

# Adsorption of Chromium from Aqueous Solution Using Activated Carbon Coated Sand

Mei-ling HUANG<sup>a</sup> and Shi-quan LIU<sup>b,\*</sup>

School of materials science and engineering, University of Jinan, Jinan 250022, Shandong, China

<sup>a</sup>851401773@qq.com, <sup>b</sup>liusq\_ujn@hotmail.com

\*Corresponding author: Shiquan Liu

**Abstract**—Activated carbon coated silica sand (AC@sand) synthesized by hydrothermal carbonization and KOH activation was used to adsorb chromium from aqueous solution. The factors which influence the removal of Cr(VI) onto the AC@sand including the pH, initial concentration, contact time and temperature was studied. The pH and temperature influence both adsorption and reduction.

**Keywords**—Porous AC@sand; Adsorption; Chromium

## I. INTRODUCTION

Activated carbon (AC) with large surface area and porosity is used for the removal of heavy metal ions in wastewater [1-2]. However, in previous research [3], we found that it was hard to collect the used AC from the treated wastewater either by deposition or filtration due to the light weight of the AC powder. Sand is a traditional water purification material. Due to its large specific gravity, the used sand can be easily collected from the bottom of the treated water. However, sand has a low adsorption capacity toward metal ions in water.

In this work, activated carbon coated silica sand (AC@sand) synthesized by hydrothermal carbonization and KOH-activation was used to adsorb chromium from aqueous solution. The large specific gravity of the sand facilitates the collection of the used AC@sand. The influence of pH, initial concentration, contact time and temperature on the adsorption of the Cr(VI) was researched. The isotherm models and kinetic models were studied.

## II. EXPERIMENTAL SECTION

The coated sand was prepared as follows. One gram of glucose, 1.0 g of silica sand, 10 mL of deionized water, 0.2 g of moderate sodium dodecyl sulfate and 0.5 mL of ethanediamine were first put in polytetrafluoroethylene autoclaves. The mixture was then heated at 180 °C for 8 h. Then the collected product was put into 10 mL KOH (0.01 g/mL) solution for activation. After water was fully evaporated, the sample was heated at a rate of 5 °C/min to 700 °C in N<sub>2</sub> atmosphere for 1 h. After being cooled down to room temperature, the sample was washed with diluted hydrochloride acid and deionized water. The synthesized product was denoted as AC@sand which was microporous with a surface area of 61.58 m<sup>2</sup>/g. The HK model based pore size distribution curve was relatively narrow, showing a main pore width of 0.37 nm.

Chromium (VI) ion solutions were prepared by dissolving analytic grade K<sub>2</sub>Cr<sub>2</sub>O<sub>7</sub> (Tianjin Guangcheng chemical reagent company) in distilled water. AC@sand was added to 100 mL of the prepared chromium solution. The pH of the solution was adjusted by 18% HCl or 0.1 M NaOH, respectively. The mixture was shaken in an incubator at fixed temperatures for different contact times.

The concentrations of Cr(VI) (Cr<sub>1</sub>) in water were determined according to the standard of 1.5 Diphenylcarbohydrazide spectrophotometric method on a 722 visible light spectrometer (Jinghua, China). The concentrations of the total Cr atoms (Cr<sub>2</sub>) in water were determined on a PinAAcle 900T atomic absorption spectrometer (PerkinElmer, USA).

## III. RESULTS AND DISCUSSION

### A. Effect of Initial pH

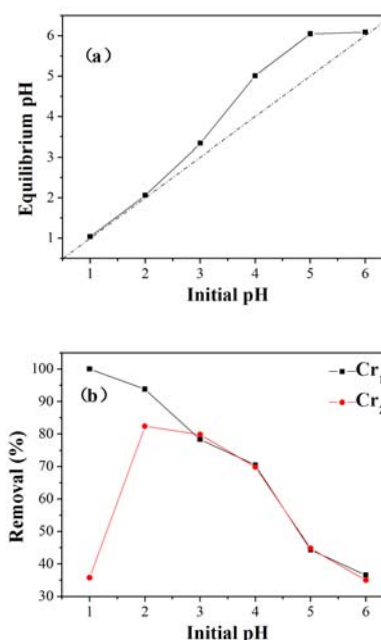


Figure 1. The effect of initial pH:

- (a) Effect of initial pH on equilibrium pH in the present of Cr(VI)  
(b) The removal of Cr with the change of the initial pH

The pH of solution is one of the most important factors influencing the adsorption efficiency of adsorbent. It affects not only the active sites on the adsorbent but also the solution chemistry of heavy metals in wastewater. Hydrolysis, complexation by organic and/or inorganic ligands, redox reactions and precipitation of the metal ions are influenced by pH [4]. The effect of pH on Cr(VI) removal was studied by adjusting initial pH from 1.0 to 6.0. One gram of AC@sand was added into 100 mL of Cr(VI) solution with the initial concentration of 5 mg/L.

