# Study on the Theory of Projectile Firing Process during Marching Fire

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Abstract—The initial disturbance of the projectile is the premier factor that takes effect on the marching fire accuracy of the conventional weapon, which depends on the projectile firing process of the conventional weapon. In this paper, the theory of projectile firing process of the conventional weapon during marching fire was studied. Combining the projetile motion equations in gun tube with the system dynamics equations which can be obtained by various multibody system dynamics methods, the motion of the projectile in barrel and the initial disturbance of the projectile can be exactly simulated. This work provides both theoretical foundation and simulation approaches for improving the marching fire accuracy of the conventional weapon.

Keywords-marching fire; projectile firing process; firing accuracy; initial disturbance

#### I. INTRODUCTION

The launch process has great influence on the dynamic property of weapons, especially on the marching fire accuracy of weapons. It is verified by the theory and tests that1, 2, the initial disturbance of the projectile is the premier factor which takes effect on the marching fire accuracy of weapons. Meanwhile, the influence of road excitation, vibration and stabilization precision on the marching fire accuracy can also be reflected by the initial disturbance of the projectile. To a major extent, the marching fire accuracy of weapons depends on the behavior of its projectile firing process. The projectile firing process3 is a novel subject which studies the principle of forces and the movements of the weapon system in the launch process. Further, it provides the theorem and techniques of control and principles of forces and movements for system design and test of dynamic properties of weapon systems. Developed for many years, theory of projectile firing process has come into the stage of engineering applications by Xiao-ting Rui, et al4-9. Fruitful achievement has been gained in improving the firing accuracy and reducing ammunition consumption. The launch dynamics of tanks and self-propelled artilleries marching fire were studied by many scholars10-12,

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however, the dynamics models of weapon systems are relatively simple, and the theory of projectile firing process during marching are imperfect. Thereby, it is impossible to get the accurate initial disturbance of the projectile, and thus difficult to discuss the way of improving the marching fire accuracy of weapons.

Aiming at these problems, this paper studied on the theory of projectile firing process of weapons during marching fire. Take a self-propelled and tank artillery as examples, the motion of the projectile in barrel, the initial disturbance of the projectile and the vertical target dispersion were exactly simulated, meanwhile, the results of simulation are verified by tests.

## II. THE PROJECTILE MOTION EQUATIONS IN GUN TUBE DURING MARCHING

Based on the previous studies<sup>1-9, 13</sup>, regarding the projectile as a rigid body, the elastic effect of projectile-barrel interaction modeled as the elastic contact forces between barrel and bourrelet, and between the barrel and the bearing band.

## *A.* The coordinate systems of the projectile motion in gun tube

Based on literature [2], the barrel coordinate system  $O_4 x_4 y_4 z_4$  (b.c.s) is introduced. At the initial time, the origin  $O_4$  of b.c.s and the origin  $O_3$  of the artillery coordinate system  $O_3 x'_o y'_o z'_o$  (a.c.s) match together, the positive direction of  $x_4$ -axis is along the tangent of barrel axis pointing to the muzzle,  $y_4$ -axis is perpendicular to  $x_4$ -axis in the vertical plane,  $z_4$ -axis is determined by the right-hand rule. The coordinate system is fixed with the barrel. The artillery coordinate system, the ground coordinate system (g.c.s), the projectile axis coordinate system (p.c.s) are defined in ref. [2].

# B. The differential equations of motion of the projectile mass center during marching fire

$$\boldsymbol{F}_{\boldsymbol{C}} = \boldsymbol{m}(\boldsymbol{a}_{\boldsymbol{C}}' + \boldsymbol{A}_{4,0}^{\mathrm{T}}\boldsymbol{D}_{1}\ddot{\boldsymbol{x}}_{p} + \ddot{\boldsymbol{r}}_{o_{3}\boldsymbol{C}}). \tag{1}$$

applying the relative moment of momentum theorem

relative to moving coordinate system, the differential

of

the

projectile

are

According to the Newton's second law of motion, the equations of motion of the projectile mass center (m.c.) during marching is

