

Research on seismic performance of the multi-storey steel frame structure with additional oil dampers

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Keywords: Oil dampers. Damping multiples. Time history analysis. Damping effect.

Abstract. Based on the study of the multi-storey steel frame structure with additional oil dampers and consider composed of viscous coefficient c_1 、 c_2 with bilinear systems, vibration differential equations and computer programs are established. Taking damping multiples n as a parameter for elastic-plastic time history analysis, change rules of the particle displacement、the absolute acceleration response value and the oil damper energy reaction are discussed^[1].

Introduction

Seismic action is equal to the input of vibration energy on the structure. Buildings under seismic action, therefore, should have sufficient energy dissipation capacity in order to avoid damage. Energy dissipation structure is that some non bearing members(such as bracing, shear wall, connectors, etc.) are designed to energy dissipation members or install energy dissipation device in a portion of the structure(space, node and connecting seam, etc.).This structure protects the main structure and components from damage and ensures the safety in strong earthquake. The oil damper is a kind of energy dissipation device which has superior performance, simple structure, convenient production. The oil damper has the advantages of small volume, large energy absorption, good damping effect, high efficiency, low price, good durability and so on. It has been shown that energy dissipation effect is very obvious and the damper has wide application prospect^[2].

Analysis of structure with additional oil dampers

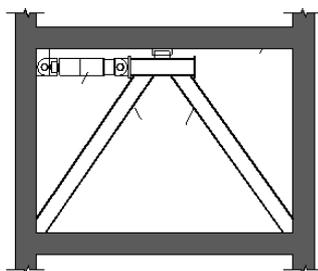


Fig.1 Additional oil damper structure diagram

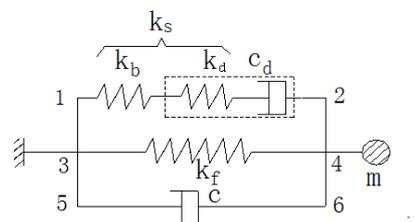


Fig.2 Additional oil dampers structural analysis model

The research object of this article is a multi-storey structure with additional oil dampers^[3]. Figure 1 shows the connecting way of oil damper. Figure 2 shows analysis model of additional oil dampers structural. Among them, 1-2 segment represents attached system of oil damper and series of bracing, k_b represents the horizontal bracing lateral stiffness, k_d represents the internal stiffness of oil damper, c_d represents internal viscous damping coefficient of oil damper, k_s represents sum of support stiffness and internal damper stiffness. Its value is:

$$k_s = k_b k_d / (k_b + k_d)$$

(1)

In this formula, $k_d = qc_d$, q is internal stiffness coefficient, usually takes 4.5~18 (1/s). 3-4 segment represents the main part of structure (beams and columns), among them, k_f represents the lateral stiffness of structure. In the 5-6 segment, c represents the damping coefficient of structure, m is mass^[4].

The vibration differential equation of multi-storey structure with additional oil dampers in strong earthquake is:

$$M \ddot{x} + C \dot{x} + K_F x + F_C = M \ddot{x}_g$$

(2)

In this formula, M represents the mass matrix of structure; C represents internal viscous damping coefficient matrix of structure, using Rayleigh damper, $C = aM + bK$; K_F represents lateral stiffness matrix of structure with additional oil damper, its value is $K_F = K_f + K_s$; F_C represents damping force of additional system. x , \dot{x} , \ddot{x}_g represents the displacement, velocity and acceleration of structure. \ddot{x}_g represents ground acceleration.

Principle Analysis

In this paper, we assume that structure under seismic loading is always in a state of elastic deformation. The lateral stiffness is k_f , damping ratio is 0.02. Internal elastic stiffness of oil damper is k_d , the plastic stiffness is zero. Lateral stiffness of the bracing in series with the damper is k_b . Assume that k_b is much greater than k_d . According to equation (2), k_s is determined by k_d .

