

# A method for determining the spatial attitude of the mooring system

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**Abstract.** In this paper, the stress condition and design method of single point mooring system in shallow water observation network are studied. We analyze the force condition of the whole system, through the stress point of the lower end of the chain hypothesis, we can get the relationship between the depth of water and the stress of each part of the system, and find out the spatial distribution of each part. According to different situations, we can use this method to design the mooring system. In this paper, the problem of different wind speed and water flow is also discussed, and the corresponding solutions are given.

**Keywords:** Mooring System, Moment-equilibrium, Force analysis, binary chop

## INTRODUCTION

The transmission nodes of near shallow sea observation network are composed of buoy system, mooring system and underwater acoustic communication system. The buoy system is simplified to the shape of cylinder, the mooring system is composed of a steel pipe (4 section), steel drums, heavy ball, welding anchor and special anti drag anchor. The angle between the tangent direction of the link chain requirements and the end of the anchor and seabed does not exceed 16 degrees, or the anchor will be towed away. The underwater acoustic communication system is installed in a sealed cylinder. When the vertical steel drum, underwater acoustic communication equipment work best. If the drum tilt, will influence the equipment working effect. When the tilt angle (the angle between the steel drums and vertical lines) more than 5 degrees, the poor equipment working effect. We can hang heavy ball to control the inclination angle steel. We mainly study the attitude of each part of the mooring system.

Known parameters are as follows:

Buoy cylinder: diameter 2m, high 2m, mass 1000kg

Anchor: 600kg

Steel pipe: length 1m, diameter 50mm, mass 10kg

Sealed cylinder: length 1m, diameter 30cm, total mass 100kg

Anchor: length 105mm (a section), mass per unit length 7kg/m

Schematic diagram is as follows:

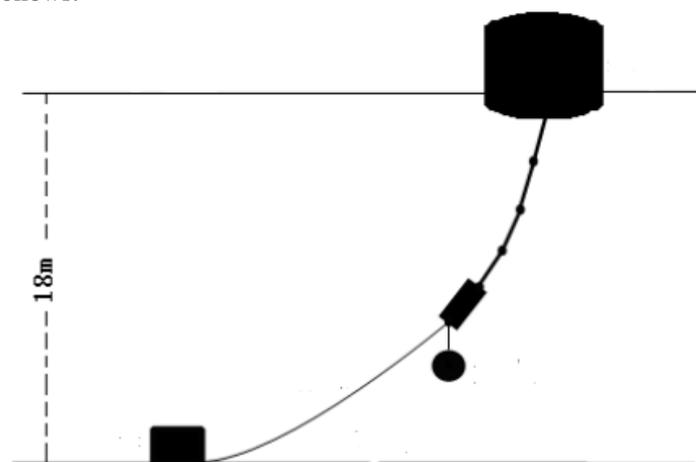


FIGURE1. Transmission node diagram

## ASSUMPTIONS

1. It is assumed that all elements in the system are rigid bodies, which can not be elastically deformed.
2. Assuming that the flow velocity is uniform, ignoring the wave action.
3. Center of gravity hypothesis and equipment at the geometric center of steel drums.
4. Assuming that the heavy ball is a solid steel ball.

5. Offshore wind load can be calculated by the approximate formula  $F=0.625 \times S v^2(N)$ ,  $S$  is the projection of wind in normal plane.  $v$  is wind's velocity.

6. Near sea water flow force can be calculated by approximate formula  $F=374 \times S v^2(N)$ .  $S$  is the projection of flow in normal plane.  $v$  is flow velocity .

