

Finite element simulation, safety assessment and countermeasure of the coke drum leaning process during the quenching stage

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Abstract. The coke drum with a side channel at the beginning of cooling was simulated numerically using ANSYS, and the time history of the stress and strain fields were also acquired with indirect coupling method. The calculation results indicate that temperature stress and bending stress caused by the cold spots will cause bulging of the shell and the tilt of coke drum. With the coke drum tilting, the shell at the skirt seat will yield and the coke drum was in a dangerous state. The results of ANSYS show that the reinforcement of arc plate can effectively reduce the membrane stress on the skirt. The side channel and reinforcement of arc plate serve as the analysis for coke drum leaning and design of the skirt seat.

Introduction

Coke drums are vertical pressure vessels used in the delayed coking petroleum refineries and normally they are arranged in pairs, with alternating cycles between two drums [1]. In routine operation, coke drums experience preheating、filling stage、steam cooling、water cooling and coke removal. In preheating stage, the empty coke drum is heated to 350°C by injecting steam followed by hot vapor into the drum. In filling stage, the hot feed material, with a temperature ranging from 440°C to 500°C, is injected. At the end of the filling stage, a concentrated carbon material is produced and remains within the drum. After the coke has reached a predetermined level within the drum, usually 67% of the drum's capacity. Following this, these coke drums are cooled by vapor then a high rate of quenched water is injected into the drum, cooling the drum to an appropriate temperature. After the water cooling, the coke is cut by high pressure water from coke cutter.

Coke drums experience severe cyclic thermal and mechanical loadings and appear drums tilt、convex deformation and skirt cracking in the process of operation. The useful life of coke drums is much shorter than the designed value. At present, some researches had been carried out on the coke drums. But it is mainly aimed at the temperature field, convex deformation and skirt cracking of coke drums. For example, Zhong Wenzhen [2] analyzes the deformation mechanism of coke drums by using the bending theory of cylindrical shell. It is found that a periodical plastic residual deformation occurs in the quenching processes and increases with the running cycles of coke drums. The bulging deformation of coke drums mainly results from the progressive plastic deformation. Chen Sunyi [3] analyzes stress caused by the circumferential uneven temperature with the analytical and FEM. It is found that the circumferential uneven temperature field is one of the main factors of the sway and the slack of the anchor bolt nut of the tower. Ju Feng [4] analyzed the elastic plastic behavior of a coke drum subjected to both thermal and mechanical loadings based on abaqus. It is found that cold spots occurred in the quenching process will cause bulging of the shell. Wang Zheng [5] simulated the temperature field of the coke drum's working process by ANSYS. It is found that temperature change rate is high and the trend of thermal gradient variation is complex during the quenching process.

The middle channel model of coke had been used in the above research, without taking into

account the impact of uneven distribution of coke on the deformation of the tower. There is no paper on the quantitative safety evaluation and effective control measures for the tilt of coke drum in the quenching processes.

Tilt of the coke drums researched in this paper happened in the quenching process and restoration to the original position after the coke removal. The direction and size of the coke drums tilt are random, the maximum displacement at the top of tilt reached 160mm, after fastening bolts, the maximum tilt in 90mm. At the same time, it is found that when the coke drum produces different kinds of coke, the tilt of the coke drum will be different. Compared to asphalt coke with compact structure, the needle coke with the loose structure can cause more severe tilt of the coke drum. The periodic tilt of coke drum is not only harmful to the safe life, but also may cause the pipeline accident. Therefore, it is of great significance to study the tilt of coke drums at the quenching process. Based on the results of previous studies, a branched channel coke model is developed to study the tilt of coke drums at quenching stage by ANSYS. The variation of thermal stress and thermal deformation was calculated by the indirect coupling method. The results that the axial and circumferential temperature uneven distribution caused by the cold spots will make the coke drums bend at the quenching stage. With the coke drum tilting, the shell at the skirt seat will yield and the coke drum was in a dangerous state. The results of ANSYS show that the reinforcement of arc plate aimed at the insufficient strength of the skirt can effectively reduce the membrane stress on the skirt.

Finite element model of coke drum

Branched channel model of coke.

Foreign researchers have conducted studies on coke structure. Pohokinko [6] pointed out: When the axial feeding is adopted, the fluid coke tends to form the axial main channel and branched channel. These channels will remain at the end of the coking cycle due to the continuity of the movement. Great Laker of Carbon [7] researched the structure of needle coke from the coke drums. They put forward "dendritic structure". Due to the existence of nonuniform and random channeling flows of water through the residual coke mass during the quenching stage, certain locations of drum shell may be cooled down earlier than the surrounding areas, causing cold spots in the shell. Cold spot attacks may induce significant temperature differences and gradients in the structure, resulting in excessive stresses and strains. However, the middle channel without branched channel was widely used in scholars. In this paper, the branched was used to analyze the tilting process of coke drums in quenching stage. Figure 1 shows the coke model. The height of the coke layer is $\frac{2}{3}$ of the coke drums. The diameter is equal to the inner diameter of the tower. The diameter is chosen to be 320mm for the middle channel and 70mm for the branched channel.

