

# Fabrication and Catalytic Performance of Au/3DOM Fe<sub>2</sub>O<sub>3</sub> Catalysts for the Oxidative Removal of Toluene

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**Abstract**—Three-dimensionally ordered macroporous (3DOM) Fe<sub>2</sub>O<sub>3</sub> and 0.48–1.95 wt% Au/3DOM Fe<sub>2</sub>O<sub>3</sub> catalysts were prepared using the poly(methyl methacrylate)-templating and polyvinyl alcohol-protected reduction methods, respectively. It is found that the porous catalysts with a surface area of 45–46 m<sup>2</sup>/g were of a rhombohedral  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub> crystal structure, and Au nanoparticles (NPs) with a size of 4–6 nm were well dispersed on the 3DOM Fe<sub>2</sub>O<sub>3</sub> surface. The 1.95Au/3DOM Fe<sub>2</sub>O<sub>3</sub> sample possessed the best low-temperature reducibility and showed the highest catalytic activity ( $T_{50\%} = 162$  °C and  $T_{90\%} = 204$  °C at SV = 20,000 mL/(g h)) for toluene oxidation, which was associated with its well-dispersed and small sized Au NPs, good low-temperature reducibility, and strong interaction between Au NPs and 3DOM Fe<sub>2</sub>O<sub>3</sub>.

**Keywords**—three-dimensionally ordered macropore; iron oxide; supported gold catalyst; toluene oxidation; volatile organic compound

## I. INTRODUCTION

Most of volatile organic compounds (VOCs) are harmful to the atmosphere and human health. Catalytic oxidation is believed to be an effective pathway for the removal of VOCs, in which the catalyst plays a key role in determining the efficiency of such a process.

In the past years, oxidation of VOCs over transition metal oxide (e.g., Co<sub>3</sub>O<sub>4</sub>, Mn<sub>3</sub>O<sub>4</sub>, and Fe<sub>2</sub>O<sub>3</sub>)-supported precious metal catalysts has been studied. These materials are catalytically active for the oxidation of VOCs. For example, Wang et al. reported that the good catalytic performance for *o*-xylene oxidation of Pd/porous Co<sub>3</sub>O<sub>4</sub> was associated with the Pd particle size, oxidized Pd species, and oxygen vacancies in Co<sub>3</sub>O<sub>4</sub> [1]. Solsona et al. observed that the Au-deposited partially ordered mesoporous Co<sub>3</sub>O<sub>4</sub> catalysts were highly active for toluene oxidation [2]. Ji and coworkers found a strong morphological effect of Mn<sub>3</sub>O<sub>4</sub> nanocrystallites on catalytic performance of Au/Mn<sub>3</sub>O<sub>4</sub> for benzene combustion [3].

Fe<sub>2</sub>O<sub>3</sub> is an important catalytic material due to its low cost, non-toxicity, and high resistance to corrosion [4]. Although iron oxide is less active than cobalt or manganese oxide, it presents a high sintering temperature that can avoid deactivation. It was reported that the iron oxide catalysts showed moderate activity for the total oxidation of lower alkanes (e.g., propane and propene) at low temperatures [5].

The Fe<sub>2</sub>O<sub>3</sub>-supported noble metal catalysts were more active than those supported on other materials [6]. Gold nanoparticles (NPs) supported on reducible transition-metal oxides (e.g., Fe<sub>2</sub>O<sub>3</sub>) show good catalytic activities for VOCs oxidation. Simona et al. [7,8] examined the activities of the Au/Fe<sub>2</sub>O<sub>3</sub> catalysts for the oxidation of numerous VOCs (methanol, propanol, acetone, and toluene), and found that the highly dispersed Au NPs could activate the gas-phase oxygen molecules and undermine the strength of Fe–O bonds, thus improving the performance of the Fe<sub>2</sub>O<sub>3</sub>-supported Au samples.

Using the poly (methyl methacrylate) (PMMA) as hard template and methanol-ethyl glycol as solvent, Masahiro et al. [9] prepared the three-dimensionally ordered macroporous (3DOM) Fe<sub>2</sub>O<sub>3</sub> samples with a surface area of 13–57 m<sup>2</sup>/g. Previously, we used the PMMA-templating strategy to generate 3DOM Fe<sub>2</sub>O<sub>3</sub> materials with a surface area of 32–46 m<sup>2</sup>/g [10]. However, there have been no reports on the use of three-dimensionally ordered macroporous (3DOM) Fe<sub>2</sub>O<sub>3</sub>-supported gold catalysts for the oxidation of toluene. In this work, we report the fabrication of the Au/3DOM Fe<sub>2</sub>O<sub>3</sub> catalysts using the PMMA-templating and polyvinyl alcohol (PVA)-protected reduction methods and their catalytic performance for the oxidation of toluene.