**SYMBOL SPECIFICATION**

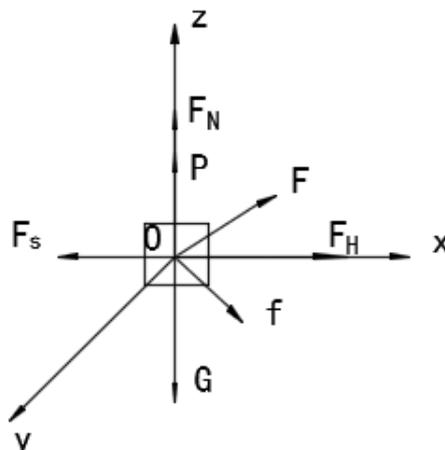
**TABLE1.**Symbol and its meaning

symbol	meaning
$P$	the sum of the buoyancy of the system (N)
$G$	the sum of the gravity of the system (N)
$P_i$	buoyancy of parts themselves (N)
$G_i$	gravity of parts themselves (N)
$\theta_i$	the angle between the pull force and the horizontal direction of the parts ( $ \theta_i  \leq 90^\circ$ )
$F$	wind power(N)
$\alpha_i$	angle of part and horizontal direction
$T_i$	tension between parts (N)
$M_T$	moment(tension)(N)
$M_{GP}$	moment(Gravity and buoyancy)(N)
$m_0$	mass of heavy ball (kg)
$F_s$	static friction of anchor(N)
$F_N$	support of seabed to anchor(N)
$\rho$	seawater density(kg/m)
$m$	mass of buoy(kg)
$S'$	base of buoy(m <sup>2</sup> )
$H$	height of buoy(m)
$l$	bottom diameter of buoy(m)

**ESTABLISHMENT OF SPATIAL MODEL**

**Balance of forces**

In this paper, the spatial coordinate system is established based on the anchor point. We take the direction of water flow and wind force for X axis forward, take vertical direction as Z axis.<sup>[1]</sup> We have made the stress diagram of system as follows:



**FIGURE2.**stress diagram of system

Because of the force balance of the system, we know  $\vec{F}_H = \vec{f} + \vec{F} = -\vec{F}_S$ , so our analysis of the anchor is as follows:

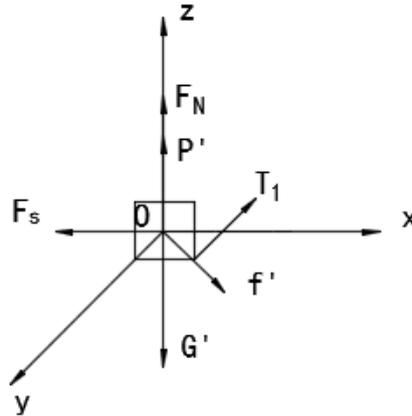


FIGURE3. stress diagram of anchor

Anchor received force of friction ( $F_S$ ), force of wind and flow ( $F_H$ ), stamina of seabed ( $F_N$ ), tension of anchor chain ( $T_1$ ), gravity and buoyancy ( $G'$  and  $P'$ ). Because of the force balance of the anchor, is the force on plane  $XoZ$ , and  $F_H$  is the component in the x direction.  $F_H \tan \theta_1$  is the component in the z direction.

Then, we analysis the stress condition of the first anchor chain, we can show all of the forces through the following figure.

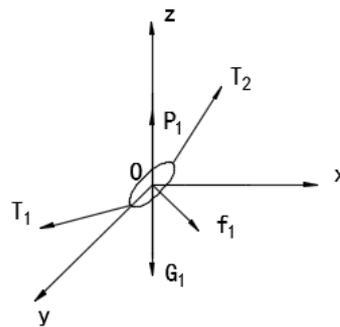


FIGURE4. stress diagram of the first anchor chain

Its force include: gravity and buoyancy, tension between anchor and chain ( $T_1$ ), the angle between the force and the plane is  $\theta_1$ , the force of the next section chain is  $T_2$ , the angle is  $\theta_2$ . Through the analysis of its force, we can get components in every direction. By this way, we can know the tension of the last chain ( $T_{i+1}$ ), its component in x direction

is  $F_H + \sum_{m=1}^i f_{mx}$ ,  $\sum_{m=1}^i f_{my}$  in y direction,  $F_H \tan \theta_1 + \sum_{m=1}^i (G_m - P_m)$  in z direction.

Due to the influence of the metal ball, we analysis the stress condition of steel pipes and the steel drum (we take the steel drum as example). First, we analysis the stress condition of the heavy ball.