Figure 2 shows the geometry of a real coke drum. The overall height and diameter of the coke drum are respectively 23888mm and 4850mm. The thickness of the base layer is 32mm for course 1, and 28mm for course 2, and 26mm for course 3, while the thickness of clad is 3mm for all courses. The materials for the clad and the shell are respectively TP410S stainless steel and 14Cr1MoR low alloy steel. The material for the skirt is Q345R and the thickness is 18mm. Their mechanical and thermal properties are given in reference [8].

The bottom of the skirt supported by ribs has great rigidity and it is no deformation. By increasing the elastic modulus of the supporting material, it can be used to simplify the model. In this paper, the 20 nodes 3D solid elements (solid 186) was used in the thermal analysis. To correspond with solid186, solid90 was used in the structural analysis. The mesh of the coke drum is shown in figure 3. The number is 596810 for elements, 1039925 for nodes, 5952890 for free degrees.

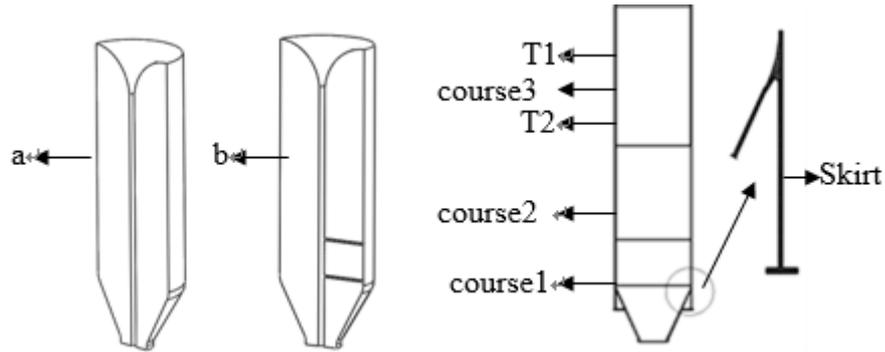


Fig. 1 middle channel model (a) and branch channel model (b) Fig. 2 geometry model of coke drum

Analysis of transient temperature field in coke cooling stage

Temperature change rate is high and the trend of thermal gradient variation is complex during water-cooling stage. It is the most dangerous time for the coke drum. At the beginning of the water-cooling stage, the coke drum tilted. In this paper, the transient temperature field of coke drum is simulated.

The temperature field at the end of steam cooling is used as the initial temperature field water-cooling stage. Temperature boundary condition is treated as follows: the adiabatic boundary condition is applied on the symmetry plane. The convective heat transfer coefficient of the insulation layer surface with the 20°C air is 10 W/(m²·K). The temperature of upper tower (T1、T2) and cooling water (T3) is known from operation date, as given in table 1. The convective heat transfer coefficient is 2.5×10⁵ W/(m²·K) for coke layer surface with cooling water, and 100 W/(m²·K) for upper tower with cooling water. According to this, the temperature field of the cooling-water stage is shown in figure 4.

Table 1 temperature of measurement points at water cooling stage

T/time	t=0h	t=0.5h	t=1h	t=1.5h	t=2h	t=2.5h	t=3h	t=3.5h
T1/°C	296	255	214	201	187	174	160	135
T2/°C	345	314	283	263	242	222	201	140
T3/°C	97	76	42	57	71	86	100	73

The axial temperature on the left side of coke drum covering by coke is first increases and then decreases. Due to the existence of branched channel, the location of branched channel was cooled down earlier than the surrounding areas. The cooling water through these branched channel, the temperature is 50°C for these locations, but 200°C for the surrounding areas. In the radial direction, the temperature of both sides increase from inside to outside.

Stress analysis of coke drum

Constraint and loading.

The internal pressure of 0.02MPa is imposed on the internal surface of the coke drum. The self weight of the coke drum material is considered by an acting gravitational force in vertical direction and a coke drum material density of 7850kg/m³ was used. The weight of the coke and quenched water were considered. The density of combination of coke and water is assumed to be 1481kg/m³ and this load is imposed as a hydrostatic pressure in the inner drum surface. The structural boundary conditions as follows: the Z displacement of meridian plane is zero. The underside of base-ring is ALL DOF.

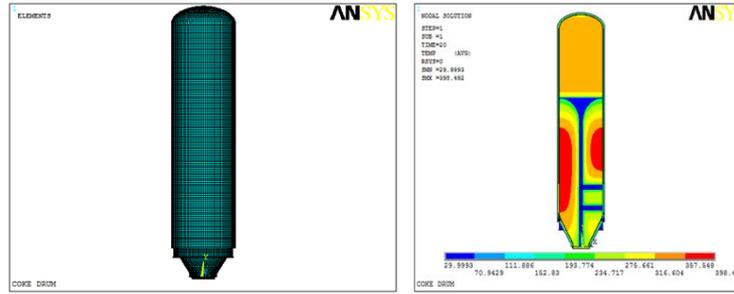


Fig. 3 finite element mesh of coke drum Fig. 4 temperature field of quenching stage

Coke tower deformation analysis.

