

Low-Cycle Fatigue Behavior of Al-4.5Cu-0.6Mg-0.3Si Alloy Containing 0.3%Ce

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Abstract—Fatigue test of Al-4.5Cu-0.6Mg-0.3Si-(0.3Ce) alloy with solution plus artificial aging treatment state was carried out on fatigue experimental machine. The low cycle fatigue behavior and fracture behavior of Al-4.5Cu-0.6Mg-0.3Si-(0.3Ce) alloys were studied. The results show that Al-4.5Cu-0.6Mg-0.3Si-(0.3Ce) alloy can exhibit the cyclic hardening, softening and stable cyclic stress response which mainly depends on the imposed total strain amplitudes. The addition of rare earth element Ce can effectively enhance the cyclic deformation resistance and low-cycle fatigue life of Al-4.5Cu-0.6Mg-0.3Si alloy. For the Al-4.5Cu-0.6Mg-0.3Si (-0.3Ce) alloy, the relation between plastic and reversals to failure as well as elastic strain amplitudes can be described respectively by Coffin-Manson and Basquin equations. The observations on fracture surfaces reveal that under low-cycle fatigue loading condition, the fatigue cracks initiate transgranular at the surface of fatigue samples and propagate transgranular for the Al-4.5Cu-0.6Mg-0.3Si-(0.3Ce) alloy.

Keywords—Al-4.5Cu-0.6Mg-0.3Si-(0.3Ce) alloy; at treatment; low-cycle fatigue; fatigue fracture

I. INTRODUCTION

Fatigue behavior of aluminum alloy research has made great progress as an important part in the field of materials science [1-3]. Many scientific research on the fatigue performance have been done due to the fatigue property of aluminum alloy is closely linked with the practical application [4-6]. It was reported that the Al-Cu-Mg alloy has a higher fatigue crack growth resistance in electric field. Rare earths in non-ferrous metal materials, especially in the application of aluminum and its alloy has

made obvious effect, brought a certain economic and social benefits [7]. Rare earth elements can through with the solution of pests to take all kinds of stable compounds, reducing inclusions in aluminum liquid, at the same time reduce the rate of pinhole and the porosity of castings, purification of aluminum alloy [8]. In pursuit of developing high strength aluminum alloys, micro-alloying of rare earth elements have shown remarkable effect in terms of refining as microstructure, retarding recrystallisation and refining precipitate phases [9-11]. It was reported that when adding 0.3% Ce, the dislocation and dislocation of aluminium alloy after casting tangles structure lead to changing the position of crack initiation and extension path, to improve the toughness of the alloy [12]. The role of refining grains of Ce in addition to the metamorphism of rare earth can also be explained as follows: Main enrichment of Ce on the grain boundary, or in small rare earth compounds present in the intracrystalline which can be used as the core of heterogeneous nucleation. Therefore, adding trace amounts of Ce is helpful to reduce grain size through improve the nucleation number of crystallization [13]. The present work was thus to examine such effect with a view of establishing the potential for enhancing the mechanical properties of these alloys.

In order to ensure the low-cycle fatigue behavior and explore the rules and effect of rare earth element Ce addition on the fatigue behavior of Al-4.5Cu-0.6Mg-0.3Si alloy, this paper take into consideration the theoretical discussion of the low-cycle fatigue behavior and the damage mechanism in order to improve the fatigue performance of the department alloy and provide reliable theoretical basis for practical application.

II. EXPERIMENTAL

SG-5-10 electrical resistance furnace crucible was used to melt the 99.8% aluminum ingot, industrially pure 99.9%Cu, 99.8% Mg, and Al-Ce master alloy at 730°C respectively and the melt was cast to Al-4.5Cu-0.6Mg-0.3Si and Al-4.5Cu-0.6Mg-0.3Si-0.3Ce alloy in a 130 mm cube steel mould. The 1250t horizontal extrusion machine was used to hot extrusion for aluminum alloy ingot, the extrusion ratio was 36:1, the extrusion rod processed into fatigue specimen scale with the distance is 6 mm diameter and gage length of 10 mm, then the T6 treatment to fatigue specimen with solution at 520°C for 4h and then water cooling, and aging at 180°C for 14h and then subsequently air cooling.

