

# Research on Design Schemes of 500kV Convertor Station Grounding

## Grid

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**Abstract.** With the development of HVDC, transmission capacity and transmission voltage level are both increasing. Under this situation, designing reliable grounding grid is more demanding. For areas with high soil resistivity, the grounding parameters can hardly meet relevant requirements. To solve this problem, this paper takes Luxi convertor station as an example to illustrate the designing process, and analyzes different design schemes. The results show that for areas with high deep soil resistivity the effect of using vertical grounding rods is slight, while the one of lengthening horizontal grounding objects is evident.

## Introduction

For the Ultra-high voltage converter station which plays an important role in power system interconnection and transmits huge power over long distance, designing reliable grounding grid is more demanding because transmission capacity and transmission voltage level are both increasing<sup>[1]</sup>. Transmitting the earth fault current to the underground is the main role of the grounding grid which is to limit the step potential differences and contact potential difference. At present, with the development of china market economy and HVDC, transmission capacity and transmission voltage level are both increasing<sup>[2]</sup>. Thus, the earth fault current will also increase. To maintain the electrical power system stable and safe, the permissible grounding grid resistance will be smaller and smaller. The high grounding grid resistance will lead to the high earth potential which will put workers and electrical equipment in danger. More than that, the counterattack of ground voltage will lead to destruction of insulation<sup>[3]</sup>.

Because of the lack of available arable land, most of converter stations are established in the high soil resistance area<sup>[4]</sup>. Meanwhile, there is less available land to establish converter stations. The grid grounding resistance of the convertor station usually cannot meet requirements. Under this circumstance, it is necessary to design compound grounding grids to solve this problem economically and effectively, according to the electric power environment and soil environment. To maintain that the converter stations operate safely and reliable, it has important theoretical significance and practical value<sup>[5]</sup>.

## Design Requirements

**Grounding Grid Resistance Requirements.** According to national standards, the grounding grid resistance requirements of converter station are as follows.

### (1) The Grounding Grid Resistance

$$R \leq \frac{2000}{I_G} \quad (1)$$

$R$ ——the maximum grounding grid resistance considering seasonal variation( $\Omega$ ).

$I_G$ ——the maximum effective value of ground fault unsymmetrical current(A).

(2) When the grounding grid resistance can't meet the formula (1), the limits could be relaxed considering economic factors and technical factors. Following the relevant state regulations, the ground voltage limits could increase to 5kV. If necessary, the limits could be relaxed more by the calculation and analysis. And it could not put workers and electrical equipment in danger.

GB 50150-2006 regulates that when  $I > 4000A$ ,  $Z \leq 0.5\Omega$ .

This paper designs the grounding grid which meets the requirements that grounding grid resistance is under  $0.5\Omega$  and the ground voltage is under 5kV.

**Step Potential Differences and Contact Potential Difference Requirements.** DL/T 621-1997 regulates that step potential differences and contact potential difference of converter station should meet the requirements as follows.

For 110kV and above grounding grid, when it occurs single-phase ground short circuit or two-phase ground fault, step potential differences and contact potential difference of converter station should be as follows.

$$U_t = \frac{174 + 0.17 r_f}{\sqrt{t}} \quad (2)$$

$$U_s = \frac{174 + 0.7 r_f}{\sqrt{t}} \quad (3)$$

$U_t$ ——contact potential difference, V

$U_s$ ——step potential differences, V

$r_f$ ——earth resistivity,  $\Omega \cdot m$

$t$ ——duration of fault short-circuit current, s

### Main Methods of Resistance Reducing

**Vertical grounding rods.** According to DL/T621-1997, when soil resistivity of deep layer soil is low, grounding grid resistance could be reduced by setting up vertical grounding rods. Especially to high soil resistivity area which is inappropriate to set up grounding device by regular methods, vertical grounding rods is an effective way to reduce the grounding grid resistance.

**Extensional horizontal grounding objects.** The area of grounding grid and soil resistivity is the key to grounding grid resistance. The most effective way to reduce grounding grid resistance is expanding the grounding grid area. Expanding the grounding grid area is the fundamental principle of extensional horizontal grounding objects. High land-use fees are not necessary to this way. But it is subject to land area, amplifying grounding objects is commonly used to expanding the grounding grid area.

