

Dynamic corrosion of refractories by Na_2CO_3

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Keywords: dynamics, refractories, Na_2CO_3

Abstract. The corrosion of refractories by Na_2CO_3 at high temperature has become a severe issue. For a better understanding of corrosion mechanisms, this paper works out the kinetics mechanism of corrosion reaction including characteristic parameters and dynamics equation. The results provide the theoretical basis of sodium carbonate corrosion on refractories and give an evidence of the direction of corrosion resistance of refractories .

Introduction

Refractories are widely used in industries such as iron and steel, cement, and so on. However, there are severe corrosion in boilers. Therefore the scholars have studied in resistance of various refractory materials to corrosion, in order to solve the problem of corrosion.

Many researches show that refractories containing Cr_2O_3 have excellent performance in resistance to slag corrosion. Firstly, Cr_2O_3 has smaller solubility in the slag and could increase the viscosity of the molten slag, resulting in reducing chemical erosion of refractory. Secondly, increase of viscosity reduced the permeability and wettability of refractory materials and the formation of the metamorphic layer, thereby reducing flake refractory materials' structure. Refractory materials containing Cr_2O_3 have better performance among the basic refractory materials. But in waste incineration boiler alkali metal salts can cause severe corrosion in refractories, in addition, refractories were more prone to mechanical damage in high temperature, so that the service life of refractory material might be shorten and great hidden danger and economic losses might be happened.

Experimental

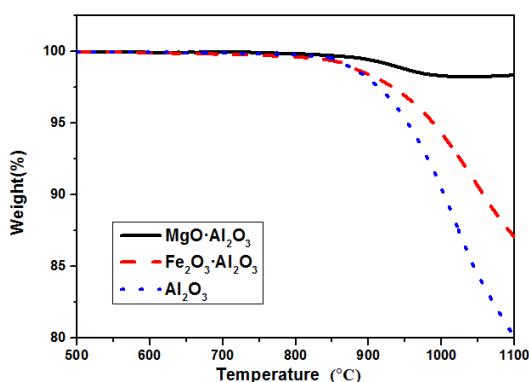
In order to have a better understanding of chromium refractory corrosion by Na_2CO_3 , this paper studies the dynamic corrosion. Synchronous thermal analyzer (SDT) of the TA instrument company is provided for the experimental and its type is SDT-Q600. The samples will be analyzed with differential scanning calorimetry (DSC) and thermogravimetric analysis (TGA) at the same time. Its test temperature range from room temperature to 1500 °C and its measurable parameters include material internal change, heat flux, weight change. Raw materials are reacted at the ratio of 1:1 and the heating rate of 30°C / min.

For isothermal reaction, the reaction rate is only a function of time under the certain reaction conditions. Thus, the study make the reaction rate of the reaction time under different reaction time in the dynamic equation of the form of linear according to the following table, resulting in the kinetic model and kinetic parameters.

Table 1 kinetic model

functions	mechanism	Integral form
G-B	Three dimensional diffusion, spherical symmetric, 3d, D4, deceleration α curve	$(1-2/3\alpha) - (1-\alpha)^{2/3}$
Jander	3 d, D3, reduction of α curve, $n = 2$	$[1-(1-\alpha)]^{1/3}]^2$
Jander	Three dimensional diffusion, 3 d, $n = 1/2$	$[1-(1-\alpha)]^{1/3}]^{1/2}$
Jander	The two-dimensional diffusion, 2 d, $n = 1/2$	$[1-(1-\alpha)]^{1/2}]^{1/2}$
Avrami-Erofeev	Random nucleation and subsequent growth, A2, s-shaped α curve. $N = 1/2$, $m = 2$	$[-\ln(1-\alpha)]^{1/2}$
Avrami-Erofeev	Random nucleation and subsequent growth, A3, s-shaped α curve, $n = 1/3$, $m = 3$	$[-\ln(1-\alpha)]^{1/3}$
Avrami-Erofeev	Random nucleation and subsequent growth. $N = 4$	$[-\ln(1-\alpha)]^4$
Avrami-Erofeev	Random nucleation and subsequent growth, A4, s-shaped curve of α , $n = 1/4$, $m = 4$	$[-\ln(1-\alpha)]^{1/4}$
Avrami-Erofeev	Random nucleation and subsequent growth, $n = 2$	$[-\ln(1-\alpha)]^2$
Avrami-Erofeev	Random nucleation and subsequent growth, $n = 3$	$[-\ln(1-\alpha)]^3$
order reaction	$n=3$	$1-(1-\alpha)^3$
order reaction	$n=2$	$1-(1-\alpha)^2$
order reaction	$n=4$	$1-(1-\alpha)^4$
order reaction	$n=1/4$	$1-(1-\alpha)^{1/4}$
Mample Power	Phase boundary reaction (d), R1, $n = 1$	α
Mample Power	$n=3/2$	$\alpha^{3/2}$
Mample Power	$n=1/2$	$\alpha^{1/2}$
Mample Power	$n=1/3$	$\alpha^{1/3}$
Mample Power	$n=1/4$	$\alpha^{1/4}$

