

Research on the bending moment-curvature relationship of wide notch concrete beam strengthened with EBR CFRP plate

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Abstract. Based on the hypothesis of neglecting tensile strength of concrete when concrete beam is bent, the simple bending concrete cover of four-point bending concrete beam is cut, thus forming a “ π -shaped” notch on the side elevation of the beam. Such beam is called a wide notch concrete beam, which is a new abnormal concrete beam used to study the characteristics of the CFRP (Carbon fiber reinforced plastic plate) plate-concrete interface. With consideration of some theoretical hypotheses, computational analysis, and static load test of 4 common concrete beams with externally bonded reinforcement of CFRP plate (EBR CFRP), 4 concrete beams with wide notch and 3 simple concrete beams (control group), this study investigated the calculation formula for the bending moment-curvature of concrete beam with EBR CFRP and wide notch under different loading phases. The theoretical values of cracking load, yield load, ultimate load and corresponding curvature of the reinforced concrete beam were then calculated. These theoretical values agree well with the test results.

Keywords: externally bonded reinforcement; carbon fiber reinforced plastic plate; seismic strengthening; wide-notch concrete beam; moment-curvature.

1 Introduction

Externally bonded reinforcement of CFRP plate (EBR CFRP) is used for concrete members that fail to adopt embedding CFRP reinforcement. However, numerous experimental studies reported debonding failure of CFRP on concrete members using EBR CFRP[1-5]. Such debonding failure is identified as brittle failure without evident mechanical signs before failure but with low stress-strain in the CFRP bar at failure. This failure not only causes material waste, but also significantly reduces the security of the reinforced system[6-9]. The bonding properties of CFRP plate-concrete interface is the key factor influencing concrete beams using EBR CFRP. Based on the hypothesis of neglecting tensile strength of concrete when concrete beam is bent, the simple bending concrete cover of four-point bending concrete beam is cut, thus forming a “ π -shaped” notch on the side elevation of the beam. Such beam is called a wide notch concrete beam, which is a new abnormal concrete beam used to study the characteristics of the CFRP plate-concrete interface. With consideration of some theoretical hypotheses, computational analysis and static load test of 4 common concrete beams with EBR CFRP, 4 concrete

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beams with wide notch and 3 simple concrete beams (control group), this paper investigated the calculation formula of bending moment-curvature of concrete beam with EBR CFRP and wide notch under different loading phases. The theoretical values of cracking load, yield load, ultimate load and corresponding curvature of the reinforced concrete beam were then calculated. These theoretical values agree well with the test results[10-13,15].

2 Experiment of concrete beam with EBR CFRP and wide notch

2.1 Test materials

Lica-200 epoxy resin building structure adhesive was used as the testing adhesive. The CFRP plate was 1.4 mm thick and 50 mm wide. The bar was measured to have 2504.6 Mpa tensile strength and 1.7×10^5 Mpa elasticity modulus. The Strength grade of concrete was C30. A total of 11 150 mm \times 300 mm \times 2600 mm concrete beams were prepared. In the experiment, the beam span (l) was 2,300 mm and four-point bending loading was applied. The bottom longitudinal bar used $2\phi 14$, where the bearing rod used $2\phi 8$. The net concrete cover on the longitudinal bar is 30 mm thick ($c=30$ mm), where that on the bearing rod is 25 mm thick ($c'=25$ mm). To resist shear force, $\phi 8@150$ stirrup was used at $1/3$ length of the beam span, where $\phi 8@100$ stirrup was used at $1/3$ of both beam ends as support[14].

2.2 Construction of test beam

The test of the concrete beam with EBR CFRP bar is designed to study the bonding-slip relationship of the CFRP-concrete interface(Fig.1). For the clear force analysis of the CFRP, the middle segment of the beam ($l_0(600\text{mm})$) was emptied into 20 mm. The total length of the CFRP is 2100. $l_1=750\text{mm}$ and the interval between two loading points is not 700 mm. Apparently, AA'B'B and DD'C'C apparently fall within the simple bending section. The reinforced concrete beam is not influenced by shearing crack at early loading. In other words, additional anti-shearing sections exist at the two ends of the notch to offset the stress concentration at the boundaries.