Low cycle fatigue experiments in the laboratory static pressure air medium under the axial tensile-full reverse total strain amplitude control mode at room temperature with strain ratio of $R_e=1$ on the PLD-50 fatigue test machine. The name of the total strain amplitude range 0.4% to 1.2% and the frequency was 1 Hz. All fatigue experiments are conducted to the cyclic stress amplitude decreased to 80% of the peak of stress amplitude in the entire process of fatigue deformation and the cyclic number is defined as the fatigue life. S-3400N scanning electron microscope was used to scanning analysis the fatigue fracture, JEM-2100 transmission electron microscopy was used to observe the microstructure of fatigue deformation zone. The process of TEM sample

preparation was as follows: first of all was mechanical thinning, Electrolytic thinning experiment was conducted in the MTP-1 type electro polisher. Electrolyte is 30% HNO_3 + 70% CH_3OH (volume fraction) mixture at 30°C, the voltage was 17V, electric current was 40 mA.

III. RESULTS AND DISCUSSION

A. Cyclic Stress Response Behavior of Al-4.5Cu-0.6Mg-0.3Si(-0.3Ce) Alloys

The cyclic stress response curves of the Al-4.5Cu-0.6Mg-0.3Si(-0.3Ce) alloys at various total strain amplitudes are shown in Figure 1. As shown in Figure 1(a), the stable cyclic stress response of the Al-4.5Cu-0.6Mg-0.3Si alloy is noted at the whole fatigue deformation at the total strain amplitude of 0.4%. At the total strain amplitude of 0.5%~1.2%, the alloy exhibits the continuous cyclic strain hardening, but the hardening rate decreases significantly at the later stage of fatigue deformation until the fracture. Figure 1(b) comprehensively shows that when plus total strain amplitude is 0.4% or 0.5%, the Al-4.5Cu-0.6Mg-0.3Si and Al-4.5Cu-0.6Mg-0.3Si-0.3Ce alloys characterized by cyclic hardening in the early stages of the fatigue deformation, and then show the cycle stability. When plus total strain amplitude is 0.6%, 0.8%, 1.0% or 1.2%, Al-4.5Cu-0.6Mg-0.3Si and Al-4.5Cu-0.6Mg-0.3Si-0.3Ce alloys characterized by cyclic hardening in the early stages of the fatigue deformation, and then show the cycle softening.

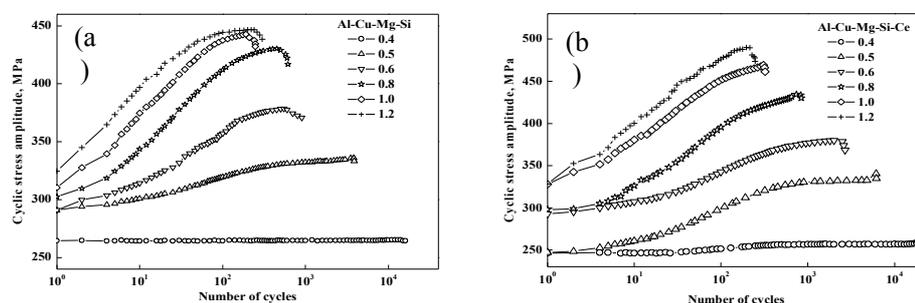


Figure 1. Cyclic stress response curves of extruded Al-4.5Cu-0.6Mg-0.3Si(-0.3Ce) alloys with T6 treatment

