

Research on Gearbox Fault Detection and Diagnosis Based on Improved Spectral Kurtosis Algorithm

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Abstract—A gearbox fault detection and diagnosis test table of wheeled armored vehicles is designed and established. Typical faults and vibration experiments can be preset. Aiming to the d that traditional spectral kurtosis algorithm cannot be applied to gearbox fault signal feature extraction under strong noise interference, the minimum entropy deconvolution theory is adopted, and a new kind of gearbox fault diagnosis method based on MED and FSK is proposed, which realizes the single fault diagnosis of gears and bearings at different speed conditions, and also achieves good result for composite fault diagnosis of rolling bearing inner and outer rings. Compared with the traditional method of wavelet analysis and EMD, the proposed method for gearbox vibration signal has better noise reduction result.

Keywords—spectral kurtosis; minimum entropy deconvolution; gearbox; fault detection; fault diagnosis

I. INTRODUCTION

Gearbox is the important transmission device of mechanical equipments. It has complicated internal structure and high assembly accuracy. Because of the formidable working conditions, the fault rate of gearbox is high and the corresponding fault influence is enormous. Spectral kurtosis is a kind of signal transaction method to detect the ballistic part in signal. Its basic principle is computing the durtosis value of every spectral line and reflecting the transient ballistic corresponding to different durtosis value. Because of the rather large interference of working condition to gearbox's vibration signals, the signal extraction effectiveness of traditional spectral kurtosis algorithm for low SNR signal is not obvious^{[1][2]}. In this paper, the minimum entropy deconvolution theory is adopted and a new kind of gearbox fault detection and diagnosis method based on minimum entropy deconvolution and rapid spectral kurtosis algorithm is put forward. It retains the advantages of traditional spectral kurtosis algorithm to extract the signal characteristics by adaptive band-pass filter parameter selection. The credibility is verified by gearbox's single fault diagnosis test and bearing inward-outward ring compound fault diagnosis test.

II. GEARBOX FAULT DETECTION AND DIAGNOSIS TEST

In the fault diagnosis process of gearbox, the signals of normal state are relative easy to collect. But in practical engineering, there are many types of gearbox's fault. Especially, weak faults after complex transmission require optimal

measuring stations for sensors. Gearbox usually adopt sealed structure and is difficult to install sensors and collect fault signals. To collect sufficient fault signals for fault detection diagnosis, a gearbox fault diagnosis test table is established. Typical faults can be located based on the test table to explore and verify the corresponding gearbox fault diagnosis method.

A. Composition of Test Table

The test table of gearbox fault detection and diagnosis is composed of electromagnetic variable-speed motor, second-level decelerator, clutch, sensors, direct-current power, magnetic-particle brake and signal collection instrument. The test table composition is shown as Figure I.



FIGURE I. THE TEST TABLE COMPOSITION OF GEARBOX FAULT DETECTION AND DIAGNOSIS

TABLE I. COMPOSITION OF GEARBOX TEST TABLE

<i>Name</i>	<i>Type</i>	<i>Number</i>
Electromagnetic variable-speed motor	YCT180-4A	1
Gearbox	200	1
Clutch		2
Magnetic-particle brake	FZJ-5	1
Direct-current power	WLY-1A	1
Rotation speed and rotation torque sensor	JN338	1
Vibration acceleration sensor	B&K4506	4
Synergy signal collection instrument	PH16H	1
Power distribution box	XL-3-2	1

In the gearbox's working process, the rotation speed is controlled by electromagnetic variable-speed motor, the load of magnetic-particle brake can be adjusted by the direct-current power to realize different rotation speed and different load. In the signal collection process, the sensor of B&K4506 is located on the surface of gearbox, the sensor signals of vibration acceleration, rotation speed and rotation torque are recorded by data collection instrument of SynergyPH16H. The detailed composition of gearbox test table is shown as Table I.

Same time interval sampling method is adopted to collect the vibration response signals. The control device of electromagnetic variable-speed motor adjusts the rotation speed of gearbox. So the collection of vibration acceleration signals under different rotation speeds can be realized. In order to research the fault process of gears and bearings, the sensors are installed in the intermediate shaft, output shaft and bearing bases.

In the signal collection process, set the sampling frequency as 10kHz, adjust the motor speed by the control device of electromagnetic variable-speed motor, measure the rotation speed of the gearbox's input shaft by rotation speed and torque sensors. The Synergy signal collection instrument has five channels. The CH1 channel is connected with JN338 rotation speed and torque sensor to collect the rotation speed signal of gearbox's input shaft. Other four channels are connected with four vibration acceleration sensor. The signal collection process should begin after the gearbox is working smoothly and steadily.