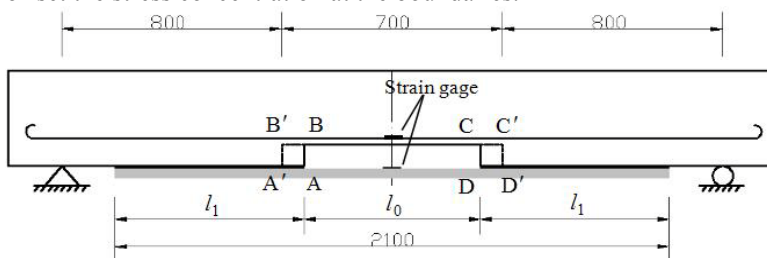


Figure 1. Improved test of EBR CFRP (unit: mm)

2.3 Test program and results

Eleven testing concrete beams, including 3 concrete beams (hereinafter referred as CB), 4 concrete beams using EBR CFRP (hereinafter referred as EBR), and 4 concrete beams with EBR CFRP and wide notch (hereinafter referred as EBRK). Were used. The notch position and test program of EBRK are shown in Fig.1. To export the bonding-slip constitutive relation of CFRP-concrete interface, the author pastes strain gages densely on 11 CFRPs to measure the stress intensity distribution along the length of the CFRP and the relative slippage of the CFRP-concrete interface.

The static load characteristic values of the 11 tested concrete beams are listed in Table 1. P_{cr} denotes the cracking load of beams. P_y is the yield load of beams. P_u is the ultimate load of beams. Table 1 shows that EBR receives a better reinforcement effect of CFRP than EBRK. Compared with CB, EBR has 28.3%, 36.1% and 35% higher P_{cr} , P_y and P_u , whereas EBRK has 15%, 11.1% and 17.5% higher P_{cr} , P_y and P_u . EBR achieves twice the growth of EBRK[14].

Table 1. Significant load value of beams

Beam No.	P_{cr}/kN	P_{cr} growth	P_y/kN	P_y growth	P_u/kN	P_u growth	Failure mode
CB	15	—	90	—	100	—	Midspan concrete is crushed and bottom breaks
EBRK1	16	6.7%	100	11.1%	130	30%	Debonding failure of CFRP and brittle failure covers the whole beam
EBRK2	18	20.0%	100	11.1%	120	20%	Debonding failure of bottom concrete caused by CFRP
EBRK3	18	20.0%	100	11.1%	110	10%	Debonding failure of bottom concrete caused by CFRP
EBRK4	17	13.3%	100	11.1%	110	10%	Debonding failure of bottom concrete caused by CFRP; brittle fracture
EBR1	19	26.7%	100	11.1%	120	20%	Tensile failure of CFRP at concrete support. Concrete remains uncrushed.
EBR2	20	33.3%	120	33.3%	130	30%	Tensile failure of CFRP at east concrete support. Concrete remains uncrushed.
EBR3	18	20.0%	140	55.6%	150	50%	Tensile failure of CFRP at east concrete support. Concrete remains uncrushed.
EBR4	20	33.3%	130	44.4%	140	40%	Tensile failure of CFRP at east concrete support. Concrete remains uncrushed.

3 Bending moment-curvature relationship of EBRK

3.1 Basic hypotheses

The deformation performance of EBRK was studied on the basis of following hypotheses: (1) plane cross-section assumption; (2) relative slippage between CFRP and concrete beam is neglected; (3) concrete stress-strain relationship uses model in the Design Code for Concrete Structures; (4) reinforcing steel bar uses elastic-perfectly plastic material, without consideration of stress strengthening; (5) stress-strain relation of CFRP is linear elasticity; (6) tensile concrete and adhesive layer stand aloof from tension; and (7) effects of shrinkage, creep and temperature stress of concrete and adhesive are neglected.

3.2 Yield moment (M_y) and yield curvature (ϕ_y)

The bending moment-curvature relationship of the EBRK cross section at bending yield can be determined from the geometrical relationship, physical relationship, and condition of static equilibrium.

The stress and strain distributions on the EBRK cross section at bending yield are shown in Fig.2[14].