(a) Al-4.5Cu-0.6Mg-0.3Si alloy; (b) Al-4.5Cu-0.6Mg-0.3Si-0.3Ce alloy

The cyclic stress response curves of Al-4.5Cu-0.6Mg-0.3Si(-0.3Ce) alloys at various total strain amplitudes are

illustrated in Figure 2, it can be seen from the graph that the Al-4.5Cu-0.6Mg-0.3Si-0.3Ce alloy exhibits the higher cyclic stress level on the whole fatigue deformation stage under the same plus total strain amplitude. This phenomenon can be explained by that Ce can strengthen the grain boundary, refine and dispersion the strengthening phase of Al-4.5Cu-0.6Mg-0.3Si alloy, so as to improve the cyclic deformation resistance of Al-4.5Cu-

0.6Mg-0.3Si alloy. In addition, Ce can inhibit recrystallization, combined to obtain certain external reinforcement, external toughening effect. Moreover, rare earth element Ce can form intermetallic compound Al_3Ce with aluminum. It will increase the stacking fault energy of $\{111\}$ surface, then increase the coplanar slip tendency of Al-4.5Cu-0.6Mg-0.3Si alloy.

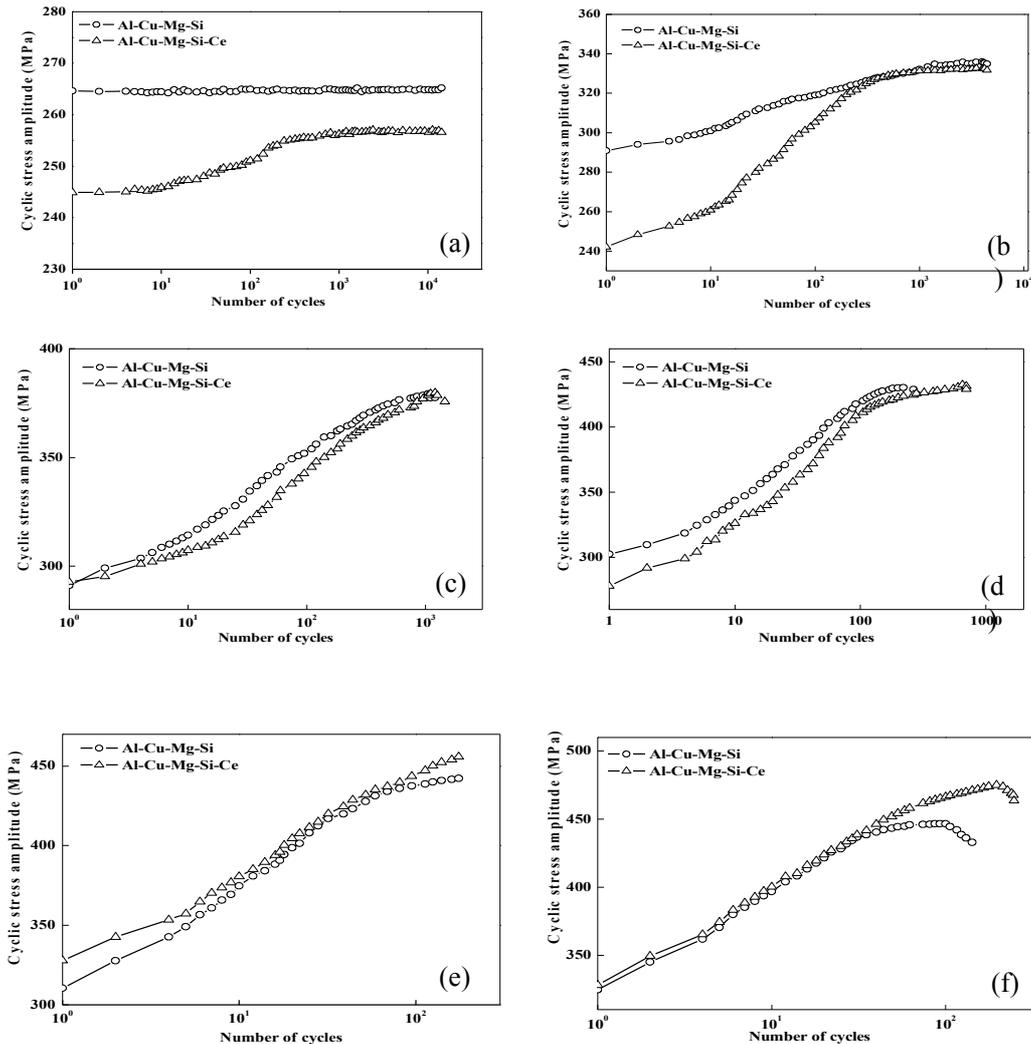


Figure 2. Comparison in cyclic stress response curves for Al-4.5Cu-0.6Mg-0.3Si (-0.3Ce) alloys with T6 treatment