III. TRADITIONAL SPECTRUAL KURTOSIS THEORY

Spectral kurtosis theory was used to analyze the instantaneous impact composition in gear and bearing vibration signals firstly. Carry out Cramer decomposition to the signal $x(t)$. The corresponding expression is^[3]

$$X(t) = \int_{-\infty}^{+\infty} e^{j2\pi ft} H(t, f) dX(f) \tag{1}$$

Where $H(t, f)$ is a complex envelope function. Adopt short time Fourier transform method to compute

$$H(t, f) = \int_{-\infty}^{+\infty} [x(\tau)\gamma * (\tau - t)]e^{-j2\pi ft} dt \tag{2}$$

Where $\gamma(\tau)$ is a window function with small time width. Define the fourth order spectrum cumulant of $Y(t)$ process is

$$C_{4Y}(f) = S_{4Y}(f) - 2S_{2Y}^2(f) \quad f \neq 0 \tag{3}$$

Where is the instantaneous torque spectrum of 2n orders.

$$S_{2nY}(f) = E\{|H(t, f)dX(f)|^{2n}\} / df \tag{4}$$

Then the spectral kurtosis is

$$K_Y(f) = \frac{C_{4Y}(f)}{S_{2Y}^2(f)} = \frac{S_{4Y}(f)}{S_{2Y}^2(f)} - 2 \tag{5}$$

If the signal $x(t)$ is stationary signal, the corresponding spectral kurtosis zero. If the signal $x(t)$ is interfered by stationary noise signal $b(t)$, its spectral kurtosis is^[4]

$$K_Z(f) = \frac{K_x(f)}{[1 + \rho(f)]^2} \quad f \neq 0 \tag{6}$$

Where $\rho(f)$ is the bottom of signal to noise ratio of signal $x(t)$.

The Fourier transform has no effective treating method for the trade-off problem between the time domain and frequency domain resolution. The basis of spectral kurtosis is short time Fourier transform. So the spectral kurtosis method can not realize fault diagnosis under the condition of strong noise interference.

IV. IMPROVED SPECTRUAL KURTOSIS THEORY

Energy operator is a kind of mathematical algorithm to track the narrowband signal. Define the energy operator of continuous signal $x(t)$ by mathematical method

$$\Psi_c[x(t)] = \left(\frac{dx(t)}{dt}\right)^2 - x(t)\frac{d^2x(t)}{dt^2} = [x(\dot{t})]^2 - x(t)x(\ddot{t}) \tag{7}$$

Where Ψ_c is the energy operator, $\dot{x}(t)$ and $\ddot{x}(t)$ is the first two derivative of the original signals.

As for an undamped free vibration system, the vibration displacement is

$$x(t) = A \cos(\omega_0 t + \theta) \tag{8}$$

Its energy operator is

$$\Psi_c[x(t)] = \Psi_c[A \cos(\omega_0 t + \theta)] = (A\omega_0)^2 \tag{9}$$

The energy of undamped oscillation system has no change with time. And its energy value is equal to the sum of kinetic energy and potential energy at a certain moment. The computation formula is

$$E_0 = (A\omega_0)^2 / 2 \tag{10}$$

As for discrete signal $x(n)$, the computation formula of energy operator is

$$\Psi_d[x(n)] = x^2(n) - x(n-1)x(n+1) \quad (n = 0, \pm 1, \pm 2, \dots) \tag{11}$$

Define the sampling cycle of discrete signal as T , and replace the continuous variable t by discrete variable nT . Establish the reflection between two kinds of signal energy operators as

$$\begin{cases} \dot{x}(t) \leftrightarrow [x(n) - x(n-1)]/T \\ \ddot{x}(t) \leftrightarrow [x(n) - 2x(n-1) + x(n-2)]/T^2 \\ \Psi_c[x(t)] \leftrightarrow \Psi_d[x(n-1)]/T \end{cases} \quad (12)$$

V. GEARBOX FAULT DETECTION AND DIAGNOSIS

Because of the complex working condition and noise interference, fast spectral kurtosis algorithm can't extract the complete feature information. In this case, minimum entropy solution of convolution operation should be carried out to the original vibration signals of gearbox, and highlight the spike pulse composition. Fast spectral kurtosis algorithm is carried out to MED filtering signal again. Pass filter is finished under the optimal center frequency and bandwidth band. Energy operator demodulation method is adopted for envelope spectrum analysis of filtering signals. Compared with traditional Hilbert change method, energy operator demodulation method has high temporal resolution, high adaptive ability and simple computation process^{[2][3]}. By comparing spectral envelope with fault frequency theory values of gearbox, different fault types can be analyzed.