The bending yield of EBRK includes longitudinal bar yield and CFRP yield. According to the equilibrium of forces[15]:

$$\frac{1}{2}bx_cE_c\varepsilon_c + E'_s\varepsilon'_sA'_s = A_sE_s\varepsilon_s + KE_s\varepsilon_sn'_{pf}A_{pf} \quad (1a)$$

and

$$M_y = \frac{1}{2}bx_cE_c\varepsilon_c(h_0 - \frac{x_c}{3}) + A'_sE'_s\varepsilon'_s(h_0 - a'_s) + KE_s\varepsilon_sn'_{pf}A_{pf}(h_{pf} - h_0) \quad (1b)$$

where h_0 is the distance from the center line of the main reinforcement to the upper edge of concrete; a_s is the distance from the center line of the main reinforcement to the lower edge of concrete; a'_s is the distance from the center line of the bearing rod to the upper edge of concrete; x_c is the distance from the neutral axis to the upper edge of concrete; h' is the height of the concrete beam (including EBRCFRP), $h' = h_0 + a_s + d_{pf}$ (d_{pf} is thickness of CFRP); h is the height of the concrete beam,

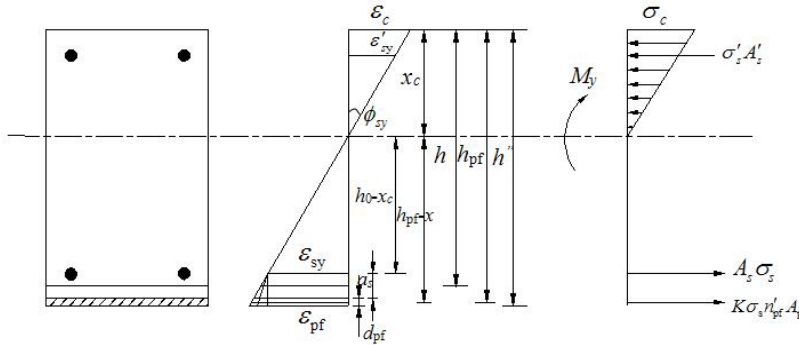


Figure 2. Stress and strain distribution on cross section of EBRK at bending yield

$h = h_0 + a_s$; E_s is the elasticity modulus of tensile reinforcement; E'_s is elasticity modulus of compression reinforcement; E_c is the elasticity modulus of concrete; E_{pf} is the elasticity modulus of CFRP; ε_s is the strain of tensile reinforcement; ε'_s is the strain of compression reinforcement; ε_c is the strain of concrete; ε_{pf} is the strain of CFRP ($\varepsilon_{pf} = K\varepsilon_s = K\varepsilon_s$); K is the strain correction coefficient of CFRP ($1 \leq K \leq \frac{h' - x_c}{h_0 - x_c}$); h_{pf} is the distance from the section centroid of CFRP to the top beam fiber; $n'_{pf} = E_{pf}/E_s$ is the elasticity modulus ratio of CFRP and reinforcing steel bar; A_{pf} is the cross-sectional area of CFRP; A_s is the cross-sectional area of the main reinforcement; and A'_s is the cross-sectional area of the bearing rod.

Given fixed section parameters, x_c can be calculated from Equation (1a) after which M_y can be calculated from Equation (1b) according to the balance condition of bending moment. At this moment, the yield curvature is: $\phi_y = \frac{\varepsilon_c}{x_c} = \frac{\varepsilon_{pf}}{h_{pf} - x_c}$.

3.3 Ultimate bending moment (M_u) and ultimate curvature (ϕ_u)

3.3.1 Definition of failure mode of reinforced beam

When calculating the ultimate bearing capacity of reinforced members, the failure modes include the following: (1) after tensile reinforcement is yielded, compression concrete is destroyed, but CFRP isn't yielded. Such failure mode is the expected ductile failure of EBRK, which occurs upon the appropriate reinforcement ratio of the original beam and CFRP reinforcement. At balanced-reinforcement failure, CFRP is extended fully despite not being broken because the adhesive layer remains undamaged. (2) After tensile reinforcement is yielded, compression concrete isn't destroyed, but CFRP is broken ($\varepsilon_s = \varepsilon_y$). Such failure mode occurs with low reinforcement ratio of the original beam and

