

Voltage Distribution in Power Transformer Winding under Transient Impulse

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Abstract. Field experience verifies that even when good insulation coordination studies and well-accepted insulation design practices are applied, power transformers suffer dielectric failure as reported in the literature. The analysis of the failures and prevention of transformer require comprehensive knowledge of the transient voltages distribution in transformer winding. So this paper constructs a transformer circuit model to calculate transient voltage distribution along the transformer winding, which is based on a multiconductor transmission line (MTL) model. The simulated transient voltage distribution of axial series capacitance and shunt capacitance to ground is analyzed and proved out in the paper, which are in accord with the existing conclusion.

1. Introduction

In service, the transformer insulation system is subjected continuously to operating voltages and occasionally to over-voltages [1-3]. Due to these transient voltages, transformers must be subjected to impulse tests to prove the Basic Insulation Level (a method of expressing the magnitude of the voltage surge that a transformer will tolerate without dielectric breakdown) according to specific standards. In view this point, it is significant to investigate transient over-voltages transient overvoltage by different methods [4-8]. G. B. Gharehpetain put forward a hybrid model of the black box model with the detailed model superimposed m segments, which solves the problem of using different structure types in the same coil [9]. Z. J. Wang proposed a multi-transmission line distribution parameter model and the double disk circle lumped parameter model of the hybrid model, to better solve the inter-turn oscillation [10, 11]. In this paper, a simulation circuit for high-frequency impulse effect was established based on the multi-conductor transmission line (MTL) theory. The circuit could simulate and verify the transient voltage distribution along winding, voltage between turns and voltage of nodes to earth. In addition, the simulation results can help to assess the damage of transformer insulation and adjust transformer insulation design flexibly.

2. Model of Transformer Windings

2.1 MTL Theory. For continuous-type transformers, the windings were turned on at each turn, and the entire winding became a multi-coupled and end-to-end transmission line, so that the winding could be modeled as a loss uniform multi-conductor transmission line [12]. Figure 1 displays the model of the transformer windings by its individual turns, where $U_S(i)$, $I_S(i)$, $U_L(i)$ and $I_L(i)$ represents the voltage and current vectors at the beginning and end of the conductor correspondingly. The model could also be described by the following equation:

$$\begin{aligned} \frac{d\mathbf{U}}{dx} &= -(\mathbf{R} + j\omega\mathbf{L})\mathbf{I} \\ \frac{d\mathbf{I}}{dx} &= -(\mathbf{G} + j\omega\mathbf{C})\mathbf{U} \end{aligned} \quad (1)$$

where \mathbf{U} and \mathbf{I} are the voltage and current vectors at position x along the lines; \mathbf{R} , \mathbf{L} , \mathbf{G} , and \mathbf{C} are the per unit length resistance, inductance, conductance, and capacitance matrix, respectively.

According to [12], the transfer function from the terminal of arbitrary turn k to the input is

$$A(k) = \frac{U_R(k)}{U_S(1)} = \frac{T(k+1,1)T(N+1,N+1) - T(k+1,N+1)T(N+1,1)}{T(1,1)T(N+1,N+1) - T(N+1,1)T(1,N+1)} \quad (2)$$

where \hat{Y} is a $(N + 1) \times (N + 1)$ matrix, and $T = \hat{Y}^{-1}$.

According the equation 2, we can calculate the voltage distribution of the transformer windings at any time.

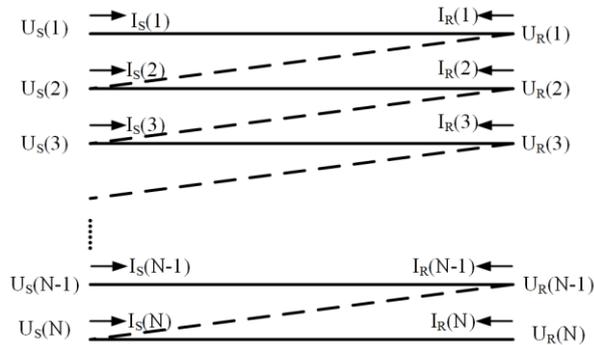


Fig. 1. Multi-conductor transmission line model

2.2 The Equivalent Circuit Model. As turns should be considered and this leads to a large number of equations and solving the problem requires very large matrix operations, the equivalent circuit built up in turn is too complex to simulate and calculate. When the coil length of each line disk is far less than 1% of the wavelength of lighting, an equivalent circuit of transformer winding based on the disk unit was established, as shown in Figure 2.

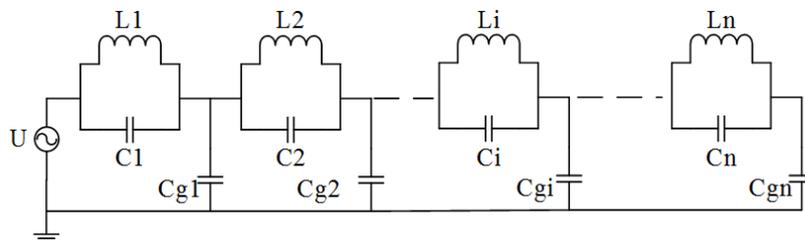


Fig. 2 Circuit diagram for simulation

The equivalent circuit is constituted of continuous lumped parameter components such as L_1, C_1, C_{g1} which are usually used to study the transient response of windings. In Fig2, L_1, L_2, \dots, L_n represent inductance along the windings, and $C_{g1}, C_{g2}, \dots, C_{gn}, C_1, C_2, \dots, C_n$ respectively represent the capacitance to ground along the windings and inter-turn capacitance. Therefore, taking the disk as unit the model of transform windings was established.