As shown in Figure 1(a), the equilibrium pH levels of the solution were higher than the initial pH levels, indicating that the solution becomes more basicity than the initial one. The result suggests that the removal of Cr(VI) was accompanied by the consumption of  $H^+$  ions. Figure 1(b) shows that the removal of  $Cr_1$  by the AC@sand increases with increasing pH. It is known that Cr(VI) exists in aqueous solution as anions ( $HCrO_4^-$ ,  $[HCrO_4]^-$ ,  $[CrO_4]^{2-}$  or  $[Cr_2O_7]^{2-}$  [5-6]. The extent of protonation of the surface of the carbon layer decreased with increasing solution pH, vice versa. Thus, the electrostatic attraction at low pH and the electrostatic repulsion at high pH between the carbon layer and Cr(VI) anions would be promoted and hindered the Cr(VI) removal, respectively. However, it is also found from Figure 1(b) that the removal of  $Cr_2$  by the AC@sand increases when pH increases from 1.0 to 2.0, followed by an obvious decrease with increasing pH. When pH is lower than 3.0, the removal of  $Cr_2$  was much lower than that of  $Cr_1$ , and the difference between them becomes smaller. It indicated the occurrence of reduction of Cr(VI) to Cr(III). With the increase of pH value, the amount of the Cr(III) reduced decrease. Until pH 3.0, there is no Cr(VI) ions was reduced to Cr(III) because of the high pH. The produced Cr(III) ions at low pH could be released into aqueous solution by electrostatic repulsion between positively charged Cr(III) ions and protonated surfaces of the AC@sand. The lower total Cr removal at pH of 1.0 compared to that at pH of 2.0 were mainly due to the competition of excess  $H^+$  ions for sorption sites and the strong electrostatic repulsion between Cr(III) ions and positive charged carbon surface.

As a result, the removal of Cr(VI) by the AC@sand was the highest (about 100%) at the pH of 1.0, while the optimal pH for the total Cr removal was 2.0 (about 82.38%) due to both the adsorption and reduction of Cr(VI).

## B. Effect of Solution Initial Concentration

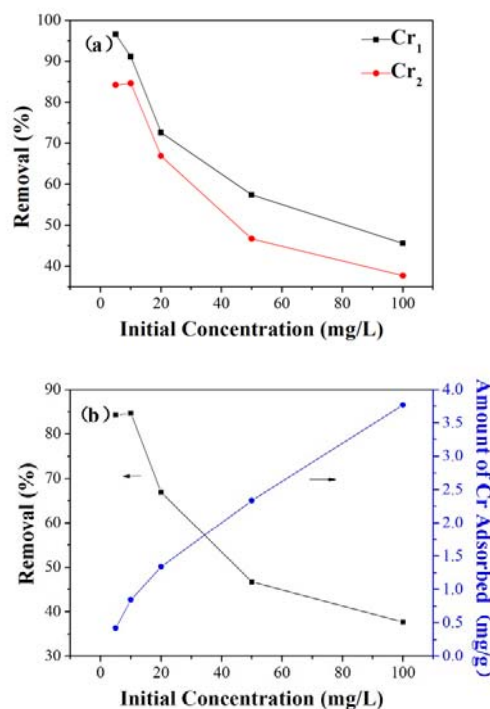


Figure 2. The effect of solution initial concentration:

- (a) The removal of Cr with the change of the initial concentration
- (b) The removal efficiency and amount of the total Cr adsorbed with the change of the initial concentration

To study the effect of initial concentration of Cr(VI) ions on the adsorption, the adsorption tests were carried out with varying initial metal ion concentrations (5, 10, 20, 50 and 100 mg/L) at 25 °C, using 1.0 g of adsorbent at pH 2.0.