**Filling ground resistance reducing material.** According to DL/T621-1997, in the high soil resistivity area, soil around grounding electrode could be replaced by ground resistance reducing

material to reduce the grounding grid resistance. Normally, filling ground resistance reducing material is supplementary method in coordination with vertical grounding rods and extensional horizontal grounding objects.

## Maximum Grounding Fault Current

According to power system topology, power system parameter, transformer parameter, line parameter of Luxi back to back converter station, we establish short-circuit current calculation model and calculate the maximum grounding fault current under different current divider coefficient for the maximum rounding grid resistance limit.

According to power system parameter, we set up different short-circuit points to calculate fault current by ATP. Such as rectifier side inverter station, the first tower on the rectifier side, the second tower on the rectifier side, inverter side in converter station, the first tower on the inverter side, the second tower on the rectifier side.

The result shows that short-circuit current are highest when single-phase short circuit occurs on the rectifier side in converter station. For the high grounding fault current in Luxi converter station and high soil resistivity can't meet the grounding grid resistance requirements. In this section, aerial earth wire to current divider is given.

Reducing the grounding grid resistance of the second tower from  $50\Omega$  to  $20\Omega$ , ground potential is under 5kV. The result is as follow in Table 1.

Tab1.Short-circuit current(ground potential under 5kV)

No.	Type	Value
1	short-circuit current (kA)	29.19
2	earth-fault current (kA)	4.27
3	neutral point of transformer branch current on rectifier side(kA)	6.38
4	aerial earth wire branch current on rectifier side (kA)	13.72
5	neutral point of transformer branch current on inverter side(kA)	0.06
6	aerial earth wire branch current on inverter side(kA)	5.55
7	branch current(kA)	24.93
8	shunt factor	0.15
9	grounding grid resistance( $\Omega$ )	1.00

Reducing the grounding grid resistance of the second tower from  $50\Omega$  to  $10\Omega$ , grounding grid resistance is  $0.5\Omega$ .The result is as follow in Table 2.

Tab 2.Short-circuit current

No.	Type	Value
1	short-circuit current (kA)	29.19
2	earth-fault current (kA)	6.90
3	neutral point of transformer branch current on rectifier side (kA)	6.38
4	aerial earth wire branch current on rectifier side (kA)	12.30
5	neutral point of transformer branch current on inverter side (kA)	0.04
6	aerial earth wire branch current on inverter side (kA)	4.48
7	branch current (kA)	22.33
8	shunt factor	0.24
9	Maximum earth-fault current(kA) $D_f = 1.1669$	8.07

## Equivalent Soil Resistivity

The equivalent soil resistivity plays an important role in determining the grounding grid parameters. According to measurement results of soil resistivity, equivalent method of soil resistivity is given in this section based on CDEGS in Table 3.

Tab3.Soil resistivity equivalent result

Layer	Soil Resistivity( $\Omega\text{m}$ )	Depth (m)
1	144.9184	1.992869
2	565.4620	15.44711
3	1215.847	infinity

Thus, it is concluded that the surface layer soil resistivity in Luxi converter station is about  $144.9184\Omega\text{m}$ . According to (2) and (3), the contact potential difference limit is 334V, and the step potential difference is 464V.

## Grounding Grid Design

**Preliminary Design.** According to the floor plans of Luxi converter station, preliminary grounding grid design is given. In the station, the material of grounding objects is 80x8 galvanized flat steel. Flat bar spacing is 4~15m. Burial depth is 0.8m. In GIS, the diameter of horizontal grounding objects is 11.484mm, the material of grounding objects is 4/0 solid copper, solid copper spacing is 4.5~10m.

Horizontal grounding objects spacing,

- (1) Spacing of edge and corner are smaller than spacing of inside.
- (2) Grounding objects spacing is small around GIS.
- (3) Grounding objects only established around the building.

There are different ways to reduce the grounding grid resistance in Table 4.