Results and Discussion

Fig.1 thermogravimetric curves of reactions of Al_2O_3 -spinel with Na_2CO_3

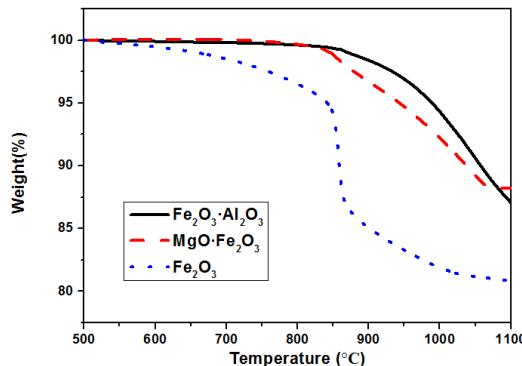


Fig.2 thermogravimetric curves of reactions of Fe₂O₃-spinel with Na₂CO₃

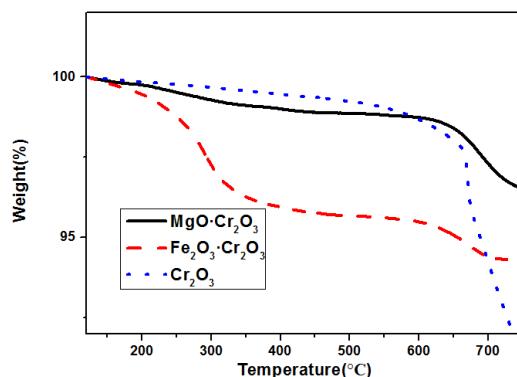


Fig. 3 thermogravimetric curves of reactions of Cr₂O₃-spinel with Na₂CO₃

Fig.1 depicts that the reaction of Al₂O₃ with Na₂CO₃ at the heating rate of 30 °C/min won't reach to reaction equilibrium when up to 1200 °C. while Al₂O₃ began to react with Na₂CO₃ after 800 °C and the reaction speed up at 950 °C. Magnesium aluminate spinel reacts with Na₂CO₃ at above 850 °C and when at 1200 °C the reaction is accelerated but not balance. The reaction of Hercynite with Na₂CO₃ began at around 800 °C, accelerating rapidly with rising temperature. What's more, the reaction get the maximum reaction rate at 1048 °C and is not balanced when 1200 °C.

Fig.2 shows the reaction of Fe₂O₃ with Na₂CO₃ is lower than the reaction of Na₂CO₃ with magnesium spinel reaction in temperature, speeding up at 700 °C and becoming a negative reaction between 850 °C to 860 °C. The products of Magnesia spinel reacting with Na₂CO₃ under the condition of high temperature are magnesium and iron material. So thermogravimetric curve of weightlessness is caused by releasing CO₂ in the process of forming acid sodium and the weightlessness rate is related to reflecting the generated rate of sodium ferrate. magnesia spinel has the obvious reaction with Na₂CO₃ until around 800 °C and at about 1000 °C reach equilibrium.