In Figure 2, it shows that the removal efficiency of either the  $Cr_1$  or  $Cr_2$  decreases with increasing the initial concentration (Fig.2a), although the actual amount of Cr ions adsorbed by per gram of AC@sand increases with the increase in initial concentration (Fig.2b).

Isotherm equations based on Langmuir [7], Freundlich [8] and Temkin [9] models are listed in Table I and applied to fit the experimental data. In the equations,  $C_e$  (mg/L),  $q_e$  (mg/g),  $q_m$  and  $K_L$  are the concentration of analyte in solution, the amount of adsorbed analyte at equilibrium, Langmuir constants related to adsorption capacity (mg/g) and the energy of adsorption (L/g), respectively.  $K_f$  and  $1/n$  are the Freundlich constants related to sorption capacity and sorption intensity, respectively.  $K_t$  is the equilibrium binding constant (L/mol) corresponding to the maximum binding energy and constant B is related to the heat of sorption.

Comparison of the  $R^2$  values (Table I) for different isotherms show that the Freundlich adsorption model provides the best fit indicated by its largest  $R^2$  of 0.9714. Freundlich isotherm describes the heterogeneous surface energy by multilayer sorption, suggesting that the adsorption of Cr(VI) onto the AC@sand was multilayer and the

adsorbent surface was heterogeneous. Moreover, the value of  $1/n$  for Freundlich isotherm is found to lie between 0 and 1,

indicating that Cr ion was favorably adsorbed by AC@sand [8].

TABLE I. FREUNDLICH, LANGMUIR AND TEMKIN ISOTHERM CONSTANTS FOR CR ADSORPTION ON AC@SAND

Analyte	Isotherms		
	Langmuir	Freundlich	Temkin
Formula	$\frac{C_e}{q_e} = \frac{1}{q_m K_L} + \frac{C_e}{q_m}$	$\ln q_e = \ln K_F + \frac{1}{n} \ln C_e$	$q_e = B \ln K_t + B \ln C_e$
	$Y=0.2407x+2.6016$	$Y=0.4567x-0.2520$	$Y=0.6961x+0.4203$
Cr(VI)	$q_m = 4.1545$	$K_F = 0.7772$	$K_t = 1.8290$
	$K_L = 0.0925$	$1/n = 0.4567$	$B = 0.6961$
	$R^2 = 0.9427$	$R^2 = 0.9714$	$R^2 = 0.9218$

### C. Effect of Contact Time

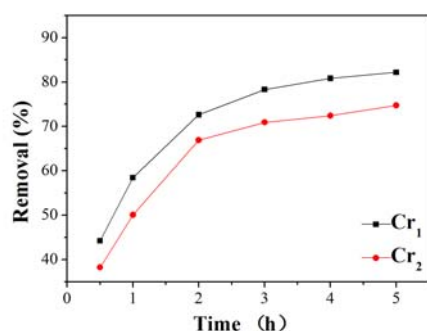


Figure 3. The removal of Cr with the change of the contact time

The equilibration time is one of the parameters for adsorption in economical wastewater treatment application. Many facts influence the equilibration time such as the transfer of metal ions caused by associated driving forces (shaking or concentration gradient), the availability of active sites [10], the binding interactions between the metal ions and functional groups ( $-NH_2$ ) located on the surface of the activated carbon and so on. In order to investigate the effect of contact time on the Cr(VI) removal by the AC@sand, 1.0 g of AC@sand was added into 100 mL of 20 mg/L Cr(VI) solution with pH of 2.0.

The effect of contact time on the adsorption of Cr(VI) ions on AC@sand is shown in Figure 3. It shows that the removal of both the Cr<sub>1</sub> and Cr<sub>2</sub> rapidly increase with the increase of the contact time within 2 h, but the increase becomes slower after 2 h. According to these results, an agitation time of 2 h is selected for the following the adsorption tests.

In the present study, kinetic models equations based on pseudo-first-order [11], pseudo-second-order [12] and intra-particle-diffusion [13] models are listed in Table II and applied to fit the experimental data. In the equations,  $q_e$  and  $q_t$  refer to the amount of Cr(VI) (mg/g) at equilibrium and at any time, respectively.  $K_1$  and  $K_2$  are the equilibrium rate constants of pseudo-first-order and pseudo-second-order adsorption ( $\text{min}^{-1}$ ), respectively.  $C$  is the intercept and  $K_{id}$  is the intra-particle diffusion rate constant.