The deformation of the coke column in the water-cooled stage is shown in figure 5. The maximum displacement is 68.7mm (DMX in figure) for the middle channel, 76mm for the branched channel. There is no tilt for the middle channel model. At the beginning, tilt of the coke drum is 23mm for the branched channel and 31mm at the end of the cooling-water stage. Compared with the middle channel, it is known that the branched channel caused the tilt of coke drum. Water through the channel during the quenching stage, certain locations would be cooled down earlier than the surrounding areas, causing cold spots. Cold spots caused the uneven distribution of thermal stress make the coke drum bend and tilt.

Stress analysis of coke drum.

The stress intensity of the tilted coke drum is research emphasis. Compared figure 10 with 11, the maximum stress at the skirt is increased by 80 MPa for the coke drum tilting. Based on the JB4732, the membrane stress of skirt up to 403MPa. It is higher than yield strength of Q345R. The maximum stress of perforated areas reached 242MPa and the membrane stress is as high as 155.5MPa. In addition, the maximum stress for the boundary area is 182MPa, but the membrane stress is only 73.2MPa. The stress in other areas of the coke drum is very low.

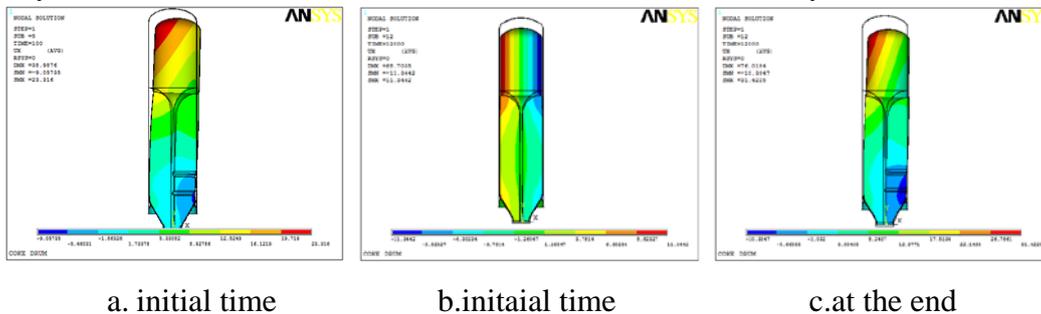


Fig. 5 horizontal displacement of branch channel model (a,c) and middle channel (b)

Design of skirt reinforcement

It is known that the skirt is insufficient strength. In this paper, reinforcement of arc plate was adopted to reduce the membrane stress of skirt. The 3D modal for the reinforcement of arc plate are depicted in figure 6. Due to the existence of reinforcement of arc plate, the membrane stress of skirt reduced to 219MPa from 403MPa. It is shown that the reinforced plate arc is an effective reinforcement measures.

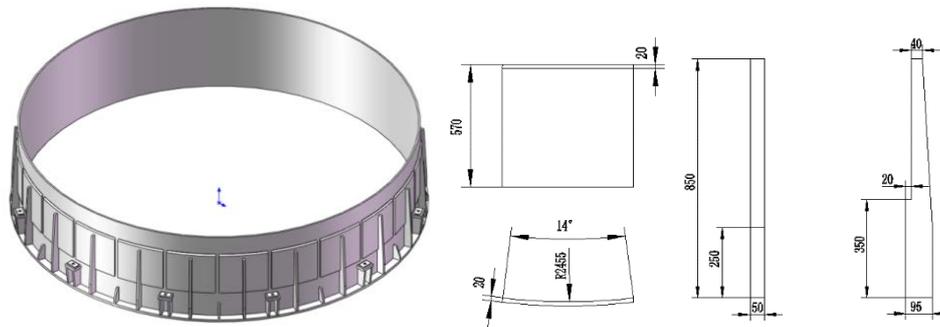


Fig. 6 3D modal of skirt with arc plate and size structure of arc plate stiffened plate

Conclusions

A finite element model of coke drum with branched channel was established to know the tilted process of coke drum at the quenching stage. It is known that temperature stress and bending stress caused by the cold spots will cause bulging of the shell and the tilt of coke drum. With the coke drum tilting, the shell at the skirt seat will yield and the coke drum was in a dangerous state. The reinforced plate arc is an effective reinforcement measures to reduce the membrane stress of skirt.

Field research from Japanese enterprises, it is known that loosening foundation bolt can effectively reduce the bending stress of skirt. But the displacement of coke drum will be bigger. So in the premise of ensuring the safety of the gas pipeline, it is one of the feasible solutions.

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