

# Absorption of Sulfur Dioxide in Ionic Liquid Supported on Porous Silica Particles

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**Abstract**—1, 1, 3, 3-tetramethylguanidinium lactate (TMGL) has been studied for SO<sub>2</sub> removal. However, before using industrial scale application, several problems need to be solved, for example, the influence on SO<sub>2</sub> absorption at high temperature. This work investigates the SO<sub>2</sub> sorption of the 1, 1, 3, 3-tetramethylguanidinium lactate (TMGL) immobilized on porous silica particles under the conditions of low SO<sub>2</sub> concentration. The effects of SO<sub>2</sub> concentration and environment temperature were evaluated. The attained results clearly imply that both of them have significant influence on absorption performance. The SO<sub>2</sub> absorption capacity reduced as the SO<sub>2</sub> concentration decreased and the environment temperature increased.

**Keywords**-supported ionic liquids; desulfurizer; sulfur dioxide; absorption capacity

## I. INTRODUCTION

Sulfur dioxide is one of the important air pollutants, leading to a serious problem and has drawn much attention throughout the world. [1-6] Ionic liquids were found to be key absorbents, due to negligible volatility, high thermal and chemical stability, and tunable chemical properties, which have been widely used in gas separation. For instance, Han et al. [7] first synthesized a base-functionalized IL, 1, 1, 3, 3-tetramethylguanidinium lactate (TMGL), and reported that it can effectively absorb SO<sub>2</sub> from a simulated flue gas with high absorption capacity (0.978 mol SO<sub>2</sub>/mol TMGL) and high selectivity. From then, various ionic liquids were explored for SO<sub>2</sub> capture.

Consider of the application of ionic liquids in industry, there are many problems need to be investigated.

(1)The high viscosity was the fatal weakness for SO<sub>2</sub> removal by TMGL. To overcome this problem, Li et al. [8, 9] synthesized poly (1, 1, 3, 3-tetramethylguanidine acrylate) (PTMGA) and crosslinked porous copolymer particles. Unfortunately, their internal pore structures would be collapsed or mostly lost after many cycles of SO<sub>2</sub> sorption. Subsequently, Li et al. [10] immobilized TMGL to porous silica (SiO<sub>2</sub>) particles, which provided large gas-solid interface. They reported that it is an effective way to improve the absorption rate and capacity (1.9 mol SO<sub>2</sub>/mol TMGL with pure SO<sub>2</sub>) of TMGL. However, the absorption capacity (0.48 mol SO<sub>2</sub>/mol TMGL) decreased dramatically when the flow gas was mixture gas containing SO<sub>2</sub> of 2160ppm.

(2)The real flue gas is not only a simple combination of

N<sub>2</sub> and SO<sub>2</sub>. In addition, the concentration of SO<sub>2</sub> emitting from flue gas is not very high, always around 2000ppm. Severa et al. [11] has reported the SO<sub>2</sub> sorption by loading ionic liquid on activated carbon sorbents under simulated atmospheric conditions, and proved the importance of testing the performance of the ionic liquid absorption of SO<sub>2</sub> under simulated real world conditions.

(3)The temperature of flue gas is very high when it just emitted. A systematic research about the influence on the SO<sub>2</sub> absorption by TMGL at high temperature is not reported.

In this study, the SO<sub>2</sub> absorption performance by TMGL loaded porous silica (TMGL/SiO<sub>2</sub>) at relatively low SO<sub>2</sub> concentration range (below 5000ppm) and temperature was being investigated.