CFRP reinforcement. The CFRP has reached its ultimate strain ($\varepsilon_{pf} = \varepsilon_{pfu}$), whereas the compression concrete isn't completely developed. Large cracks and deflection can be observed on the beam. (3) Two balanced failures will occur after tensile reinforcement is yielded. Balanced failure I refers to the case in which the : strain of the tensile reinforcement exceeds its yield tensile strain after it is yielded ($\varepsilon_s > \varepsilon_y$) and ε_{pf} reaches the ultimate tensile strain ($\varepsilon_{pf} = \varepsilon_{pfu}$). The compression concrete is crushed, which indicates that ε_c reaches the ultimate compression strain ($\varepsilon_c = \varepsilon_{cu}$). Both reinforcing steel bar and CFRP are brought into full play. Balanced failure I is an ideal critical state that usually dose not occur. In balanced failure II: when the tensile reinforcement is yielded, $\varepsilon_s = \varepsilon_y$, CFRP is broken ($\varepsilon_{pf} = [\varepsilon_{pf}]$) and the compression concrete is destroyed ($\varepsilon_c = \varepsilon_{cu}$). Balanced failure II is also an ideal critical state that usually dose not occur.

3.3.2 Compression concrete is destroyed, but CFRP is not yielded after the tensile reinforcement is yielded

The stress-strain of the cross section is shown in Fig.3. According to the equilibrium of forces, the ultimate bearingcapacity of the double-reinforcement cross section of EBRK can be calculated.

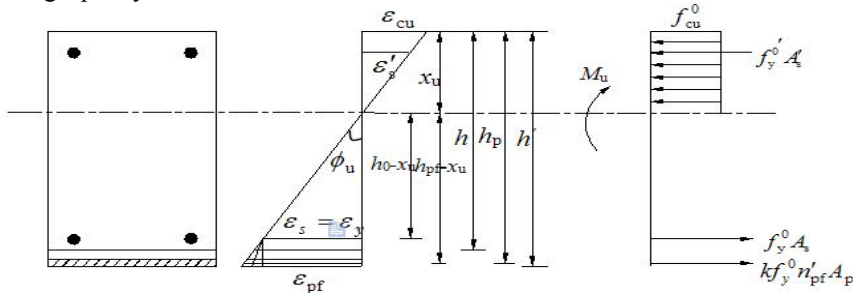


Figure 3. Stress-strain of cross section at ultimate bearing failure

$$x_u = \frac{A_s E_s \varepsilon_s + K E_s \varepsilon_s n'_{pf} A_{pf} - f_y^0 E'_s \varepsilon'_s}{f_{cu}^0 \cdot b} \quad (2a)$$

$$M_u \leq x_u \cdot b \cdot \frac{x_u}{2} f_{cu}^0 + A'_s E'_s \varepsilon'_s (x_u - a'_s) + A_s E_s \varepsilon_{sy} (h_0 - x_u) + K E_s \varepsilon_s n'_{pf} A_{pf} (h_{pf} - x_u) \quad (2b)$$

where f_{cu}^0 is the compressive strength of concrete. Therefore, the curvature of the cross section is.

$$\phi_u = \frac{\varepsilon_{cu}}{x_u} = \frac{\varepsilon_{pf}}{h_{pf} - x_u} \quad (3)$$

In Equations (2a) and (2b), the strain of CFRP uses the measured strain of its outermost fiber ($h_{pf} = h'$). Given that the vertical stress or strain distribution of CFRP is uneven, the strain at the stress center of the CFRP cross section (ε_{px}) shall be used for accurate computation (Fig.4). In Fig.4, h_1 is the distance from the cut simple bending bottom to the upper edge of the beam.

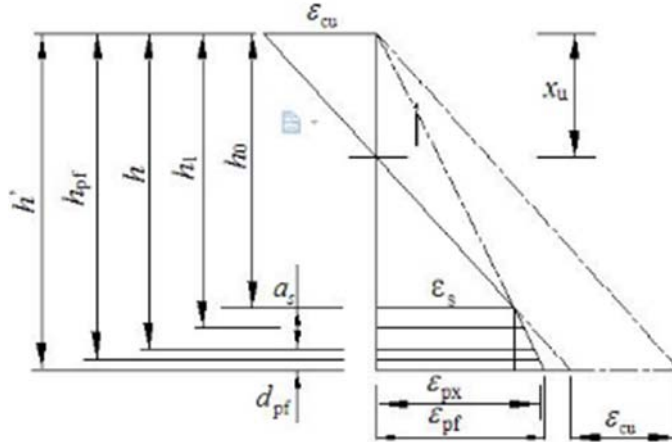


Figure 4. Calculation of ε_{px}

Given that $\varepsilon_s \leq \varepsilon_{px} \leq \varepsilon_{pf}$ and $\varepsilon_{pf} = K\varepsilon_s$, according to geometric similarity, we determine that,

$$\frac{\varepsilon_{pf} - \varepsilon_s}{a_s + d_{pf}} = \frac{\varepsilon_{px} - \varepsilon_s}{a_s + \frac{3a_s + 2d_{pf}}{6a_s + 3d_{pf}}d_{pf}} \quad (4)$$