(a) $\Delta\epsilon_t/2 = 0.4\%$; (b) $\Delta\epsilon_t/2 = 0.5\%$; (c) $\Delta\epsilon_t/2 = 0.6\%$; (d) $\Delta\epsilon_t/2 = 0.8\%$; (e) $\Delta\epsilon_t/2 = 1.0\%$ (f) $\Delta\epsilon_t/2 = 1.2\%$

B. Low-fatigue Life Behavior of Al-4.5Cu-0.6Mg-0.3Si(-0.3Ce) Alloys

The total strain amplitude ($\Delta\epsilon/2$) versus fatigue life (N_f) curves for both Al-Cu-Mg-Si and Al-Cu-Mg-Si-Ce alloys with T6 treatment are shown in Figure 3. It is noted

that the fatigue life of the Al-Cu-Mg-Si-Ce alloy is higher than that of the Al-4.5Cu-0.6Mg-0.3Si alloy at various total strain amplitudes. This can be inferred that low cyclic fatigue lives of the Al-Cu-Mg alloy with T6 treated state is significantly improved when rare earth element 0.3% Ce is added.

Figure 4 show the plastic strain amplitude and elastic strain amplitude versus reversals to failure curves of Al-4.5Cu-0.6Mg-0.3Si and Al-4.5Cu-0.6Mg-0.3Si-0.3Ce alloys.

As seen in Figure 4, the plastic and the elastic strain

amplitudes of Al-4.5Cu-0.6Mg-0.3Si and Al-4.5Cu-0.6Mg-0.3Si-0.3Ce alloys with T6 treated state as a function of reversals to failure show a linear relationship which are obey Coffin-Manson and Basquin theory.

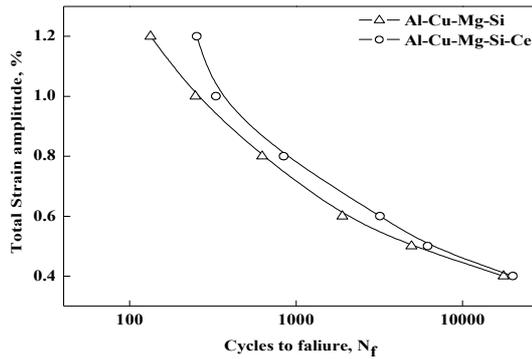


Figure 3. Total strain amplitude versus fatigue life curves for Al-4.5Cu-0.6Mg-0.3Si(-0.3Ce) alloys

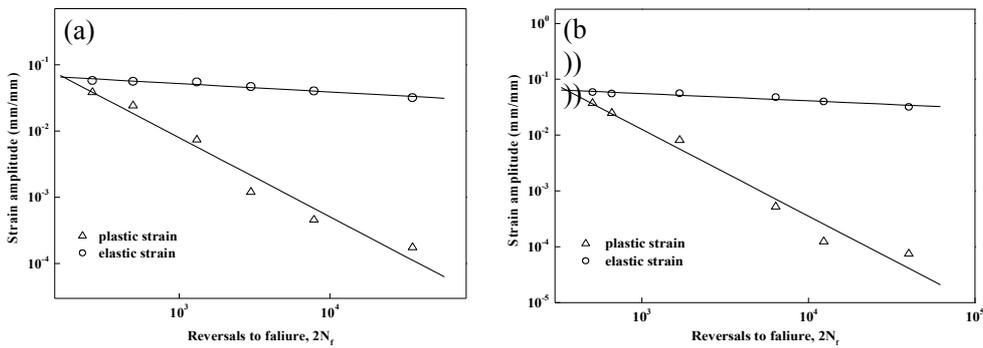


Figure 4. Strain amplitude versus reversals to failure curves of Al-4.5Cu-0.6Mg-0.3Si(-0.3Ce) alloys