## II. EXPERIMENTAL SECTION

### A. Materials

1,1,3,3-tetramethylguanidinium (TMG, ≥99.0%, Aladdin Co., LTD., China), L-lactic acid (86%, Sigma-aldrich (Wuxi) Life Science & Technology Co., LTD., China) and silica particles (SiO<sub>2</sub>, particle diameter range is 150~280 μm, Sigma-aldrich Co., USA), nitrogen (N<sub>2</sub>, ≥99.0%, Wenzhou Changsheng gas Co., LTD., China), and N<sub>2</sub>/SO<sub>2</sub> mixture gas with 2.60% SO<sub>2</sub> (Changzhou Jinghua industrial gas Co., LTD., China)

### B. Preparation and Characterization of TMGL/SiO<sub>2</sub>

TMGL/SiO<sub>2</sub> with different immobilization ratio was prepared through the impregnation-vaporization process<sup>[10]</sup>, and the TMGL/SiO<sub>2</sub> ratio  $x/1$  was expressed as TMGL/SiO<sub>2</sub>- $x/1$ , equal to the TMGL/SiO<sub>2</sub> feed ratio  $x/1$ .

TMGL/SiO<sub>2</sub>- $x/1$  and TMGL were characterized by Thermal Gravimetric Analyzer (TGA). The samples were heated to 600 °C in 10 °C/min under nitrogen. A Micromeritics ASAP 2020 instrument was used to obtain properties of particles, including the pore size distribution, pore volume, and surface area.

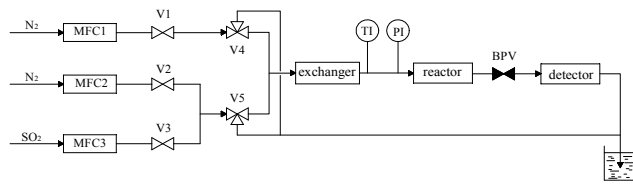
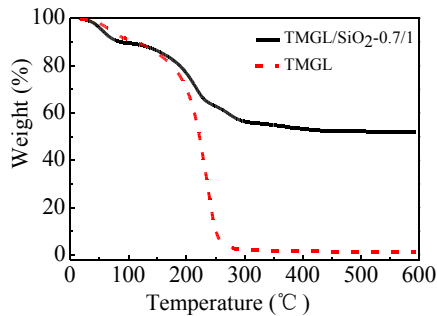


Figure 1. Experimental Setup.

Figure 2. TGA curves of the TMGL/SiO<sub>2</sub>-0.7/1 and TMGL.

### C. Absorption Experiment

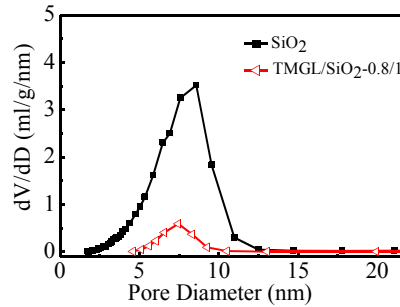
The prepared particles with different loadings (TMGL/SiO<sub>2</sub>-x/1) were used in the sorption experiments. The simulated flue gas with different SO<sub>2</sub> concentration and total flow rate were controlled by changing N<sub>2</sub> and SO<sub>2</sub> mass flowmeters. The mixture gas flowed through the Modular Microreaction System (OI-MMRS 01.2009, Ehrfeld Mikrotechnik BTS GmbH, Germany), involving coax heat exchanger, pressure sensor module, and temperature sensor module and cartridge reactor. After sorption, the mixture gas flowed through the Bruker Alpha FT-IR Spectrometer (Bruker Optik Asia Pacific Limited, Germany) for the determination of SO<sub>2</sub> concentration. The experimental setup is shown in Figure 1.

Due to scarcely absorb N<sub>2</sub> on TMGL [12], in this work N<sub>2</sub> was used as carrier gas and the effect of N<sub>2</sub> on absorption performance was neglected. Step 1, valve 1 and 4 opened for the N<sub>2</sub> gas passed the experiment setup. Then, the sorbents with the same volume were filled in the reactor, while controlling the temperature by using circulating water bath connected to the heat exchanger. Step 2, valve 2, 3 and 5 were opened (with valve 1 and 4 closed), the mixture gas with a certain SO<sub>2</sub> concentration flowed into the system, while the change in the SO<sub>2</sub> concentration was measured and recorded by the flue gas analyzer.