Viscous coefficient C_d used in this paper is bilinear systems which is composed of the first, second viscous coefficient C_1 , C_2 (Figure 3, $dup1$ is the yield velocity of the viscous unit). $C_2 = pC_1$, (p is the second viscous coefficient ratio). When the velocity of viscous unit reaches the yield velocity, its viscous coefficient will be C_2 .

In this paper, viscous coefficient of structure with additional oil dampers is taken as a parameter. Its value is $C_1 = 10n(kN \cdot (s/cm))$ and n (referred damping multiply) changes from 1 to 5. Assume that $C_2 = qC_1$, $q = 0.05$, $k_d = qC_1$, q is the internal stiffness coefficient and $q = 10$. Therefore, there is proportional relationship between the internal stiffness of oil damper k_d and damping multiply n .

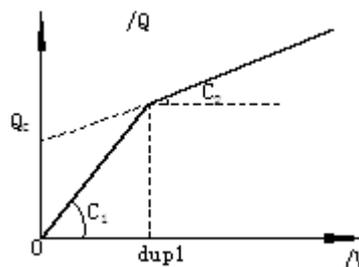


Fig.3 Damping force - velocity relationship

Displacement reaction

Under three earthquakes (sine wave, which period is 1.0s; frequent earthquake, which peak acceleration is 70cm/s^2 ; rare earthquake, which peak acceleration is 400cm/s^2), time history analysis of the original structure and structure with additional oil damper was carry on and we compared the results^[5].

In figure 4, the abscissa represents the maximum story drift of structure, the ordinate represents the number of structure layers. Taking damping multiply n as parameter, compare the results of the original structure and the structure with additional oil damper. As we can see from the picture, the

maximum story drift of the structure with additional oil damper is smaller than the original structure. When damping multiply of the structure with additional oil damper becomes larger, the maximum story drift is smaller. We can come to the conclusion that oil damper attached to the structure plays an important role in reducing the displacement. The more amount of additional damper is, the smaller story drift becomes, the damping effect is better.

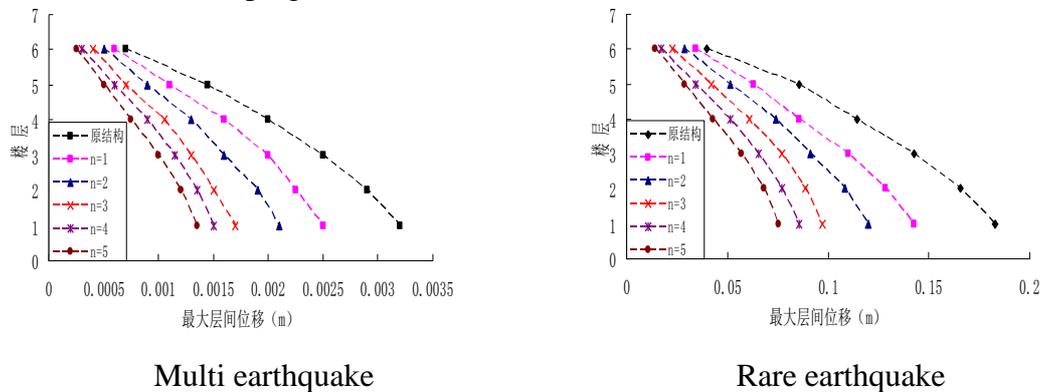


Fig.4 Displacement reaction

The acceleration response

In figure 5, the abscissa represents the maximum absolute acceleration of structure, the ordinate represents the number of structure layers. Taking damping multiply n as parameter, compare the results of the original structure and the structure with additional oil damper. As we can see from the picture, the maximum absolute acceleration of the structure with additional oil damper is smaller than the original structure. When damping multiply of the structure with additional oil damper becomes larger, the maximum absolute acceleration is smaller. We can come to the conclusion that oil damper attached to the structure plays an important role in reducing the absolute acceleration. The more amount of additional damper is, the smaller absolute acceleration becomes, the damping effect is better.