(a) Al-4.5Cu-0.6Mg-0.3Si alloy (b) Al-4.5Cu-0.6Mg-0.3Si-0.3Ce alloy

C. Cyclic Stress-strain Behavior of Al-4.5Cu-0.6Mg-0.3Si(-0.3Ce) Alloys

The relationship between cyclic stress amplitude and plastic strain amplitude can be expressed by the power law:

$$\Delta\sigma / 2 = K'(\Delta\varepsilon_p / 2)^{n'} \tag{1}$$

Where K' is the cyclic strength coefficient and n' is the cyclic strain-hardening exponent. Cyclic stress versus

strain curves for Al-4.5Cu-0.6Mg-0.3Si (-0.3Ce) alloys with T6 state are shown in Figure 5. For the Al-4.5Cu-0.6Mg-0.3Si and Al-4.5Cu-0.6Mg-0.3Si-0.3Ce alloys with T6 treated, the relationship between the plastic strain amplitude and the cyclic stress amplitude is the single slope straight line. They also obey the index relationship in (1), the K' and n' values of two alloys can be determined by linear regression analysis as shown in Table I. It can be seen from Table I that the Al-4.5Cu-0.6Mg-0.3Si-0.3Ce alloy can increase the K' and n' values compared with the Al-4.5Cu-0.6Mg-0.3Si alloy.

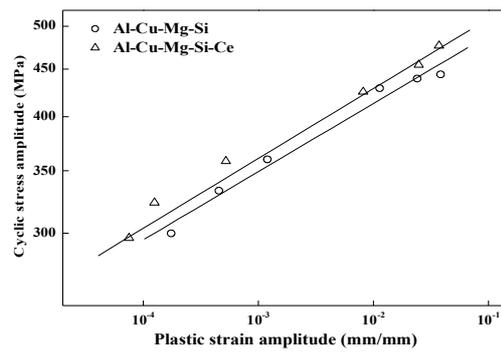
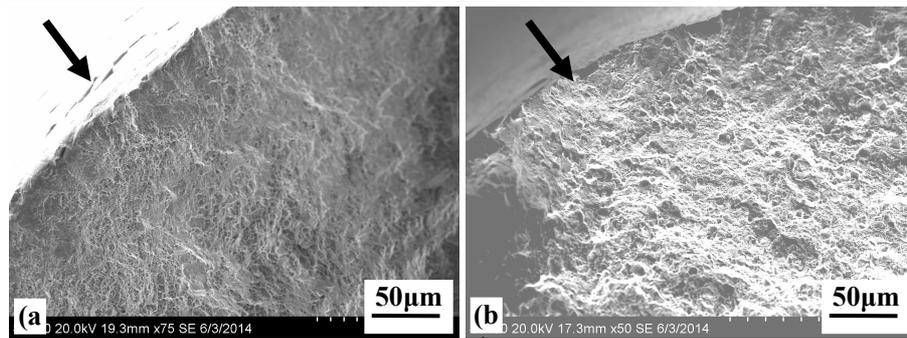
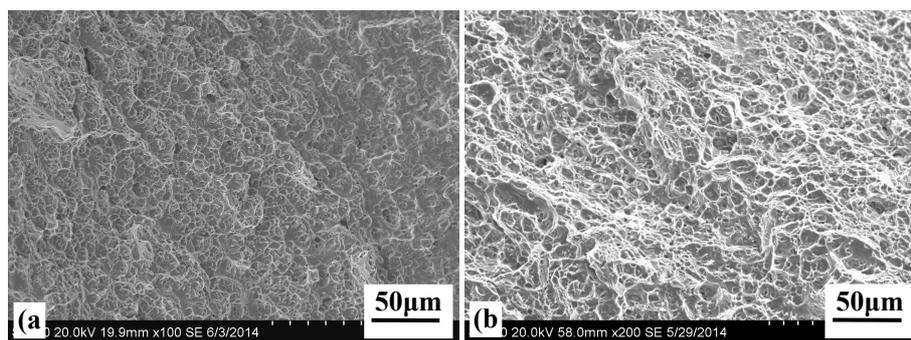