## III. RESULTS AND DISCUSSION

### A. Characterization

The prepared particles with different TMGL loadings and TMGL were investigated by TGA to get their weight ratio,

Figure 3. Pore size distribution of SiO<sub>2</sub>, TMGL/SiO<sub>2</sub>-0.8/1.

shown in Figure 2. Compared with the TGA curve of the TMGL, the weight loss was about 36% between 130 °C and 350 °C as the TGA curve of the TMGL/SiO<sub>2</sub>-0.7/1 sample shown, which can be considered as the decomposition of TMGL. Obviously, the change of the weight was correlated with the TMGL/SiO<sub>2</sub> feed ratio.

Figure 3 showed the particle size distribution of porous silica and TMGL/SiO<sub>2</sub>-0.8/1. Obviously, the pore diameter of sorbents decreased after TMGL was immobilized on SiO<sub>2</sub>.

### B. Effect of SO<sub>2</sub> Concentration on Absorption Performance of TMGL/SiO<sub>2</sub>

Different SO<sub>2</sub> concentrations (0.1%, 0.2%, 0.3%, 0.4%, 0.5%) and total flow rate of 200 ml/min was controlled by N<sub>2</sub> mass flowmeter and SO<sub>2</sub> mass flowmeter. The temperature of the water bath was set to 45 °C, TMGL/SiO<sub>2</sub>-0.2/1 and TMGL/SiO<sub>2</sub>-0.4/1 were used as sorbents, the effect of SO<sub>2</sub> concentration as shown in Figure 4.

As seen in the breakthrough curves, with the increase of SO<sub>2</sub> concentrations, the absorption rate showed an upward trend. It is more obvious for TMGL/SiO<sub>2</sub>-0.4/1, with the SO<sub>2</sub> concentration increased from 0.1% to 0.5%, the breakthrough time reduced from 50 min to 15 min.

The degree of difficulty to reach phase equilibrium ( $t_{0.9}$ ) was proposed by Chen et al. [13] to evaluate the absorption kinetics. In this work,  $t_{0.9}$  and the SO<sub>2</sub> absorption capacity were calculated, shown in Table I. It is obvious that the SO<sub>2</sub> absorption capacity of TMGL/SiO<sub>2</sub>-0.2/1 and TMGL/SiO<sub>2</sub>-0.4/1 increased as the SO<sub>2</sub> concentration increased. In contrast, the value of  $t_{0.9}$  gradually reduced with the increase of SO<sub>2</sub> concentration, which was more obvious for the higher TMGL/SiO<sub>2</sub> ratio. Under the same SO<sub>2</sub> concentration, the absorption capacity of TMGL/SiO<sub>2</sub>-0.4/1 was always bigger than that of TMGL/SiO<sub>2</sub>-0.2/1.



Figure 4. Effect of  $\text{SO}_2$  concentration on absorption performance of TMGL/SiO<sub>2</sub>-0.2/1 (a), TMGL/SiO<sub>2</sub>-0.4/1 (b).

TABLE I. THE RESULTS OF  $\text{SO}_2$  SORPTION UNDER THE DIFFERENT  $\text{SO}_2$  CONCENTRATION

Concentration (%)	$\text{SO}_2$ Absorption Capacity (AC) and the degree of difficulty to reach phase equilibrium ( $t_{0.9}$ )			
	TMGL/SiO <sub>2</sub> -0.2/1		TMGL/SiO <sub>2</sub> -0.4/1	
	AC (mol SO <sub>2</sub> / mol TMGL)	$t_{0.9}$ (min)	AC (mol SO <sub>2</sub> / mol TMGL)	$t_{0.9}$ (min)
0.1	0.1170	12.6	0.2644	48.0
0.2	0.2173	11.0	0.3148	29.2
0.3	0.2292	7.8	0.3410	21.7
0.4	0.2542	6.2	0.3534	17.3
0.5	0.2749	5.7	0.3729	14.9

### C. Effect of Temperature on Absorption Performance of TMGL/SiO<sub>2</sub>

The effect of environment temperature on  $\text{SO}_2$  sorption was studied by setting up the circulating water bath temperature whilst maintaining the  $\text{SO}_2$  concentration (0.4%) and the total flow rate (500 ml/min) constant, shown in Figure 5. For the different sorbent (TMGL/SiO<sub>2</sub>-0.6/1, TMGL/SiO<sub>2</sub>-0.8/1), the rate of  $\text{SO}_2$  sorption increased as the temperature increased. The absorption performance indicates that chemical absorption involved in the process of  $\text{SO}_2$  sorption.