Where,

equations of rotation

$$\boldsymbol{a}_{C}^{\prime} = \boldsymbol{A}_{4,0}^{\mathrm{T}} \boldsymbol{A}_{1,4}^{\mathrm{T}} \ddot{\boldsymbol{r}}_{o_{4}} + \boldsymbol{A}_{4,0}^{\mathrm{T}} (\boldsymbol{D}_{5} + 2\dot{\boldsymbol{x}}_{p} \boldsymbol{D}_{4} + \dot{\boldsymbol{x}}_{p}^{2} \boldsymbol{D}_{2} + 2\tilde{\boldsymbol{\omega}}_{4,1} (\boldsymbol{D}_{2} + \dot{\boldsymbol{x}}_{p} \boldsymbol{D}_{1}) + \dot{\tilde{\boldsymbol{\omega}}}_{4,1} \boldsymbol{r}_{o_{4}o_{3}} + \tilde{\boldsymbol{\omega}}_{4,1} \tilde{\boldsymbol{\omega}}_{4,1} \boldsymbol{r}_{o_{4}o_{3}}) + \\ \boldsymbol{A}_{\theta}^{\mathrm{T}} (\ddot{\boldsymbol{A}}_{\theta} \boldsymbol{r}_{o_{3}C} + 2\dot{\boldsymbol{A}}_{\theta} \dot{\boldsymbol{r}}_{o_{3}C} + 2\tilde{\boldsymbol{\omega}}_{\alpha} (\dot{\boldsymbol{A}}_{\theta} \boldsymbol{r}_{o_{3}C} + \boldsymbol{A}_{\theta} \dot{\boldsymbol{r}}_{o_{3}C}) + \tilde{\boldsymbol{\omega}}_{\alpha} \tilde{\boldsymbol{\omega}}_{\alpha} \boldsymbol{A}_{\theta} \boldsymbol{r}_{o_{3}C} + (\boldsymbol{B} - \tilde{\boldsymbol{\omega}}_{\psi} (\boldsymbol{A}_{\psi} \boldsymbol{\omega}_{4,1}) + \boldsymbol{A}_{\psi} \dot{\boldsymbol{\omega}}_{4,1}) \boldsymbol{A}_{\theta} \boldsymbol{r}_{o_{3}C}) \cdot$$

$$(2)$$

$$\boldsymbol{D}_{I} = \frac{\partial \boldsymbol{r}_{o_{4}o_{3}}}{\partial \boldsymbol{s}}; \quad \boldsymbol{D}_{2} = \frac{\partial \boldsymbol{r}_{o_{4}o_{3}}}{\partial \boldsymbol{t}} \quad ; \quad \boldsymbol{D}_{4} = \frac{\partial^{2} \boldsymbol{r}_{o_{4}o_{3}}}{\partial \boldsymbol{s}\partial \boldsymbol{t}} \quad ; \quad \boldsymbol{D}_{5} = \frac{\partial^{2} \boldsymbol{r}_{o_{4}o_{3}}}{\partial \boldsymbol{t}^{2}} \cdot$$
(3)

the physical meanings of symbols and the calculation methods of parameters coincide with ref. [22,23].

### *C.* The differential equations of rotation of projectile during marching fire

Taking the p.a.c.s as a moving coordinate system, the projectile geometrical center  $O_1$  (g.c.) as basic point,

$$\ddot{\gamma} \begin{bmatrix} C \\ -(A-C)\beta_{D_q} \\ -(A-C)\beta_{D_c} \end{bmatrix} + J_{o_1} \begin{bmatrix} \delta_2^I \ddot{\delta}_1^I \\ -\ddot{\delta}_2^I \\ \ddot{\delta}_1^I \end{bmatrix} + m\tilde{r}_{o_1C} A_{2,0} (A_{4,0}^T D_I \ddot{x}_p + \ddot{r}_{o_3c} - B_5 \ddot{\gamma}) = M_{o_1} + M_I$$

$$(4)$$

where

$$M_{I} = -J_{o_{1}} (\Delta + \widetilde{\omega}_{2,0} A_{2,0} \omega_{\theta} + A_{2,0} \dot{\omega}_{\theta} - \widetilde{\omega}_{\delta} A_{2,0} A_{\theta}^{\mathrm{T}} \omega_{a} + A_{2,0} A_{\theta}^{\mathrm{T}} (B + \widetilde{\omega}_{\psi} A_{\psi} \omega_{4,1} + A_{\psi} \dot{\omega}_{4,1})) - \widetilde{\omega}_{2,1} G_{o_{1}}^{r} + \widetilde{\omega}_{2,1} J_{o_{1}} \omega_{2,1} - m \widetilde{r}_{o_{1}C} A_{2,0} (a_{C}^{r} + A_{\theta}^{\mathrm{T}} (\ddot{A}_{\theta} B_{3} + 2\dot{A}_{\theta} B_{4} + 2\widetilde{\omega}_{a} (\dot{A}_{\theta} B_{3} + A_{\theta} B_{4}) + .$$

$$(B - \widetilde{\omega}_{\psi} A_{\psi} \omega_{4,1} + A_{\psi} \dot{\omega}_{4,1}) A_{\theta} B_{3} + \widetilde{\omega}_{a} \widetilde{\omega}_{a} A_{\theta} B_{3}) - \dot{\gamma}^{2} B_{3}) - \dot{\gamma}^{2} N + \frac{\widetilde{\mathrm{d}} J_{o_{1}}}{\mathrm{d} t} \omega_{2,1} + \widetilde{\omega}_{2,1} J_{o_{1}} \omega_{2,1}$$

$$(5)$$

the physical meanings of symbols and the calculation methods of parameters coincide with ref. [22,23].

#### III. THE SYSTEM DYNAMICS EQUATIONS OF WEAPONS

Multibody system dynamics provides a strong tool for dynamic performance estimation and optimizing design of weapon<sup>14</sup>. The present multibody system dynamics methods mainly include Newton-Euler vector mechanical method, Jourdam principle, Lagrange method, Gauss

principle, Transfer matrix method of multibody system, and so  $on^{15-19}$ .