## II. EXPERIMENTAL

### A. Catalyst Preparation

Well-packed monodisperse colloidal crystal template, PMMA microspheres with an average diameter of ca. 300 nm, was synthesized using the approach reported elsewhere [11]. The macroporous Fe<sub>2</sub>O<sub>3</sub> samples with crystalline mesoporous walls were fabricated using the dual templating strategy. In a typical synthesis, 10 mmol of Fe(NO<sub>3</sub>)<sub>3</sub>·9H<sub>2</sub>O and 1.0 g of P123 ( $M_{av.} = 5800$  g/mol) were dissolved in 10 mL of absolute EtOH or in 10 mL of anhydrous EG and MeOH mixed solution (EG/MeOH volumetric ratio = 3/2) under ultrasonic radiation (90 Hz), in which iron nitrate concentration of the resulting solution was 1 mol/L and the molar ratio of Fe/P123 was 232. 3.0 g of highly ordered PMMA microspheres was added and soaked by the above mixed solution. After the PMMA microspheres were thoroughly wetted, the excessive liquid was filtered via a Buchner funnel connected to vacuum (0.07 MPa). The obtained intermediate was dried in a desiccator using

anhydrous calcium chloride as desiccating agent (relative humidity < 50 %) at room temperature (RT) for 12 h, and calcined in air at a ramp of 1°C/min from RT to 300°C and kept at this temperature for 3 h, and then to 550°C at the same heating rate and maintained at this temperature for 3 h, thus obtaining the porous iron oxide products.

The 3DOM Fe<sub>2</sub>O<sub>3</sub>-supported gold NPs with different Au loadings (*x*Au/3DOM Fe<sub>2</sub>O<sub>3</sub>, theoretical gold loading *x* = 0.5, 1.0, and 2.0 wt%) were prepared using a polyvinyl alcohol (PVA)-protected reduction method. The typical preparation procedures are as follows: (i) The noble metal aqueous solution (0.01 mol/L) was in advance prepared with HAuCl<sub>4</sub> as noble metal source; (ii) a stoichiometric amount of the noble metal aqueous solution was first diluted with deionized water to be 1/50 of the original concentration, and a desired amount of PVA was then added to the above aqueous solution (Au/PVA mass ratio = 1.0: 1.5) in an ice-water bath under vigorous stirring for 10 min; (iii) after rapidly injecting the 0.1 mol/L NaBH<sub>4</sub> aqueous solution (Au/NaBH<sub>4</sub> molar ratio = 1.0 : 5.0) and continuously stirring for 20 min, a sol was obtained; (iv) a desired amount of the 3DOM Fe<sub>2</sub>O<sub>3</sub> support was added to the sol, and the obtained suspension was subjected to sonication (60 kHz) for 30 s. A N<sub>2</sub> bubble-assisted stirring operation was adopted to agitate the suspension for 10 h until complete adsorption of colloidal noble metals occurred; and (v) the solid was filtered, washed with 2.0 L of deionized water, dried at 80°C for 12 h, and calcined in air at a ramp of 1°C/min from RT to 550°C and maintained at this temperature for 3 h, thus obtaining the *x*Au/3DOM Fe<sub>2</sub>O<sub>3</sub> samples. The results of inductively coupled plasma atomic emission spectroscopic (ICP-AES, Thermo Electron IRIS Intrepid ER/S) studies show that the real Au loadings (*x*) in *x*Au/3DOM Fe<sub>2</sub>O<sub>3</sub> were 0.48, 0.97, and 1.95 wt%, respectively.

For comparison purposes, we also prepared a nonporous iron oxide sample (denoted as Fe<sub>2</sub>O<sub>3</sub>-Bulk) by calcining a certain amount of ferric nitrate in air at 650°C for 3 h and the 1.98Au/Fe<sub>2</sub>O<sub>3</sub>-Bulk sample by using the polyvinyl alcohol (PVA)-protected reduction method after calcination at 550°C for 3 h.

All of the chemicals (A.R. in purity) were purchased from Beijing Sinopharm Chemical Reagents Company and used without further purification.

