amplitude of dynamics model is the function of vibration parameters in the vibration system, to study the influence of dynamic model input parameters on the vibration response, on the basis of reference literatures and the performance of the vibrating road roller, The system related to the input parameter generation into the system response function, obtain corresponding relation curve through numerical calculation, discuss the system main input parameters effect on the output parameters of the system.

Numerical calculation and analysis

By the response type(2) about the dynamic model of the frame- vibratory wheel- soil, we know, in the system of vibration compaction, output parameters and input parameters of the dynamic model is a nonlinear relationship.By setting a single change of input parameters, and the rest of the input parameters as constant value, through numerical analysis the influence law of system stiffness, damping and vibration with the soil quality of vibration, the vibration frequency or exciting force on the system response, get on the frame -vibration wheel - soil vibration compaction system input parameters and the relationship between the wheel vibration amplitude.

According to the common vibrating road roller design data and the related literature to determine the parameters: $k_s = 1.5 \times 10^7 \text{ N/m}$, $c_s = 7.2 \times 10^4 \text{ Ns/m}$, $m_1 = 1500 \text{ kg}$, $m_2 = 3000 \text{ kg}$, $m_3 = 1800 \text{ kg}$, $w = 1500 \text{ r/min}$, $Me = 5 \text{ kgm}$; And take $c_1 = c/6$, $c_2 = c/2$, $c_3 = c/3$, $k_1 = k/6$, $k_2 = k/2$, $k_3 = k/3$

Take m_1 , m_2 , m_3 , k_1 , k_2 , k_3 , c_1 , c_2 , w to type (2), obtain expression of vibratory roller wheel vibration amplitude about c_3 , To study wheel vibration amplitude changes, When the soil damping change from 0.1 c (1200 ns/m) to c (12000 ns/m), c (12000 ns/m) to 10 c (120000 ns/m). According to the above numerical results, amplitude A on soil parameters k, c, m are obtained by Matlab software and vibration wheel vibration frequency of a series of functional relation curve as shown in the figure below(K is the distribution stiffness of soil ,c is the distribution of soil damping coefficient, M is the study of soil quality ,W is the vibration wheel vibration frequency).

In the figure 2, amplitude about damping reduce from 1.678 mm to 1.678 mm between 0.1 c (1200 ns/m) and c (12000 ns/m), Figure 3 reflects the amplitude about damping reduce from 1.662 mm to 1.33 mm between c (12000 ns/m) and 10 c (120000 ns/m).

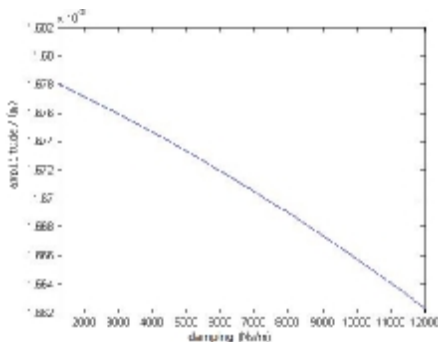


Fig.2 function relation curve of damping(0.1c-c)

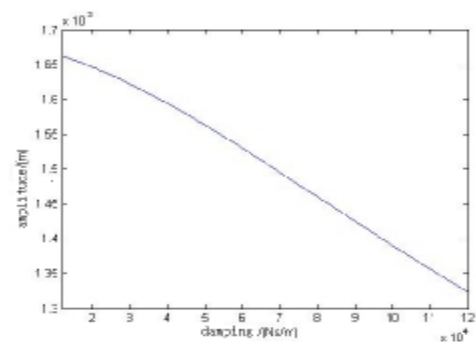


Fig.3 function relation curve of damping(c-10c) about amplitude

In the figure 4, amplitude is the state of the curve between 0.1 k (250000 n/m) and k (2500000 n/m), increase from 0.781 mm to 0.781.