Taking a self-propelled artillery and tank as examples, applying the transfer matrix method for multibody system (MSTMM) and the automatic deduction theorem of overall transfer equation<sup>20,21</sup>, the system dynamics equations of the self-propelled artillery and tank were derived in ref. [22,23]. The topological graph of the self-propelled artillery dynamics model is shown in Fig .1. more details about the model can refer to literature [22,23].



Figure 1. Topological graph of launch dynamics of a self-propelled artillery.

#### IV. THE SIMULATION OF THE SELF-PROPELLED ARTILLERY AND TANK MARCHING FIRE AND ITS TEST VERIFICATION

On the base of the preceding projectile firing process equations and the multibody dynamic equations of the self-propelled artillery and tank during marching, the simulation program of the launch dynamics of the self-propelled artillery and tank were compiled, and the simulation results of the self-propelled artillery and tank during marching fire and fire at rest were given in Fig .2 – Fig .6 and Table I – Table II.



Figure 2. The results of the breech pressure obtained by computation and test.

Fig .2 is the curves of the breech pressure obtained by computation and test, the simulation error of the maximum breech pressure is 1.13% and the simulation curves of the breech pressure are well fit with experimental results.

Fig. 3 – Fig. 4 are the simulation curves of impact force of the self-propelled artillery between the bourrelet and the barrel, the projectile vertical swing angular velocity of the self-propelled artillery respectively. Marching fire conditions: the self-propelled artillery speed is 20 Km/h, road profile is level D, fire angle is 51°.





Figure 3. between the barrel and the bourrelet.



Figure 4. Computational results of the projectile vertical swinging angular velocity of the self-propelled artillery.

Fig. 5 – Fig. 6 are the simulation curves of impact force of the tank between the bourrelet and the barrel, the projectile vertical swing angular velocity of the tank respectively. Marching fire conditions: the tank speed is 40 Km/h, road profile is level D, fire angle is  $0^{\circ}$ .

The barrel-projectile impact force and vertical swing angular velocity of projectile during marching fire are significantly distinguished from those during fire at rest.



Figure 5. Computational results of the impact force of the tank between the barrel and the bourrelet.



Figure 6. Computational results of the projectile vertical swinging angular velocity of the tank.

Table I is the simulation results of initial disturbance of the self-propelled artillery and Table II is the results of fire dispersion of the self-propelled artillery obtained by computation and test, the simulation errors during fire at rest are 8.7% (distance dispersion) and 7.2% (direction dispersion). And the results of fire dispersion obtained by computation during marching fire are worse than those during fire at rest, the situation is suitable in real cases.

 
 TABLE I.
 The results of initial disturbance of the projectile obtained by computation

$y_{o_{3}c}/(mm)$	Z <sub>03</sub> c/(mm)	$\gamma$ /(mrad)	$\delta_1^I$ /(mrad)	$\delta_2^I$ /(mrad)
-0.200	-0.031	9.302	-0.769	-0.103
$\dot{y}_{o_3c}/(mm)$	$\dot{z}_{o_3c}/(mm)$	$\dot{\gamma}$ /(mrad)	$\dot{\delta}^I_1$ /(mrad)	$\dot{\delta}^I_2$ /(mrad)
0.072	-0.395	1621.4	-0.025	-1.03

TABLE II. THE RESULT OF FIRE DISPERSION OBTAINED BY COMPUTATION AND TEST

	Fire dispersion /m		
Simulation and test result	Distance dispersion	Direction dispersion	
Simulation result (at rest)	161.3	51.2	
Simulation result (on the march)	184.2	53.4	
Test result (at rest)	176.7	48.7	

The above results have shown that the projectile firing process equations during marching established and the simulation program of the self-propelled artillery and tank launch dynamic compiled in this paper are correct and feasible.

#### V. CONCLUSIONS

The projectile motion equations in gun tube during marching fire were deduced. Take a self-propelled artillery and tank as examples, combing the projectile motion equations during marching fire with the multibody system dynamics equations of the self-propelled artillery and tank obtained by applying the MSTMM, a program of the launch dynamics of the self-propelled artillery and tank was compiled. Via the program, the motion of the projectile in the barrel, initial disturbance of the projectile and the fire dispersion are simulated.

The simulation curves of the breech pressure of the self-propelled artillery are well fit with experimental results, the simulation error of the maximum breech pressure of the self-propelled artillery is 1.13% and the simulation errors of the self-propelled artillery fire dispersion during fire at rest are 8.7% (distance dispersion) and 7.2% (direction dispersion). The simulation results show that the fire dispersion during marching fire are worse than those during fire at rest. This work provides both theoretical foundation and simulation approaches for improving the marching fire accuracy of the conventional weapon.

#### ACKNOWLEDGMENT

This work was financially supported by the Equipment Pre-research Mutual Application Techniques Foundation of China (Grant No.9140A10041013BQ02143) and the National Natural Science Foundation of China (Grant no.61304137).

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