### B. Catalyst Characterization

The real Au contents in the samples were measured using the inductively coupled plasma atomic emission spectroscopic (ICP-AES) technique on a Thermo Electron IRIS Intrepid ER/S spectrometer. The samples were dissolved in a mixture of concentrated HCl and HNO<sub>3</sub> with volumetric ratio of 3/1 prior to the analysis. X-ray diffraction (XRD) patterns of the samples were recorded on a Bruker D8 Advance diffractometer with Cu K $\alpha$  radiation and nickel filter ( $\lambda$  = 0.15406 nm). The Brunauer-Emmett-Teller surface areas of the samples were calculated on the basis of the N<sub>2</sub> adsorption-desorption isotherms obtained on a Micromeritics ASAP 2020 analyzer. The scanning electron microscopic (SEM) and transmission electron microscopic

(TEM) images of the samples were recorded on a Gemini Zeiss Supra 55 apparatus (operating at 10 kV) and a JEOL-2010 equipment (operating at 200 kV), respectively. Thermogravimetric analysis (TGA) and differential scanning calorimetric (DSC) analysis were conducted on a SDT Q600 (TA) apparatus in an air flow of 100 mL/min from room temperature to 700°C (heating rate: 10°C/min).

Hydrogen temperature-programmed reduction (H<sub>2</sub>-TPR) experiments were carried out on a chemical adsorption analyzer (Autochem II 2920, Micromeritics). Before TPR measurement, ca. 0.02 g of catalyst (40–60 mesh) was loaded to a quartz fixed-bed U-shaped microreactor (i.d. = 4 mm) and pretreated in an O<sub>2</sub> flow of 30 mL/min at 300°C for 1 h. After being cooled at the same atmosphere to RT, the pretreated sample was exposed to a flow (50 mL/min) of 5 % H<sub>2</sub>-95 % Ar (v/v) mixture and heated from RT to 600°C at a ramp of 10°C/min. The alteration in H<sub>2</sub> concentration of the effluent was monitored online by the chemical adsorption analyzer, and the H<sub>2</sub>-TPR profiles of the samples were obtained.

### C. Catalytic Activity Evaluation

Catalytic activities of the samples for the oxidation of toluene were tested in a continuous flow fixed-bed quartz microreactor (i.d. = 4 mm). In order to minimize the effect of hot spots, 0.25 g of quartz sands (40–60 mesh) was mixed with 50 mg of the catalyst (40–60 mesh). The catalyst was pretreated in 30 mL/min O<sub>2</sub> flow at 250°C for 1 h before the test. After being cooled to RT, the reactant mixture (1000 ppm toluene + O<sub>2</sub> + N<sub>2</sub> (balance)) with a flow rate of 16.7 mL/min was passed through the catalyst bed. The toluene/O<sub>2</sub> molar ratio was 1/400 and the space velocity (SV) was ca. 20,000 mL/(g h). We changed the catalyst mass for the alteration of SV. The reactants and products were analyzed online on a gas chromatograph (GC-2010, Shimadzu), equipped with a stabilwax@-DA column (30 m in length) for organic separation and a Carboxen 1000 column (3 m in length) for permanent gas separation.

## III. RESULTS AND DISCUSSION

### A. Crystal Structure, Morphology, and Surface Area

Figure 1 shows the XRD patterns of the samples. It is observed that the crystal structure of the as-obtained samples could be indexed to the rhombohedral  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub> phase (JCPDS PDF# 86-2368), as indicated in figure 1e. Similar results have been reported by other researchers [12, 13]. The loading of Au did not change the crystal structure of Fe<sub>2</sub>O<sub>3</sub>. The detection of a weak diffraction peak at  $2\theta = 38.5^\circ$  due to the Au (111) plane (JCPDS PDF# 04-0784) indicates the generation of cubic Au NPs in the 0.97Au/3DOM Fe<sub>2</sub>O<sub>3</sub>, 1.95Au/3DOM Fe<sub>2</sub>O<sub>3</sub>, and 1.98Au/Fe<sub>2</sub>O<sub>3</sub>-Bulk samples (Figure 1c–e). The difference in peak intensity suggests that the 3DOM-structured samples possessed a lower crystallinity than the bulk Fe<sub>2</sub>O<sub>3</sub> supported Au sample.

Figure 2 shows the representative SEM images of the porous samples. It can be seen that the Fe<sub>2</sub>O<sub>3</sub> and its supported Au samples displayed a high-quality 3DOM architecture, with the typical macropore sizes being 140–180

nm. The loading of Au NPs did not induce a significant alteration in particle morphology. Figure 3 shows the TEM images of the porous samples. It is observed that the Au NPs