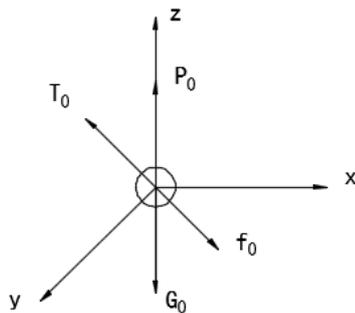


FIGURE5. stress diagram of the heavy ball

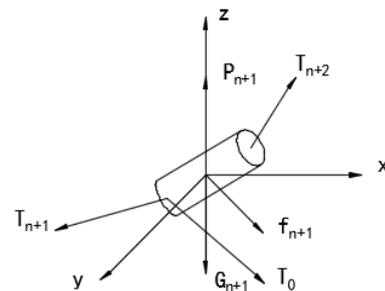


FIGURE6. stress diagram of the steel drum

The component of  $T_0$  in x direction is  $f_{0x}$  (the component of the force of wind and flow in x direction),  $f_{0y}$  in y direction (the component of the force of wind and flow in y direction),  $G_0 - P_0$  in z direction. As for the steel drum, the component of  $T_{n+2}$  (we suppose there are n section anchor chains) in x direction is  $F_H + \sum_{m=1}^i f_{mx} + f_{0x}$ ,  $\sum_{m=1}^i f_{my} + f_{0y}$  in y direction,  $F_H \tan \theta_1 + \sum_{m=1}^i (G_m - P_m) + G_0 - P_0$  in z direction.

At last, we analyze the stress condition of the buoy, we mark out the force of the buoy in figure 7.

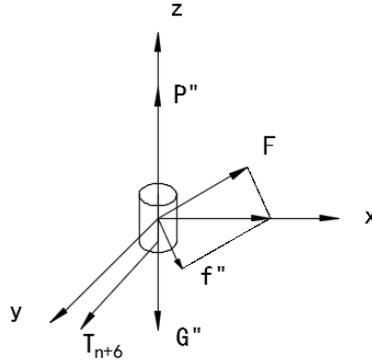


FIGURE 7. stress diagram of the buoy

From the figure, we analyze the force in z direction. we conclude:

$$F_H \tan \theta_1 + \sum_{m=1}^i (G_m - P_m) + G_0 - P_0 = \rho_l g S' h \tag{1}$$

### Moment-equilibrium

For the similar stress condition, the analysis of the moment to the part of the system is similar too.<sup>[2]</sup> In order to solve the problem, we build a space coordinate system like following:

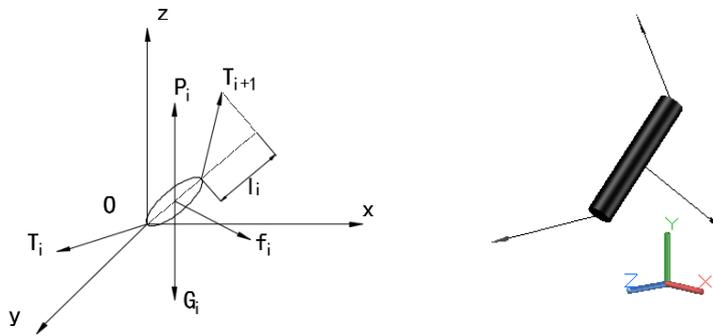


FIGURE 8. moment-equilibrium of the anchor chain

We set the top of the anchor chain as coordinate  $(x, y, z)$ , and  $x, y, z$  satisfy the equation  $l_i^2 = x^2 + y^2 + z^2$ ,  $l_i$  is the length of the anchor chain<sup>[3]</sup>. We regard some forces on the centroid of the chain, like wind, flow, buoyancy and its gravity, we view them as a composition  $(a_3, b_3, c_3)$ . We know there different tension in its two ends, because of the balance of the three forces to keep the chain, they must in a plane. We use vector to describe the tension on the end of the chain. We move  $T_{i+1}$  to the coordinate origin as  $T'_{i+1}$ . We can show them in the following:

$$\vec{T}_i (F_H + \sum_{m=1}^{i-1} f_{mx}, \sum_{m=1}^{i-1} f_{my}, F_H \tan \theta_1 + \sum_{m=1}^{i-1} (G_m - P_m)) \tag{2}$$

$$\vec{T}'_{i+1} (F_H + \sum_{m=1}^i f_{mx}, \sum_{m=1}^i f_{my}, F_H \tan \theta_1 + \sum_{m=1}^i (G_m - P_m)) \tag{3}$$