In the gear tooth root crack fault experiment, the rotation speed of input shaft of gearbox is 1468.7r/min. According to the transmission ratio, the rotation speed of intermediate shaft can be calculated and is 738.35r/min. Furthermore, the rotation frequency of intermediate shaft and gear is

$$f_r = 12.24Hz \quad (13)$$

And set the sampling interval is 2s.

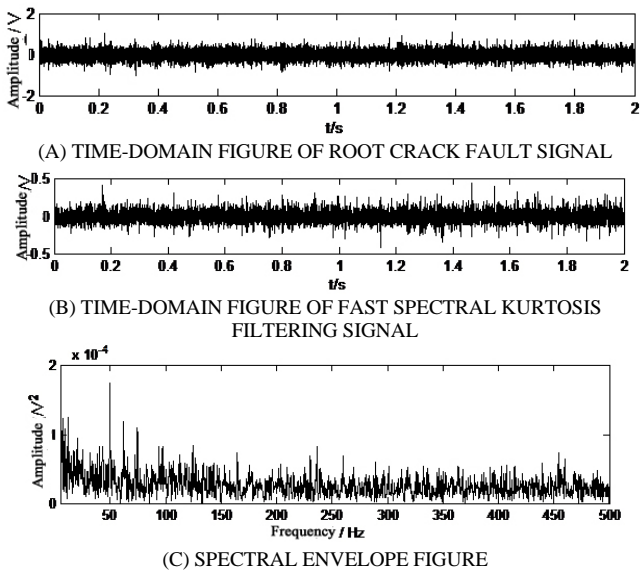


FIGURE II. FAST SPECTRAL KURTOSIS FILTERING OF ROOT CRACK FAULT SIGNAL

Figure II is the time domain and spectral envelope of original root tooth crack fault signal after spectral kurtosis filtering. We can see from Figure II that although the impact properties are enhanced, the fault information also cannot be identified from the spectral envelope in Figure II (c).

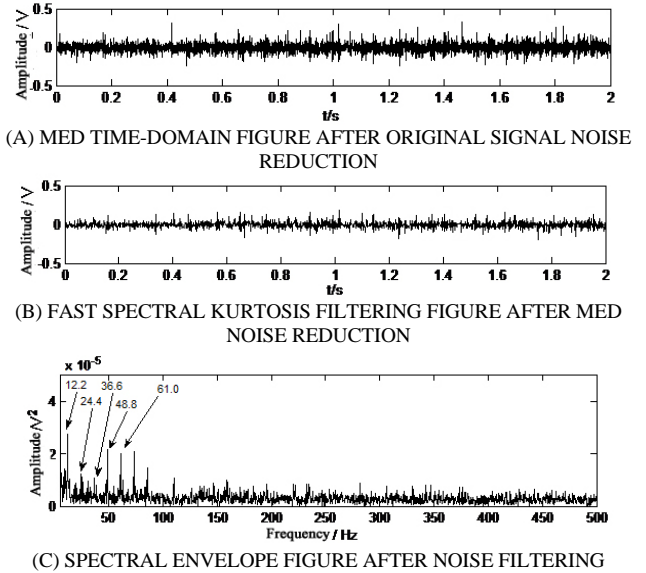


FIGURE III. FAST SPECTRAL KURTOSIS FILTERING AFTER MED NOISE REDUCTION

Figure III includes the MED time-domain figure after original signal noise reduction, fast spectral kurtosis filtering figure after MED noise reduction and spectral envelope figure after noise filtering.

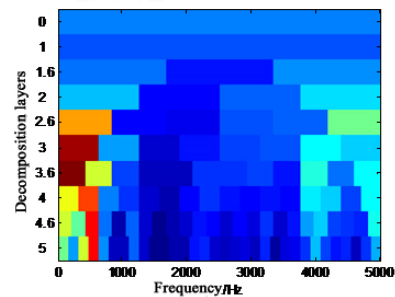


FIGURE IV. FAST SPECTRAL KURTOSIS SPECTRA AFTER MED NOISE REDUCTION

Figure IV is the fast spectral kurtosis spectra after MED noise reduction of fault signal in Figure III. Figure VI show that in fast spectral kurtosis spectra, the signal kurtosis value is maximum provided by band-pass filter when the decomposition layer is 3.6, the central frequency is 208.33Hz, the bandwidth is 416.67Hz. The corresponding color in Figure VI is deepest. Then, the band-pass filter parameters can be calculated. In Figure III, after MED and fast spectral kurtosis filtering, the signal spectral envelope clearly identify the 12.2 Hz frequency part, which accords with formula (13) and verify the effectiveness of fault signal extraction method .