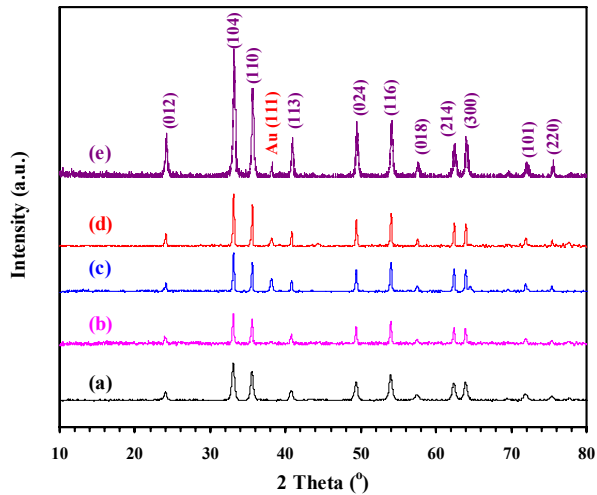


Figure 1. XRD patterns of (a) 3DOM  $\text{Fe}_2\text{O}_3$ , (b) 0.48Au/3DOM  $\text{Fe}_2\text{O}_3$ , (c) 0.97Au/3DOM  $\text{Fe}_2\text{O}_3$ , (d) 1.95Au/3DOM  $\text{Fe}_2\text{O}_3$ , and (e) 1.98Au/ $\text{Fe}_2\text{O}_3$ -Bulk.

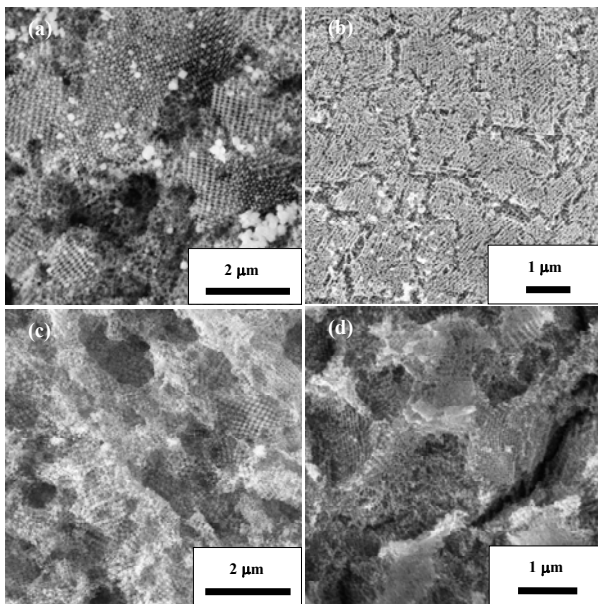


Figure 2. SEM images of (a) 3DOM  $\text{Fe}_2\text{O}_3$ , (b) 0.48Au/3DOM  $\text{Fe}_2\text{O}_3$ , (c) 0.97Au/3DOM  $\text{Fe}_2\text{O}_3$ , and (d) 1.95Au/3DOM  $\text{Fe}_2\text{O}_3$ .

were well dispersed on the surface of 3DOM  $\text{Fe}_2\text{O}_3$ . The average Au NP diameter of each sample was calculated by making a statistic analysis on the sizes of more than 200 Au NPs in the TEM images. The average Au particle sizes of the 0.48Au/3DOM  $\text{Fe}_2\text{O}_3$ , 0.97Au/3DOM  $\text{Fe}_2\text{O}_3$ , 1.95Au/3DOM  $\text{Fe}_2\text{O}_3$ , and 1.98Au/ $\text{Fe}_2\text{O}_3$ -Bulk samples were 6, 5, 4, and 12 nm, respectively. Surface areas of the 3DOM  $\text{Fe}_2\text{O}_3$  and  $x\text{Au}/3\text{DOM } \text{Fe}_2\text{O}_3$  ( $x = 0.48, 0.97,$  and  $1.95$  wt %) samples were 46.2, 45.1, 45.3, and 44.9  $\text{m}^2/\text{g}$ , respectively, whereas that of the 1.98Au/ $\text{Fe}_2\text{O}_3$ -Bulk sample was 7.6  $\text{m}^2/\text{g}$ .