Tab4.Different ways to reduce the grounding grid resistance

No	Method	Resistance / $\Omega$	Effect analysis
1	/	1.086928	Compare to base value
2	Resistance-reducing agent (0.15m thick, $1\Omega\text{m}$ ) are added to all the grounding objects.	1.082740	0.385%
3	Resistance-reducing agent(0.15m thick, $1\Omega\text{m}$ )are added to the grounding objects around the grounding grid.	1.083964	0.273%
4	All grounding objects are copper and diameter is 11.484mm,no resistance-reducing agent.	1.078490	0.776%
5	All grounding objects are copper and diameter is 11.484mm, resistance-reducing agent(0.15m thick, $1\Omega\text{m}$ ) are added to grounding objects around the grounding grid.	1.073504	1.24%
6	All grounding objects are copper and diameter is 11.484mm, resistance-reducing agent(0.15m thick, $1\Omega\text{m}$ ) are added to grounding objects.	1.071549	1.41%

**Vertical Grounding Rods Design.** The design of add 178 vertical grounding rods

- (1) All grounding objects are copper and diameter is 11.484mm.

(2) 178 vertical grounding rods (copper length is 100m and diameter is 11.484mm) are added to cross point and corner of grounding objects around the grounding grid.

(3) Resistance-reducing agent (0.15m thick,  $1\Omega\text{m}$ ) are added to all grounding objects and vertical grounding rods.

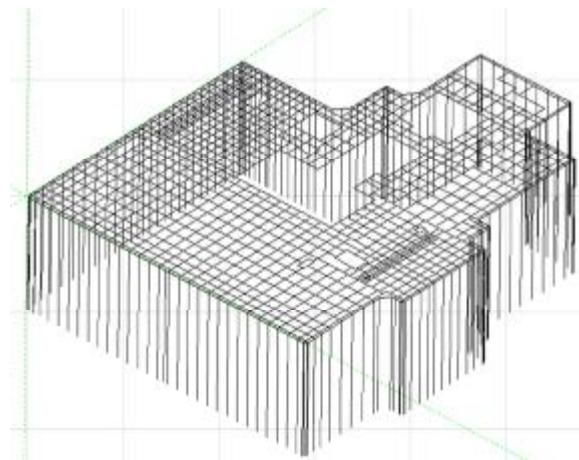


Fig 1. Vertical grounding rods design

The grounding grid resistance is  $0.8830424\Omega$  by this design in Figure 1. It can be seen that because of the high soil resistivity, vertical grounding rods design can't meet the requirement that grounding grid resistance should be under  $0.19\Omega$  or  $0.5\Omega$ .

**Extensional horizontal grounding objects design.** The design of adding 8 extensional horizontal grounding objects (length is 700m) in Figure 2.

(1) The grounding grid station has no change.

(2) 8 extensional horizontal grounding objects (length is 700m) distribute as hub-and-spoke.

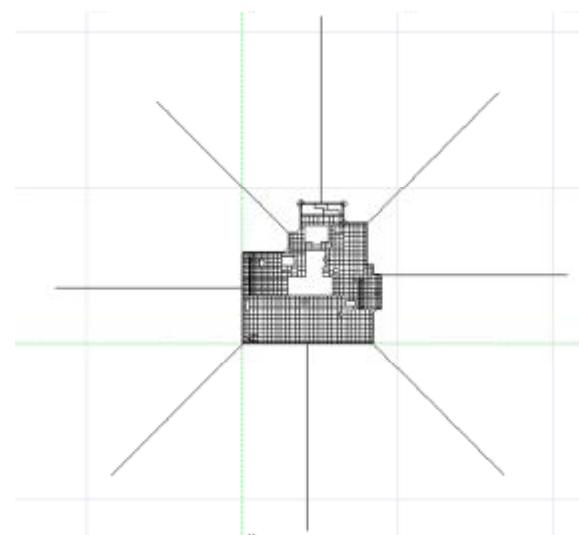


Fig 2. Extensional horizontal grounding objects (length is 700m)

**Tab 5 Different resistance reduction plans of radial 700-meter-long extension arrangement**

No.	Methods
1	(1) Grounding objects in GIS area are copper and the diameter is 11.484mm; (2) Grounding subjects in other area are 80x8 galvanized flat steel; (3) 700-meter-long extensive horizontal electrodes are 80x8 galvanized flat steel; (4) No resistance reduction agent is added to the grounding objects.
2	(1) Grounding objects in GIS area are copper and the diameter is 11.484mm; (2) Grounding subjects in other area are 80x8 galvanized flat steel; (3) 700-meter-long extensive horizontal electrodes are 80x8 galvanized flat steel; (4) Resistance-reducing agent (0.15m thick, 1Ωm) are added to grounding objects around the grounding grid and extensive electrodes.
3	(1) Grounding objects in GIS area are copper and the diameter is 11.484mm; (2) Grounding subjects in other area are 80x8 galvanized flat steel; (3) 700-meter-long extensive horizontal electrodes are flexible graphite; (4) No resistance reduction agent is added to the grounding objects.
4	(1) Grounding objects in GIS area are copper and the diameter is 11.484mm; (2) Grounding subjects in other area are 80x8 galvanized flat steel; (3) 700-meter-long extensive horizontal electrodes are flexible graphite; (4) Resistance-reducing agent (0.15m thick, 1Ωm) are added to grounding objects around the grounding grid and extensive electrodes.