However, there are not only single faults, but also composite faults under the actual working condition, which

require better fault detection and diagnosis method.

In composite crack fault diagnosis experiment of bearing's inner and outer rings, the rotation speed of input shaft of gearbox is 1492.3r/min, the rotation speed of intermediate shaft is 746.15r/min. Then, the fault frequency of bearing's inner ring is

$$f_{in} = 67.5\text{Hz} \tag{14}$$

The fault frequency of bearing's outer ring is

$$f_{out} = 44.54\text{Hz} \tag{15}$$

The rotation frequency of intermediate shaft is

$$f_r = 12.44\text{Hz} \tag{16}$$

And the sampling interval is 2s.

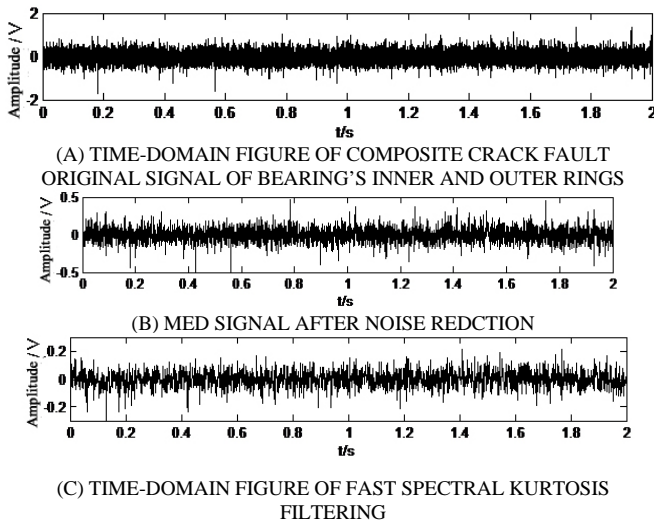


FIGURE V. FILTERING SIGNAL FIGURE OF BEARING'S COMPOSITE FAULT

Figure V is the stepwise filtering graph of composite crack fault signal for bearing's inner and outer ring. In the time-domain figure of original signal, the shock response signal of crack fault is submerged by noise and is difficult to identify. After MED noise reduction and noise filtering of spectral kurtosis, the shock response characteristic is highlight. The comparison between signal's kurtosis values before and after noise filtering is shown in Table II. Kurtosis comparison of different filtering methods

TABLE II. KURTOSIS COMPARISON AMONG DIFFERENT FILTERING METHODS

Signal	Original Signal	FSK	MED	MED+ FSK	IMF3	High Frequency of Third Layer
Kurtosis value	1.16	2.88	16.25	18.42	1.38	1.21

Table II shows that after MED and FSK filtering for original signal, the signal kurtosis value increase from 1.16 to 18.42, but the kurtosis value growth of other filtering methods is smaller. Figure VI is the signal spectral envelope after filtering.

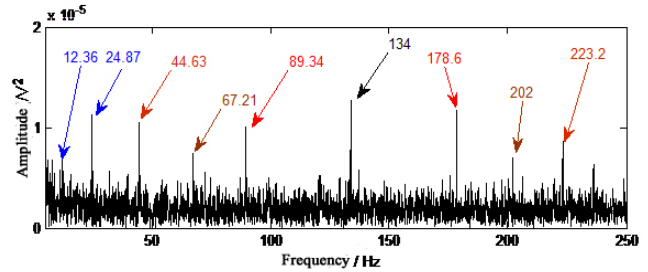


FIGURE VI. SIGNAL SPECTRAL ENVELOPE AFTER FILTERING

Figure VI shows that the signal's characteristic frequencies of MED filtering and FSK filtering are obvious. The frequency of 12.36Hz accords with the rotation frequency of intermediate shaft. And the frequency of 24.87Hz accords with the rotation frequency of input shaft. 44.63Hz is the crack fault frequency of bearing's outer ring. 89.34Hz, 134Hz, 18.6Hz and 223.2Hz are according with the double frequency to five-times frequency of crack fault of bearing's outer ring. 67.21Hz accords with the crack fault frequency of bearing's inner ring. 134Hz and 202Hz are according with the double frequency to three-times frequency of crack fault of bearing's inner ring. The above data verify the effectiveness of extraction method for composite fault feature extraction of bearing's inner and outer rings.

VI. CONCLUSION

Aiming to the difficulties in fault signal feature extraction of traditional spectral kurtosis method under large noise working conditions, the minimum entropy convolution theory and spectral kurtosis algorithm are combined, and a new kind of gearbox fault diagnosis method based on MED and FSK is put forward. Single faults and composite faults on gearbox fault test table verifies the effectiveness and precision.

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