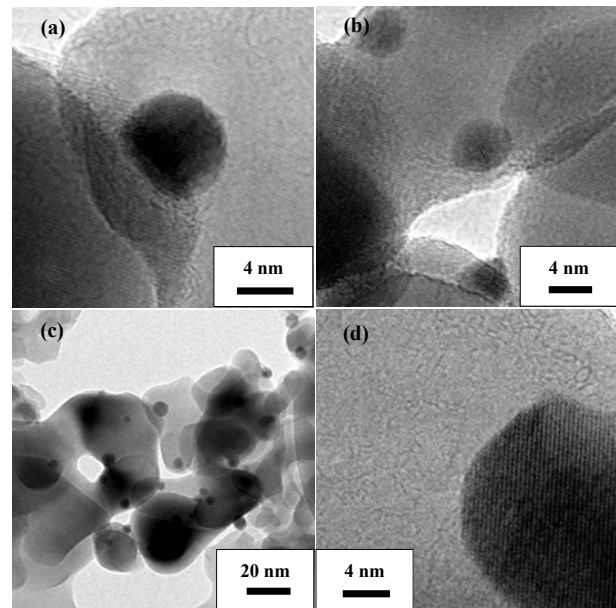


Figure 3. TEM images of (a) 0.48Au/3DOM  $\text{Fe}_2\text{O}_3$ , (b) 0.97Au/3DOM  $\text{Fe}_2\text{O}_3$ , (c) 1.95Au/3DOM  $\text{Fe}_2\text{O}_3$ , and (d) 1.98Au/ $\text{Fe}_2\text{O}_3$ -Bulk.

### B. Thermal Stability

To examine the thermal stability, we carried out the TGA/DTA experiment of the 3DOM  $\text{Fe}_2\text{O}_3$  precursor. Figure 4 illustrates the TGA/DTA profiles of the 3DOM  $\text{Fe}_2\text{O}_3$  sample before calcination. It is observed that there were weight losses of ca. 8.9 and 88.8 wt% in the temperature range of 30–160 and 160–375°C, accompanying by the appearance of well-resolved endothermic signals centered at 134 and 366°C, respectively. The two weight losses could be attributed to the removal of adsorbed water or organics (EtOH, EG, and MeOH) and the decomposition of  $\text{Fe}(\text{NO}_3)_3$  [14] as well as the oxidation of PMMA [9,11]. The result clearly demonstrates that calcining the sample intermediate above 550°C was appropriate to generate the  $\text{Fe}_2\text{O}_3$  crystals.

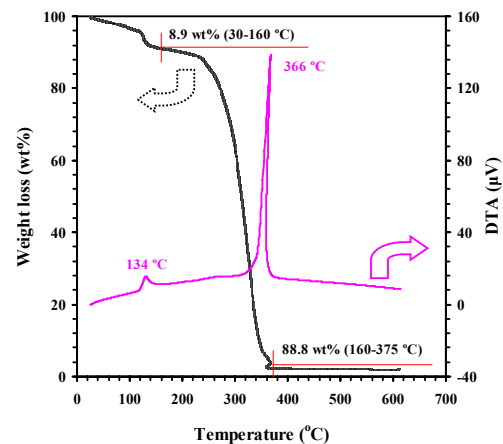


Figure 4. TGA/DTA profiles of the 3DOM  $\text{Fe}_2\text{O}_3$  sample before calcination.



### C. Reducibility

Reducibility of a transition metal oxide is highly related to its catalytic performance. Usually, the reduction of iron oxide proceeds via the order of  $\text{Fe}_2\text{O}_3 \rightarrow \text{Fe}_3\text{O}_4 \rightarrow \text{Fe}^0$  [15, 16]. Figure 5 illustrates the  $\text{H}_2$ -TPR profiles of the as-fabricated samples. For each sample, two reduction steps were clearly observed in the range of 30–300 and 300–600°C. The first step was due to the removal of adsorbed oxygen species and the reduction of oxidized gold ( $\text{Au}^{\text{ox}}$ ) species and  $\text{Fe}_2\text{O}_3$  to  $\text{Au}^0$  and  $\text{Fe}_3\text{O}_4$  [17,18], respectively, whereas the second step was due to the reduction of  $\text{Fe}_3\text{O}_4$  to  $\text{Fe}^0$  [15,17,18]. With the rise in Au loading from 0.48 to 1.95-wt%, the reduction peaks shifted to lower temperatures (especially temperature of the first reduction peak decreased

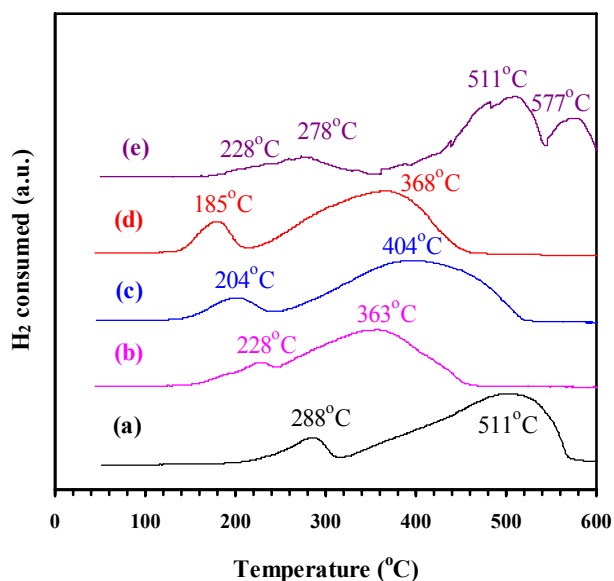


Figure 5.  $\text{H}_2$ -TPR profiles of (a) 3DOM  $\text{Fe}_2\text{O}_3$ , (b) 0.48Au/3DOM  $\text{Fe}_2\text{O}_3$ , (c) 0.97Au/3DOM  $\text{Fe}_2\text{O}_3$ , (d) 1.95Au/3DOM  $\text{Fe}_2\text{O}_3$ , and (e) 1.98Au/ $\text{Fe}_2\text{O}_3$ -Bulk.