Then,

$$\varepsilon_{px} = \left[1 + \frac{(K-1)(a_s + \frac{3a_s + 2d_{pf}}{6a_s + 3d_{pf}}d_{pf})}{a_s + d_{pf}} \right] \varepsilon_s \quad (5)$$

When calculating the ultimate bearing capacity of the EBRK cross section,

$$\sigma_{pf} = \left[1 + \frac{(K-1)(a_s + \frac{3a_s + 2d_{pf}}{6a_s + 3d_{pf}}d_{pf})}{a_s + d_{pf}} \right] n'_{pf} f_s^0 \quad (6)$$

3.3.3 CFRP is broken but compression concrete is not damaged after the tensile reinforcement is yielded

In Fig.3, the ultimate bearing capacity of the double-reinforcement cross section of EBRK can be calculated according to the equilibrium of forces:

$$M_u \leq x_c \cdot b \cdot \frac{x_c}{2} \sigma_c + A'_s f_y^{0'} (x_c - d'_s) + A_s f_y^0 (h_0 - x_c) + f_{pfu} A_{pf} (h_{pf} - x_c) \quad (7a)$$

$$x_u = \frac{A_s f_y^0 + f_{pfu} A_{pf} - f_y^{0'} A'_s}{\sigma_c \cdot b} \quad (7b)$$

where $f_y^{0'}$ is the compressive strength of the bearing rod; f_y^0 is the tensile strength of the main reinforcement; and f_{pfu} is breaking strength of CFRP. Therefore, the curvature of the cross section is

$$\phi_u = \frac{\varepsilon_s}{h_0 - x_c} = \frac{\varepsilon_{pfu}}{h_{pf} - x_c} \quad (8)$$

3.3.4 Balanced failure

In Fig.3, balanced failure I can be calculated from the deformation compatibility conditions:

$$x_u = \frac{\varepsilon_{cu} (h_{pf} - \frac{1}{2} d_{pf})}{\varepsilon_{pfu} + \varepsilon_{cu}} \quad (9)$$

Therefore, the curvature of the cross section is

$$\phi = \frac{\varepsilon_{cu}}{x_u} = \frac{\varepsilon_{pfu}}{h_{pf} - x_u} \quad (10)$$

In Fig.3, balanced failure II can be calculated from the deformation compatibility conditions:

$$x_u = \frac{\varepsilon_{cu} (h_{pf} - \frac{1}{2} d_{pf})}{\varepsilon_{cu} + [\varepsilon_{pf}]} \quad (11)$$

Therefore, the curvature of the cross section is

$$\phi = \frac{\varepsilon_{cu}}{x_u} = \frac{[\varepsilon_{pf}]}{h_{pf} - x_u} \quad (12)$$

4 Test results of bending moment-curvature relationship

ϕ_y and ϕ_u as well as the corresponding μ_ϕ (Table 2) can be derived from the above curvature formulas. The $M - \phi$ charts of beams can be drawn (Fig.5). In Table 2, ϕ_{yt} and ϕ_{yc} are the test and theoretical value of yield curvature, respectively; ϕ_{ut} and ϕ_{uc} are the test and theoretical values of ultimate curvature, respectively; $\mu_{\phi t}$ and $\mu_{\phi c}$ are the test and theoretical value of the ductility factor of sectional curvature, respectively; and P_y and P_u are yield load and ultimate load, respectively. In Table 2, $\mu_{\phi t} / \mu_{\phi c}$ of CB is 1.07. The $\mu_{\phi t} / \mu_{\phi c}$ of EBRK are 1.08, 0.98, 0.97 and 0.98. The $\mu_{\phi t} / \mu_{\phi c}$ values of EBR are 0.96, 0.98, 0.98 and 0.99, all of which are smaller than those of CB. This finding-

indicates that although CFRP can increase the cracking, yield and ultimate loads of both EBRK and EBR, CFRP decreases their ductility to a certain extent. However, the $\mu_{\phi} / \mu_{\phi_c}$ values of both EBRK and EBR are within the acceptable range, indicating that both EBRK and EBR can satisfy the ductility requirement. Moreover, the ductility factors of EBRK are smaller than those of EBR, indicating that the rigidity of EBRK is higher than that of EBR.