In this paper, the transient voltage was defined for standard lightning impulse (1.2/50 μ s), and the amplitude was 2MV. The simulation transformer has 108 disks, and the part of the equivalent parameters is shown in Table 1. The capacitance of C_{gi} in the model is 40pF.

Table 1. Equivalent parameter of transformer winding

L_1 /mH	L_2 /mH	L_3 /mH	L_4 /mH	L_5 /mH	L_6 /mH	L_7 /mH	L_8 /mH	L_9 /mH
0.2824	0.2996	0.3180	0.3180	0.7447	1.7227	3.9480	5.4865	7.8453
C_1 /pF	C_2 /pF	C_3 /pF	C_4 /pF	C_5 /pF	C_6 /pF	C_7 /pF	C_8 /pF	C_9 /pF
8265	8265	3397	1454	985	300	300	300	300

3. Results and Discussion

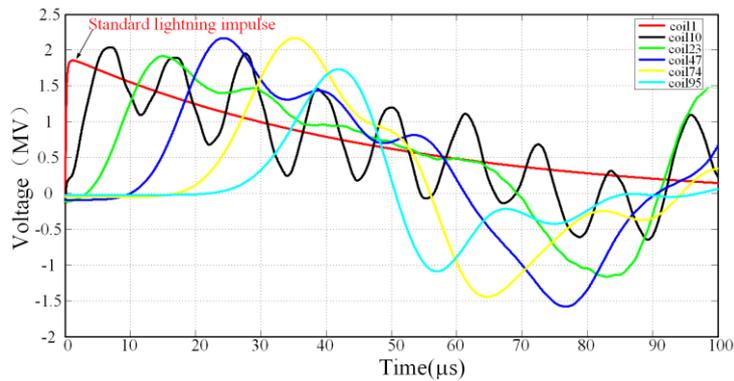


Fig. 3 Transient Voltage Waveform under Standard Lightning

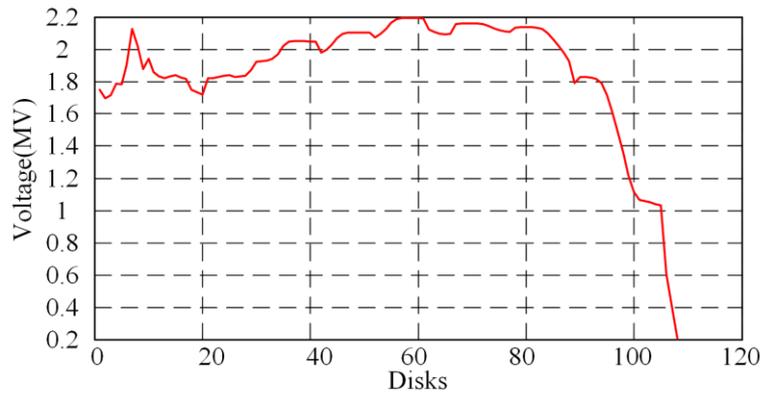


Fig. 4 Voltage distribution of each disk

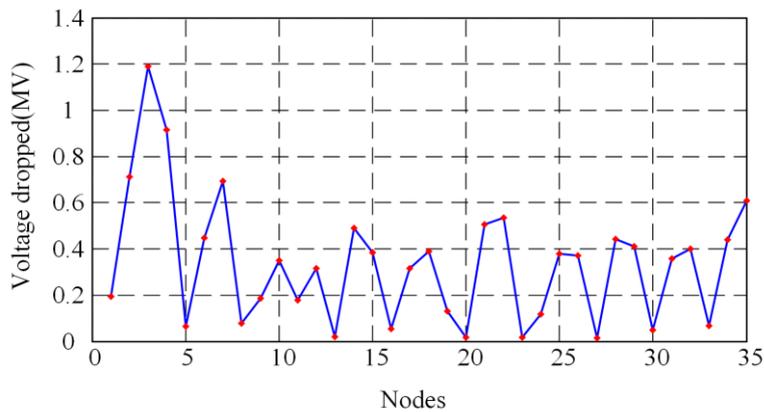


Fig. 5 Voltage drop between disks

The voltage distributions of several nodes are shown in Figure 3. The simulation results manifested that the voltage at the No. 74 is the largest and the voltage amplitude of the middle part is higher than that of the first part.

The peak voltage distribution of each disk under the lightning wave was shown in Fig 4. And Fig 5 presented the voltage drop between the disks. The simulation results indicated that the maximum voltage was in the middle of the winding under the lightning impulse, and the maximum voltage drop between disks appeared the beginning of the winding.

Summary

ATP-EMTP simulation are used to calculate the distribution of transient voltage in electric power transformer windings. When the lightning impulse imposed at the first turn of coils, the maximum voltage is in the middle layer winding disk , and the maximum voltage gradient is appeared in the first section of the winding. The simulation results demonstrated the transformer equivalent circuit used in

this paper is suitable to analyze the voltage distribution on the transformer windings under transient impulse.

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