to 185°C for the 1.95Au/3DOM  $\text{Fe}_2\text{O}_3$  sample), indicating that the loading of Au NPs improved the low-temperature reducibility. On the other hand, the shift in reduction temperature also suggests the presence of a strong interaction between Au NPs and 3DOM  $\text{Fe}_2\text{O}_3$ . The 1.98Au/ $\text{Fe}_2\text{O}_3$ -Bulk sample showed four reduction peaks at 228, 278, 511, and 577°C: the former two were the removal of adsorbed oxygen species and the reduction of  $\text{Au}^{\text{ox}}$  to  $\text{Au}^0$  and  $\text{Fe}_2\text{O}_3$  to  $\text{Fe}_3\text{O}_4$  [17, 18], while the latter two were the reduction of  $\text{Fe}_3\text{O}_4$  to  $\text{Fe}^0$  [15,17,18]. From the  $\text{H}_2$ -TPR results, one can realize that the 1.95Au/3DOM  $\text{Fe}_2\text{O}_3$  sample exhibited the best low-temperature reducibility. The low-temperature reducibility increased in the order of 3DOM  $\text{Fe}_2\text{O}_3 < 0.48\text{Au}/3\text{DOM } \text{Fe}_2\text{O}_3 < 1.98\text{Au}/\text{Fe}_2\text{O}_3\text{-Bulk} < 0.97\text{Au}/3\text{DOM } \text{Fe}_2\text{O}_3 < 1.95\text{Au}/3\text{DOM } \text{Fe}_2\text{O}_3$ .

### D. Catalytic Performance

Under the conditions of toluene concentration = 1000 ppm, toluene/ $\text{O}_2$  molar ratio = 1/400, SV = 20,000 mL/(g h),

and temperature < 400°C, no significant conversion of toluene was detected over the quartz sands loaded in the microreactor. That is to say, the complete oxidation of toluene over the present catalysts was a catalytic process. Figure 6 shows the catalytic activities of the samples for toluene oxidation. It is observed that toluene conversion increased

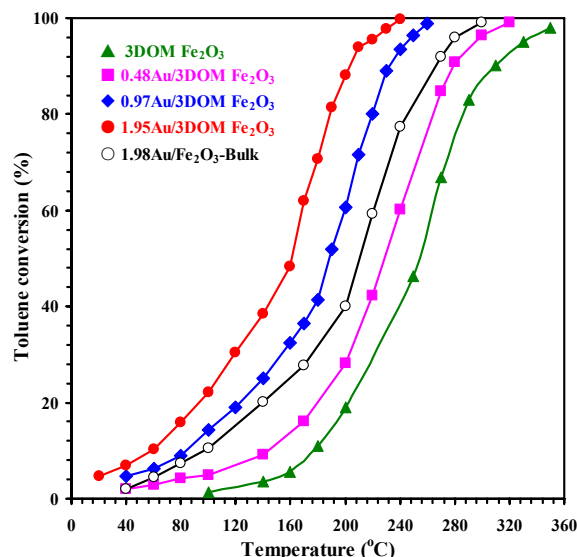


Figure 6. Toluene conversion versus reaction temperature over the as-prepared samples under the conditions of toluene concentration = 1000 ppm, toluene/ $\text{O}_2$  molar ratio = 1/400, and SV = 20,000 mL/(g h).

TABLE I. CATALYTIC ACTIVITIES OVER THE AS-PREPARED SAMPLES UNDER THE CONDITIONS OF TOLUENE CONCENTRATION = 1000 ppm, TOLUENE/ $\text{O}_2$  MOLAR RATIO = 1/400, AND SV = 20,000 mL/(g h).