Comparison of the  $R^2$  values (Table II) for different models shows that the pseudo-second-order kinetic model fits best since its largest value ( $R^2=0.9988$ ). The larger correlation coefficients of the pseudo-second-order model suggest that the kinetic model of the Cr(VI) ions adsorbed by AC@sand well follows the pseudo-second-order rate model. This means that the overall rate of Cr(VI) ions adsorption process seems to be controlled by the chemical process through sharing of electrons or by covalent forces through exchanging of electrons between adsorbent and adsorbate although it may be followed by additional layers of physically adsorbed molecules [4].

TABLE II. THE PSEUDO-FIRST-ORDER, PSEUDO-SECOND-ORDER AND INTRA-PARTICLE-DIFFUSION KINETIC MODELING CONSTANTS FOR CR ADSORPTION ON AC@SAND

Analyte	Pseudo-first-order		Pseudo-second-order		Intra-particle-diffusion	
Formula	$\ln(q_e - q_t) = \ln(q_e) - k_1 t$		$\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{t}{q_e}$		$q_t = k_{id} t^{\frac{1}{2}} + C$	
	$Y=-0.0007x+1.4229$		$Y=0.5958x+21.3450$		$Y=0.6124x+0.5256$	
Cr(VI)	$K_1$	$R^2$	$K_2$	$R^2$	$K_{id}$	$R^2$
	0.0007	0.8147	7.5771	0.9988	0.0612	0.8995

#### D. Effect of Temperature

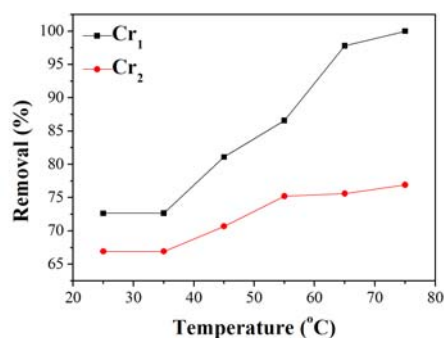


Figure 4. The removal of Cr with the change of the temperature

In order to investigate the effect of temperature on the Cr(VI) removal by the AC@sand, 1.0 g AC@sand was added into 100 mL of 20 mg/L Cr(VI) solution with pH of 2.0. As shown in Figure 4, at low temperature (between 25 and 35 °C), the removal of the Cr(VI) ions is a slightly bigger than that of the total Cr ions. But when the temperature is higher than 35 °C, the removal of the total Cr ions sharply increases. In contrast, the removal of Cr(VI) ions only slightly increases.

As we all know, carbon has the ability to reduce metal ions. The reaction needs heat to proceed. As a result, if the temperature is high enough under acidic condition, the Cr(VI) can be reduced by carbon layer thoroughly at the same time of the adsorption. In Figure 4, the difference between the removal of the Cr<sub>1</sub> ions and the Cr<sub>2</sub> is the reduced part of original Cr(VI) by AC@sand. It implies that the reduced part of original Cr(VI) increases with increasing the temperature.

#### IV. CONCLUSIONS

According to the experimental result, the optimal pH on removal of Cr(VI) by the AC@sand was 2.0 due to both the adsorption and reduction of Cr(VI). The removal of Cr(VI) ions depends on the initial metal ions concentrations and decreases with the increase of the initial metal ions concentration. The removals of both the Cr(VI) and total Cr increase with the increase of the contact time. The reduced part of original Cr(VI) increases with the increasing temperature. With the initial Cr(VI) concentration of 10 mg/L, the pH of 2.0, the contact time of 2 h and the temperature of 75 °C, 100% Cr(VI) was removed by the AC@sand through both adsorption (76.91 %) and reduction (23.09 %).

Freundlich adsorption model provides the best fit since its highest value, suggesting that the adsorption of Cr(VI) onto the AC@sand is multilayer and the adsorbent surface is heterogeneous. The pseudo-second-order kinetic model fits best, suggesting that the overall rate of Cr(VI) ions adsorption process seems to be controlled by the chemical process.

#### ACKNOWLEDGEMENT

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