**Tab6.Grounding resistance of different plans**

No.	Grounding resistance(Ω)	Effect analysis
1	0.4952850	control
2	0.4892988	-1.208%
3	0.4961835	+0.18%
4	0.4881788	-1.43%

It can be seen that when the extensional horizontal grounding object is 700 meters in table 5 and 6, all design can meet the requirement that the grounding grid resistance is under 0.5Ω. Adding resistance-reducing agent, Flexible graphite base grounding objects is better than 80x8 galvanized flat steel.

The design of adding 8 extensional horizontal grounding objects (length is 150m) in Figure 3.

- (1) The grounding grid in station has no change.
- (2) 8 extensional horizontal grounding objects (length is 150m, depth is 2m) distribute as hub-and-spoke.

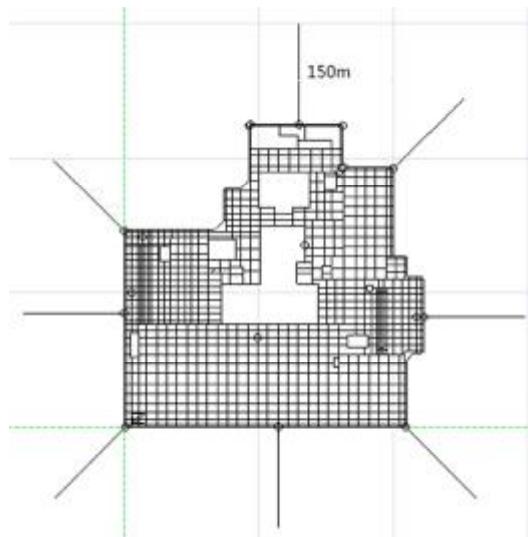


Fig 3. Extensional horizontal grounding objects (length is 150m, depth is 2m)

Tab 7. Different resistance reduction plans of radial 150-meter-long extension arrangement

No.	Resistance reduction plans
1	(1) Grounding objects in GIS area are copper and the diameter is 11.484mm;
	(2) Grounding subjects in other area are 80x8galvanized flat steel;
	(3) 150-meter-long extensive horizontal electrodes are 80x8galvanized flat steel;
	(4) Resistance-reducing agent (2.2cm thick, 1Ωm) are added to extensive electrodes.
2	(1) Grounding objects in GIS area are copper and the diameter is 11.484mm;
	(2) Grounding subjects in other area are 80x8galvanized flat steel;
	(3) 150-meter-long extensive horizontal electrodes are flexible graphite;
	(4) Resistance-reducing agent (3.6cm thick, 1Ωm) are added to extensive electrodes.

Tab 8. Grounding resistance of different resistance reduction plans

No.	Grounding resistance(Ω)	Excess
1	0.8998415	10.015%
2	0.9	10%

It can be seen that extensional horizontal grounding objects design is better than vertical grounding rods design in Table 7 and 8. The grounding grid resistance could be reduced to under  $0.5\Omega$ .

## Conclusion

This article researches on the designing plan of the grounding grid for 500kV convector station and taking Luxi convector station as an example to design the grounding grid and compare the resistance diminishing effects of different plans. The result shows that, if take the decreasing of grounding resistance to  $0.5\Omega$  as a limitation, according to most ground resistance designing principle, the plan which extends 8 700-meter-long earth electrodes meets the requirements. If the grounding voltage is extended to 5kV, both the addition of vertical grounding resistance and the extension of horizontal electrodes could achieve the goal. For areas with high solid resistivity, such as Luxi convector station, the effect of vertical grounding resistance is indistinctive, to solve this problem, the extension of horizontal earth electrodes could be applied at the same time.

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