Sample	Toluene oxidation activity (°C)		
	$T_{10\%}$	$T_{50\%}$	$T_{90\%}$
3DOM $\text{Fe}_2\text{O}_3$	180	256	311
0.48Au/3DOM $\text{Fe}_2\text{O}_3$	146	230	280
0.97Au/3DOM $\text{Fe}_2\text{O}_3$	88	190	236
1.95Au/3DOM $\text{Fe}_2\text{O}_3$	60	162	204
1.98Au/ $\text{Fe}_2\text{O}_3$ -Bulk	100	212	268

with a rise in temperature. For better comparison purposes, the reaction temperatures  $T_{10\%}$ ,  $T_{50\%}$ , and  $T_{90\%}$  (corresponding to toluene conversion = 10, 50, and 90%) were summarized in Table I. The  $T_{10\%}$ ,  $T_{50\%}$ , and  $T_{90\%}$  were 180, 256, and 311°C over the 3DOM  $\text{Fe}_2\text{O}_3$  sample, respectively. Previously,  $\text{Fe}_2\text{O}_3$  was employed as catalyst for the removal of toluene. For example, Scirè and coworkers observed a  $T_{90\%}$  of 380°C over  $\text{Fe}_2\text{O}_3$  for toluene oxidation at SV = 186 mL/(g h) [8]. Duran et al. reported that 80% toluene conversion could be achieved over  $\text{Fe}_2\text{O}_3$  at 365°C and 20,000 mL/(g h) [19]. Therefore, our 3DOM  $\text{Fe}_2\text{O}_3$  sample outperformed the  $\text{Fe}_2\text{O}_3$  samples reported above [8, 19]. With the loading of Au NPs, the catalytic activity was much improved. Over the

1.98Au/Fe<sub>2</sub>O<sub>3</sub>-Bulk sample, the  $T_{10\%}$ ,  $T_{50\%}$ , and  $T_{90\%}$  were 100, 212, and 268°C, respectively. Obviously, the 1.95Au/3DOM Fe<sub>2</sub>O<sub>3</sub> sample performed the best:  $T_{10\%}$  = 60°C,  $T_{50\%}$  = 162°C, and  $T_{90\%}$  = 204°C. Therefore, the catalytic activity increased in the order of 3DOM Fe<sub>2</sub>O<sub>3</sub> < 0.48Au/3DOM Fe<sub>2</sub>O<sub>3</sub> < 1.98Au/Fe<sub>2</sub>O<sub>3</sub>-Bulk < 0.97Au/3DOM Fe<sub>2</sub>O<sub>3</sub> < 1.95Au/3DOM Fe<sub>2</sub>O<sub>3</sub>, coinciding with the sequence in low-temperature reducibility of these samples (Figure 5). The catalytic activity of the 1.95Au/3DOM Fe<sub>2</sub>O<sub>3</sub> sample was much better than that sample ( $T_{50\%}$  = 200°C and  $T_{90\%}$  = 260°C at SV = 20,000 mL/(g h)) of the 6.55Au/Fe<sub>2</sub>O<sub>3</sub> nanodisk sample reported in the literature [20].

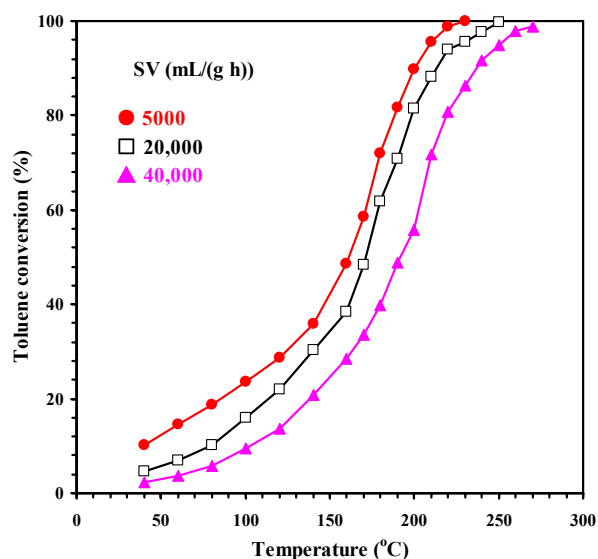


Figure 7. Effect of SV on the catalytic activity over the 1.95Au/3DOM Fe<sub>2</sub>O<sub>3</sub> sample.

Due to the presence of strong interaction between Au NPs and Fe<sub>2</sub>O<sub>3</sub>, partial Au<sup>0</sup> might react with Fe<sup>3+</sup> to generate Au<sup>δ+</sup> and Fe<sup>2+</sup> species, causing the surface Fe<sup>2+</sup> and Au<sup>δ+</sup> concentrations to increase. According to the electroneutrality principle, an increase in Fe<sup>2+</sup> content can give a rise in amount of oxygen vacancies (Table I). The generation of surface oxygen vacancies facilitates the activation of gas-phase oxygen molecules and the easy replenishment of adsorbed oxygen (O<sub>ads</sub>) species. The oxidation of organic compounds usually proceeds through the interaction of organic compounds with O<sub>ads</sub> species at oxygen vacancies. During the oxidation process of toluene over xAu/Fe<sub>2</sub>O<sub>3</sub>, the reduction of transition metal ions was associated with the reducibility of the samples, and the generation of oxygen vacancies took place concurrently. That is to say, an enhancement in reducibility would be beneficial for the generation of oxygen vacancies, and then for the activation of gas-phase oxygen molecules and the replenishment of O<sub>ads</sub> species. Therefore, it is understandable that the better low-temperature reducibility led to better catalytic performance in the present study. There are several kinds of active sites (noble metal, transition metal oxide, and interfaces between