Figure 5. Cyclic stress-strain curves of Al-4.5Cu-0.6Mg-0.3Si(-0.3Ce) alloys

TABLE I. STRAIN FATIGUE PARAMETERS OF AL-4.5CU-0.6MG-0.3SI AND AL-4.5CU-0.6MG-0.3SI-0.3CE ALLOYS

	σ'_f (MPa)	b	ϵ'_f (%)	c	K' (MPa)	n'
Al-Cu-Mg-Si alloy	862.7	-0.125	0.0641	1.480	578.3	0.073
Al-Cu-Mg-Si-Ce alloy	964.8	-0.132	0.0681	2.753	605	0.075


 Figure 6. Fatigue crack initiation region for extruded Al-4.5Cu-0.6Mg-0.3Si(-0.3Ce) alloys with T6 state
 (a) Al-4.5Cu-0.6Mg-0.3Si alloy, $\Delta\epsilon_t/2=0.8\%$; (b) Al-4.5Cu-0.6Mg-0.3Si-0.3Ce alloy, $\Delta\epsilon_t/2=0.8\%$

 Figure 7. Fatigue crack propagation region for extruded Al-4.5Cu-0.6Mg-0.3Si(-0.3Ce) alloys with T6 state
 (a) Al-4.5Cu-0.6Mg-0.3Si alloy, $\Delta\epsilon_t/2=0.8\%$; (b) Al-4.5Cu-0.6Mg-0.3Si-0.3Ce alloy, $\Delta\epsilon_t/2=0.8\%$

D. Fatigue Fracture of Al-4.5Cu-0.6Mg-0.3Si(-0.3Ce) Alloys

Fatigue crack initiation region for extruded Al-4.5Cu-0.6Mg-0.3Si (-0.3Ce) alloys under the different plus total

strain amplitude with T6 state are shown in Figure 6. The crack initiation in the sample surfaces of Al-4.5Cu-0.6Mg-0.3Si (-0.3Ce) alloys are both in a manner of transgranular.

Fatigue crack propagation region for extruded Al-4.5Cu-0.6Mg-0.3Si (-0.3Ce) alloys with T6 state are shown in Figure 7. It can be seen that fatigue crack extend in the form of transgranular in the process of fatigue deformation.

IV. CONCLUSIONS

(1) Under low-cycle fatigue loading condition, the cyclic stress response behaviors of Al-4.5Cu-0.6Mg-0.3Si and Al-4.5Cu-0.6Mg-0.3Si-0.3Ce alloys mainly exhibit exhibit the cyclic strain hardening and cycle stability, the cyclic deformation resistance of Al-4.5Cu-0.6Mg-0.3Si alloy with T6 treated state is significantly improved when Ce is added.

(2) When the total strain amplitudes various from 0.4%~1.2%, the cyclic deformation resistance of Al-4.5Cu-0.6Mg-0.3Si-0.3Ce alloy is higher than the Al-4.5Cu-0.6Mg-0.3Si alloy.

(3) The plastic strain amplitude and elastic strain amplitude with reversals to failure of Al-4.5Cu-0.6Mg-0.3Si and Al-4.5Cu-0.6Mg-0.3Si-0.3Ce alloys follow the Coffin–Manson and Basquin laws.

(4) Under the condition of low cycle fatigue loading, the fatigue crack initiation of Al-4.5Cu-0.6Mg-0.3Si (-0.3Ce) alloys in both in a transgranular manner and extension in a transgranular manner the surface of the sample.

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