Table 2. Ductility factor of sectional curvature of testing beams

Beam No.	P_y /kN	P_u /kN	P_u / P_y	Yield curvature (10^{-5} mm)		Ultimate curvature (10^{-5} mm)		μ_{ϕ_t}	μ_{ϕ_c}	$\mu_{\phi_t} / \mu_{\phi_c}$
				ϕ_{yt}	ϕ_{yc}	ϕ_{ut}	ϕ_{uc}			
CB	90	100	1.11	6.01	6.91	13.56	14.36	2.26	2.08	1.07
EBRK1	100	130	1.30	3.98	4.19	8.49	8.31	2.13	1.98	1.08
EBRK2	100	120	1.20	4.60	4.39	9.41	9.22	2.05	2.10	0.98
EBRK3	100	110	1.10	4.21	4.01	8.76	8.58	2.08	2.14	0.97
EBRK4	100	110	1.10	4.92	4.73	9.48	9.31	1.93	1.97	0.98
EBR1	100	120	1.20	4.02	3.82	8.45	8.31	2.10	2.18	0.96
EBR2	12	130	1.10	5.57	5.36	11.85	11.7	2.13	2.18	0.98
EBR3	140	150	1.10	6.49	6.31	13.69	13.56	2.11	2.15	0.98
EBR4	130	140	1.10	6.18	5.99	12.24	12.10	2.00	2.02	0.99

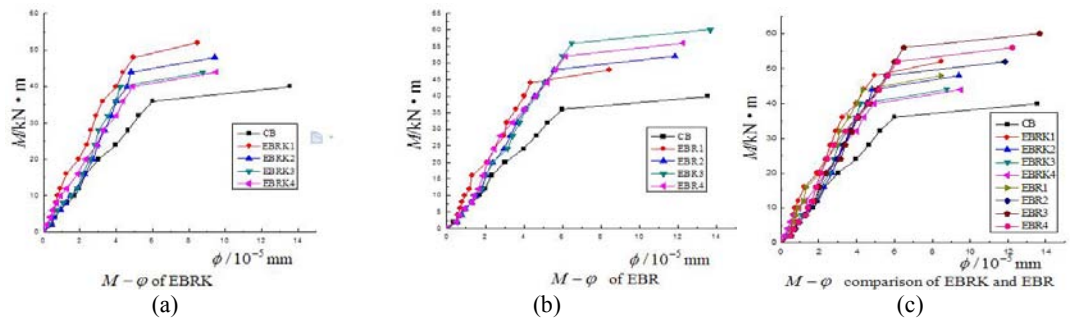


Figure 5. $M - \phi$ of testing beams

4 Conclusions

On the basis of the force analysis of 3 CB, 4 EBRK and 4 EBR under the cracking, yield and ultimate phases, we can conclude that:

- (1) Compared with EBR, EBRK presents clearer forces on CFRP. This condition is convenient for the strain test and force analysis of CFRP. EBRK is superior for use in studying the bonding slippage and macroscopic bearing capacity of CFRP-concrete interface.
- (2) CFRP can improve the deformation resistance of EBRK and EBR to a certain extent. EBRK shows smaller deformation than EBR.
- (3) A formula for calculating the bending moment-curvature of EBRK and EBR under different stress phases is proposed. The calculated results agree well with the test results, indicating that the derived formulas and calculation method are feasible. This approach can provide theoretical references for engineering designers for practical engineering applications.

Acknowledgement

This work was financially supported by The National Natural Science Foundation of China(51678430),China Postdoctoral Science Foundation(2016M591707),The Science and Research

Program of Hunan Province(2015SK20543), key scientific research project of Education Commission of Hunan Province (16A050), Doctoral Science Foundation of Hunan Institute of Engineering.

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