However, as seen in Table II, with the environment temperature increased from 30 °C to 80 °C, the  $\text{SO}_2$  absorption capacity dropped by 30% at least. In addition, controlled the experimental conditions unchanged, the different between TMGL/SiO<sub>2</sub>-0.6/1 and TMGL/SiO<sub>2</sub>-0.8/1 are not obvious on the value of absorption capacity. The absorption performance can be explained by the different pore characteristics with the TMGL/SiO<sub>2</sub> ratio changed.

## IV. CONCLUSION

In this work, the  $\text{SO}_2$  sorption performance on TMGL/SiO<sub>2</sub> under different conditions was investigated, including the  $\text{SO}_2$  concentration and the environment temperature. Compared to the results reported in the literature for the capacity of TMGL/SiO<sub>2</sub> reached 1.9 mol  $\text{SO}_2$  per mol TMGL with pure  $\text{SO}_2$  gas, the absorption capacity significantly is smaller under the condition of the low  $\text{SO}_2$  concentration. Results under different temperature suggest that the significant effect of temperature on the  $\text{SO}_2$  absorption performance. Therefore, the  $\text{SO}_2$  absorption by

TMGL/SiO<sub>2</sub> under the high temperature should be avoided. It should be pointed out that further work need be carried. For example, the real flue gas is not only involve  $\text{SO}_2$  with low concentration, but also other gases included, such as  $\text{NO}_x$ ,  $\text{CO}$ , which may have influence on the  $\text{SO}_2$  absorption behavior.

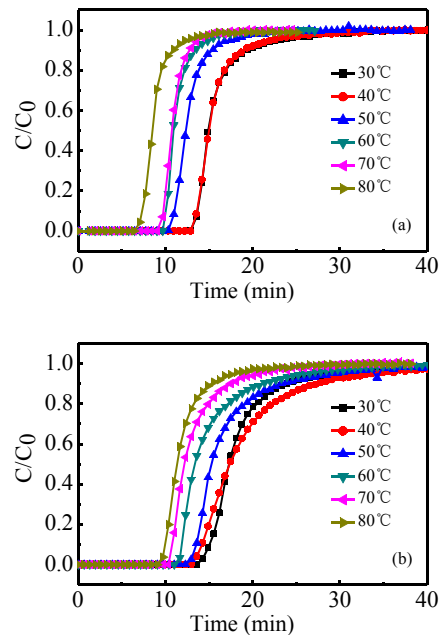


Figure 5. Effect of temperature on absorption performance of TMGL/SiO<sub>2</sub>-0.6/1 (a), TMGL/SiO<sub>2</sub>-0.8/1 (b).

TABLE II. THE RESULTS OF SO<sub>2</sub> SORPTION IN DIFFERENT TEMPERATURE

Temperature (°C)	SO <sub>2</sub> Absorption Capacity (AC) and the degree of difficulty to reach phase equilibrium (t <sub>0.9</sub> )			
	TMGL/SiO <sub>2</sub> -0.6/1		TMGL/SiO <sub>2</sub> -0.8/1	
	AC (mol SO <sub>2</sub> / mol TMGL)	t <sub>0.9</sub> (min)	AC (mol SO <sub>2</sub> / mol TMGL)	t <sub>0.9</sub> (min)
30	0.4777	14.7	0.4229	18.2
40	0.4445	14.7	0.4848	21.4
50	0.3833	11.9	0.3809	18.5
60	0.3605	10.4	0.3541	16
70	0.3004	10.0	0.3129	13
80	0.2724	8.4	0.2803	11.5

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