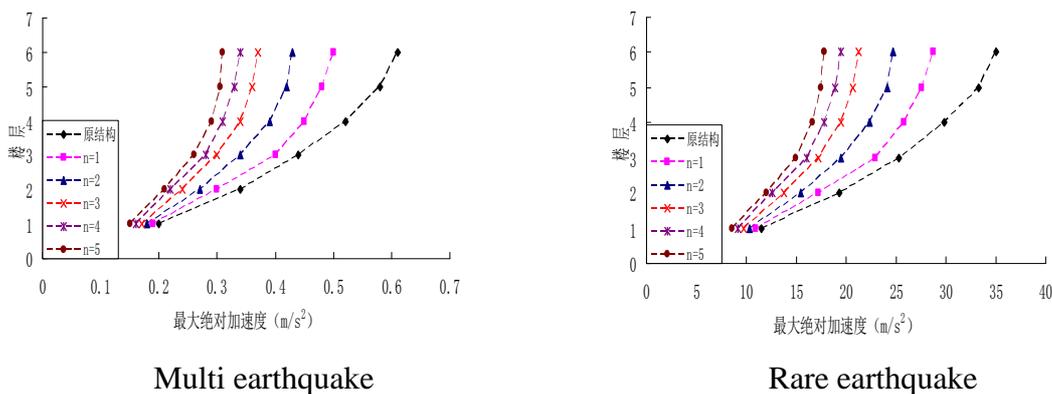


Fig.5 Acceleration response

Energy response

In figure 6, the abscissa represents time, the ordinate represents the energy consumed by the damper. Taking damping multiply as parameter, compare the results of the original structure and the structure with additional oil damper. As we can see from the picture, when damping multiply of the structure with additional oil damper becomes larger, the energy consumed by the damper becomes larger. Therefore, additional oil damper can control structural damage effectively, it can transfer damage to the replaceable additional oil dampers and protect the main structure effectively.

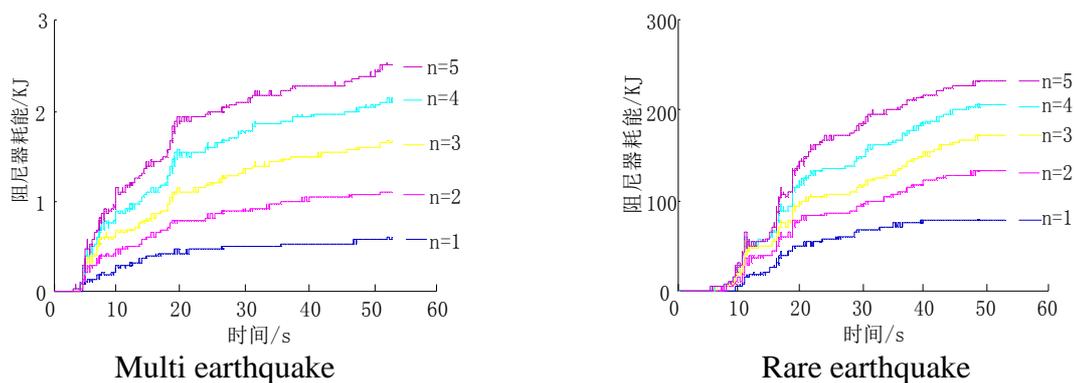


Fig.6 Oil damper energy reaction

Conclusions

The research object of this paper is a multi-storey steel frame structure with additional oil dampers. Conclusions are as follows:

(1) When damping multiply is larger, the internal elastic stiffness of additional damper k_d is larger, story drift of structure is smaller, the damping effect is better.

(2) When damping multiply is larger, absolute acceleration of structure is smaller, the damping effect is better.

(3) When damping multiply is larger, the internal elastic stiffness of additional damper is larger, the energy consumed by the damper becomes more, the energy consumed by the structure becomes less.

In conclusion, the additional oil damper reduces story drift, absolute acceleration of structure and energy consumed by the structure, thus achieves good damping effect.

References

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