noble metal and transition metal oxide) in the reducible metal oxide-supported noble metal catalysts. As we know, the Au particle size is an important factor influencing catalytic activity of a supported Au sample [21]. In the present study, the average size of Au NPs in 1.95Au/3DOM Fe<sub>2</sub>O<sub>3</sub> was 4 nm, whereas that in 1.98Au/Fe<sub>2</sub>O<sub>3</sub>-Bulk was 12 nm. Therefore, it is understandable that the 1.95Au/3DOM Fe<sub>2</sub>O<sub>3</sub> sample performed better than 1.98Au/Fe<sub>2</sub>O<sub>3</sub>-Bulk for toluene oxidation. Figure 7 shows the effect of SV on catalytic activity of the 1.95Au/3DOM Fe<sub>2</sub>O<sub>3</sub> sample. It is observed that toluene conversion increased with the drop in SV, which might be a result due to the elongation of contact time between reactant molecules and catalyst.

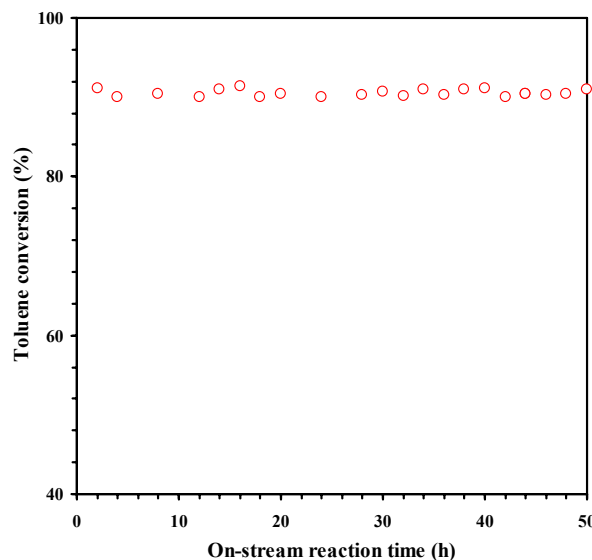


Figure 8. Toluene conversion as a function of on-stream reaction time over the 1.95Au/3DOM Fe<sub>2</sub>O<sub>3</sub> sample at 204°C and SV = 20,000 mL/(g h).

In order to evaluate the catalytic stability, 50-h on-stream toluene oxidation experiment at 204°C over the 1.95Au/3DOM Fe<sub>2</sub>O<sub>3</sub> sample was carried out. Under the adopted reaction conditions, no significant loss in catalytic activity was detected within 50 h of on-stream reaction (Figure 8), demonstrating the 1.95Au/3DOM Fe<sub>2</sub>O<sub>3</sub> sample was catalytically durable.

#### IV. CONCLUSIONS

3DOM Fe<sub>2</sub>O<sub>3</sub> and 0.48–1.95Au/3DOM Fe<sub>2</sub>O<sub>3</sub> catalysts were prepared using the PMMA-templating and PVA-protected reduction methods, respectively. The 3DOM Fe<sub>2</sub>O<sub>3</sub> and 0.48–1.95Au/3DOM Fe<sub>2</sub>O<sub>3</sub> catalysts possessed a rhombohedral  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub> crystal structure and a surface area of 45–46 m<sup>2</sup>/g. Au NPs with a size of 4–6 nm were highly dispersed on the surface of 3DOM Fe<sub>2</sub>O<sub>3</sub>. Catalytic activity for toluene oxidation enhanced with the loading of Au NPs, with the 1.95Au/3DOM Fe<sub>2</sub>O<sub>3</sub> sample showing the highest catalytic activity ( $T_{50\%}$  = 162°C and  $T_{90\%}$  = 204°C at SV = 20,000 mL/(g h)). It is concluded that the good catalytic performance of 1.95Au/3DOM Fe<sub>2</sub>O<sub>3</sub> was associated with its

highly dispersed Au NPs and better low-temperature reducibility as well as the strong interaction between Au NPs and 3DOM Fe<sub>2</sub>O<sub>3</sub>.

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