In order to simple the model, we use  $(a_1, b_1, c_1) (a_2, b_2, c_2)$  to describe  $\vec{T}_i$  and  $\vec{T}'_{i+1}$ , in this way, we can use moment-equilibrium to get a quadratic equation with three variables.

$$\begin{cases} l_i^2 = x^2 + y^2 + z^2 \\ x_0x + y_0y + z_0z = 0 \\ 2l_i\sqrt{a_2^2 + b_2^2 + c_2^2 - (xa_2 + yb_2 + zc_2)^2} = l_i\sqrt{a_3^2 + b_3^2 + c_3^2 - (xa_3 + yb_3 + zc_3)^2} \end{cases} \quad (4)$$

In this way, we can get the value of z. By analysis all parts of the system, we can conclude  $\sum_{m=1}^{n+5} z_m + h = H$ .

**Example calculation**

If the depth of water is at the range of 16 to 20 meter, the maximum of wind is 36m/s, the maximum of flow is 1.5m/s. In this method, we conclude that there are 258 section chains and the ball's mass is 4630.811kg.

We test out the system in different condition like this:

TABLE 2. System competition (depth 16m, wind speed 36m/s)

flow speed(m/s)	drum tilt angle	buoy movement range(m)	section of hanging chain	Steel pipe inclination angle
1.5	5.0000	25.4955	258	4.67
1.0	2.7751	24.2628	193	2.61
0.5	1.3692	23.1058	149	1.31
0.0	0.9074	22.3814	131	0.90

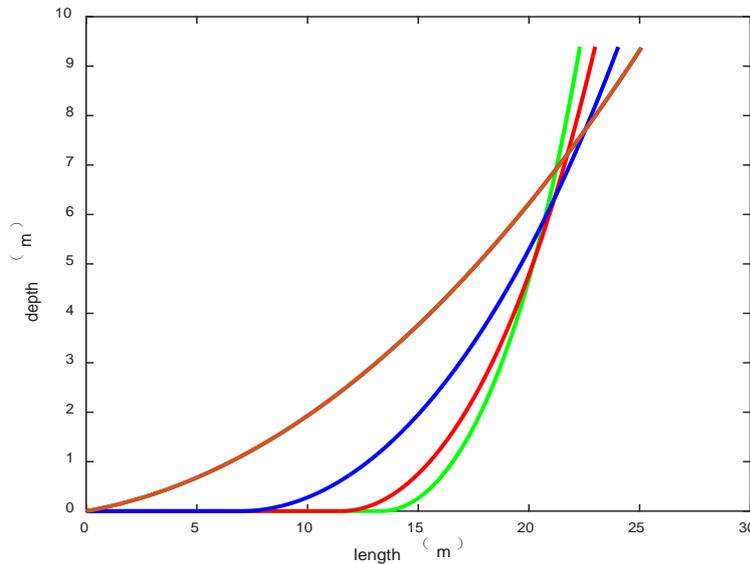


FIGURE 9. the shape of the chain in the water (brown 1.5m/s, blue 1.0m/s, red 0.5m/s, green 0.0m/s)

**CONCLUSION**

By using the force balance and moment balance, the spatial model of the mooring system is established. We can understand every parts of the system, both in force and gesture. In this way, we can design mooring system in different environment, to keep the instrument work well, and get the different parts' parameter. What's more, we should care that sometimes the total section chain are not hanging, there are some chain in the seabed.

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**REFERENCES**

[1] Detao Luo, Jiading Chen, Static analysis of mooring positioning system, Ship Engineering, Vol 3, 1982  
 [2] Ruijie Zheng, Internal forces analysis of mooring system, Dalian University of Technology, 2006(6)

[3]Triantafyllou MS.Preliminary Design of Mooring System[J].1982,26(1):25-36