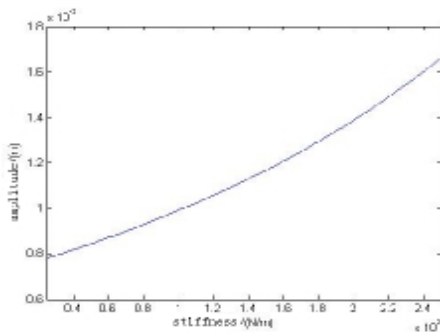


Fig.4 function relation curve of stiffness (0.1k-k)

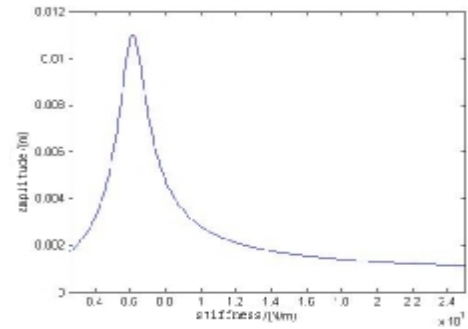


Fig.5 function relation curve of stiffness (k-10k) about amplitude

Figure 6 is the curve of amplitude about quality between 0.1 m (180 kg) and m (1800 kg), reduce from 2.52 mm to 1.662 mm .Figure 7 is the amplitude (1800 kg) about quality from 1m to 10 m (18000 kg), from 1.662 mm to tending to zero, and then slowly increase.

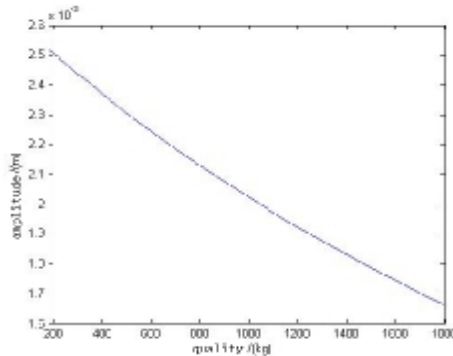


Fig.6 function relation curve of quality (0.1m-m)

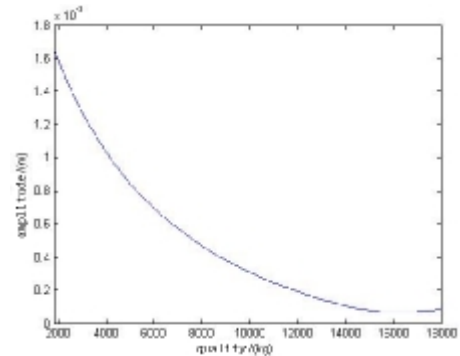


Fig.7 function relation curve of quality (m-10m) about amplitude

Figure 8, the amplitude increase sharply with the increase of w , amplitude is equal to maximum 9.6 mm when the frequency is 18 r/s .Amplitude sharply reduce with the increase of frequency, reach a minimum value, then the curve increases sharply, amplitude is equal to maximum 105.9 r/s when frequency is 2.32 mm.

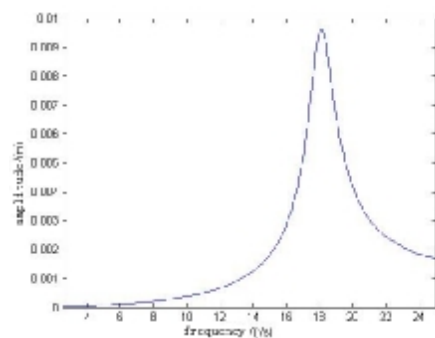


Fig.8 function relation curve of frequency(0.1w-w).

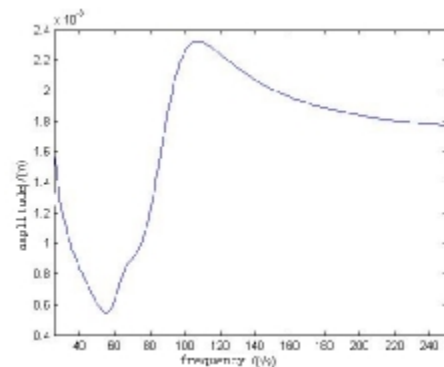


Fig.9 function relation curve of frequency (w-10w)about amplitude

Conclusion

DuringVibration roller compaction,when Soil quality is 200 kg, the compaction effect is best; to the natural frequency of soil, wheel vibration amplitude is the largest, the compaction effect is best.

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