Fig.3 illustrates the reaction of iron chromium spinel with Na₂CO₃ starts below 600 °C and balances out at around 750 °C at the heating rate of 30 °C/min. Thermogravimetric curve shows that the reaction when 700 °C has been completed by more than 90%. reaction of Chrome oxide with Na₂CO₃ begin at about 600 °C and level off when 1000 °C. Furthermore, reaction quickened at 680 °C and is more easy to take place than that of Fe₂O₃ with Na₂CO₃. Reaction of Magnesium chromium spinel with Na₂CO₃ speed when 600 °C and is basically reach equilibrium when 800 °C.

According to the methods of studying kinetics under the condition of non-isothermal, reaction rates at different temperature are plugged into mechanism functions (F(α)) in the table below and are resolved by linear regression method. Through the analysis of the linear correlation coefficient and the sum of squared residuals, there was a good linear relationship between LnF(α)/T² and 1/T in process of Na₂CO₃ reacting with Fe₂O₃. Its process is in line with the Avrami - Erofeev model and its is random nucleation and growth. The integral form is [-ln(1-α)]⁴. The formula of F(α) is in the following:

$$F(\alpha) = \int_0^{\alpha} \frac{da}{f(\alpha)} = \frac{ART^2}{\beta E} \left(1 - \frac{2RT}{E}\right) e^{-\frac{E}{RT}} \quad (1)$$

The dynamic results of corrosion reactions are in the following table.

Table 2: Dynamic analysis

Materials	E(kJ/m ol)	A(min ⁻¹)	Kinetic Equations
Fe ₂ O ₃	414.92	6.08×10 ⁴³	dα/dT=1.52×10 ⁴³ exp(-49.90×1/T)(1-α)[-ln(1-α)] ⁻³
Cr ₂ O ₃	191.45	2.54×10 ¹⁵	dα/dT=6.35×10 ¹⁴ exp(-23.03×1/T)(1-α)[-ln(1-α)] ⁻³
Al ₂ O ₃	849.75	4.40×10 ³¹	dα/dT=1.10×10 ³¹ exp(-102.20×1/T)(1-α)[-ln(1-α)] ⁻³
Iron chromium spinel	225.12	2.26×10 ¹⁰	dα/dT=5.65×10 ⁹ exp(-27.08×1/T)(1-α)[-ln(1-α)] ⁻³
Magnesium chromium spinel	460.15	1.13×10 ²³	dα/dT=2.83×10 ²² exp(-55.35×1/T)(1-α)[-ln(1-α)] ⁻³
hercynite	672.81	3.97×10 ²¹	dα/dT=9.93×10 ²⁰ exp(-80.91×1/T)(1-α)[-ln(1-α)] ⁻³
Iron magnesia spinel	905.75	5.22×10 ³⁶	dα/dT=1.31×10 ³⁶ exp(-108.93×1/T)(1-α)[-ln(1-α)] ⁻³
Magnesium aluminate spinel	1328.4	5.75×10 ⁵³	dα/dT=1.44×10 ⁵³ exp(-159.76×1/T)(1-α)[-ln(1-α)] ⁻³
	0		

Conclusion

Integral method is used to deal with thermogravimetric experiments data. Through linear regression method we know that the reactions of refractories with Na₂CO₃ are all in line with the Avrami - Erofeev model. In addition, the mechanism is random nucleation and growth and the integral form is [-ln(1-α)]⁴. The characteristic parameters of reactions are obtained at the heating rate of 30°C/min. Reactions with Na₂CO₃ are sorted alphabetically by activation energy as follows: Cr₂O₃ < iron chromium spinel < Fe₂O₃ < magnesium, chromium spinel < hercynite < Al₂O₃ < alumina magnesia spinel < magnesium aluminate spinel. Reaction kinetics equations are as follows:

$$d\alpha/dT = 1/4A \exp(-E/RT)(1-\alpha) [-\ln(1-\alpha)]^3 \quad (2)$$

Acknowledgement

The authors thank the financial support for this work provided by the National Science and Technology Support Program(2013BAG25B03), Beijing Higher Education Young Elite Teacher Project (YETP0712), the Fundamental Research Funds for the Central Universities (2015MS20).

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