

Simulation Research on Hydraulic Support Based Virtual Prototyping

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Abstract—To overcome limitations of current designs of hydraulic supports based on conventional physical prototype, we propose a virtual prototyping based design mode for hydraulic supports. In this study, a 3D numerical model of hydraulic support was established by numerical simulations and stress distributions on hydraulic support were investigated. Also, motion simulation and interference detection of the working process of hydraulic supports were involved. The results indicated that the proposed hydraulic support based virtual prototyping is viable and the simulation results are consistent with practical working conditions of hydraulic supports. Indeed, virtual prototyping can improve the design method and reduce the design period. This study facilitates optimized design of hydraulic supports, thus providing references for industrial applications.

Keywords—virtual prototype, hydraulic support, simulation

I. INTRODUCTION

As a key equipment for work safety in coal mining, hydraulic support is usually working under complicated geological conditions and in harsh environment. Owing to the high cost of hydraulic supports (100, 000 to 1, 000, 000 RMB), a physical prototype of hydraulic support for tests is quite challenging and the tests are usually destructive. Additionally, detections of failure cause and fault points in practical tests are usually extremely difficult due to the sophisticated structure and interactive components. Therefore, the physical prototype based mode severely limits improvements of hydraulic support design. With virtual prototyping, the design concepts and structural components can be dynamically visualized. In this way, any single component can be modified easily. Additionally, kinematic and dynamic characteristics of hydraulic supports can be evaluated by virtual simulations so that problems can be identified and the product design can be optimized. Currently, virtual prototyping based designs for hydraulic supports have been intensively studied. References[1-4] proposed 3D entity modeling of hydraulic supports using 3D mechanical design

software and defects in the design can be visualized and easily handled. References [5-17] reported finite element analysis of bearing characteristics of key components in hydraulic support using 3D numerical modelling and proposed optimization of structural design. References [18-21] established a kinematic model of hydraulic supports and reported kinematic and dynamic simulations of hydraulic supports, followed by design optimization. Additionally, a virtual prototype analysis platform was established for virtual prototypes using SolidWorks. Kinematics of components in the hydraulic support system were obtained by motion simulation and dynamic interference detection [22-24].

In summary, owing to sophisticated structures of hydraulic supports, most studies involving structure simplification in 3D modeling and precise 3D modeling of hydraulic supports are widely absent. Meanwhile, strength analyses were applied for key structural components only and few studies involved entire frame finite element simulations of hydraulic supports. Therefore, this study proposes precise 3D modeling of hydraulic supports and entire frame force analysis and motion simulation of hydraulic supports to investigate their stress distribution and motion, thus providing references for design optimization of hydraulic supports.

II. 3D MODELLING OF HYDRAULIC SUPPORT

A. 3D modelling of components

The model was established using software (Pro/E). Figs. 1, 2, 3, 4, 5, and 6 shows the models of base, head beam, shield beam, front and back connecting rods, column, and lifting jack of the hydraulic support, respectively.



Fig.1 The base



Fig.6 The lifting jack

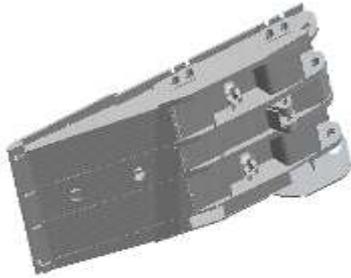


Fig.2 The head beam

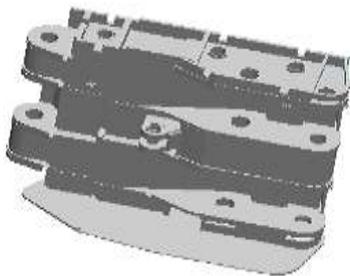


Fig.3 The shield beam



Fig.4 The front and back connecting rods



Fig.5 The column

B. Virtual prototyping based hydraulic support

Upon design of individual components, assembly of these components can be achieved accordingly. The assembly of components is indeed position constraints of these components. The assembly model of hydraulic support is regarded as a system of consisting of several sub-assemblies, including base, pre and post connecting rods, shield beam, head beam. The Pro/E allows three constraints, including “place”, “move”, and “connect”. To allow motions of assembled components, “connect” was applied for support assembly in this study. Fig.7 shows entity model of assembled hydraulic supports.

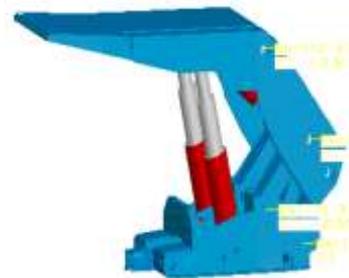


Fig.7 3D model of the hydraulic support

III. FINITE ELEMENT ANALYSIS OF HYDRAULIC SUPPORT

A. Boundary Conditions

During mining processes, the supports experience both supportive forces by columns and pressures by wall rocks in the work face. For tests, forces by wall rocks on underground support were reflected by applying different bearers. If the force on support by bearer is regarded as an external load, the hydraulic support is a hyper-static system and the force on support by bearer cannot be calculated using force equilibrium equation. Therefore, the force by bearer is regarded as part of boundary conditions instead of an external load.

B. Load Determination

As the bearer is regarded as part of the boundary conditions, the external loads are loads on the head beam by the two columns. Herein, the resistance to hydraulic support was 31.5 Mpa and the supportive force by each column was 15.75 Mpa. With safety factor of 1.2, the load on head beam was $15.75 \times 1.2 = 20$ MPa. Among all working conditions of hydraulic support, load concentration on head beam end points, eccentric loading on beam, head beam torsion, base torsion, and load concentration on base end points should be particularly investigated. This study involves simulations of hydraulic supports under these working conditions.

C. Strength Analysis of Load Concentration on Head Beam End Points

Selecting SOLID 95 and free gridding led to 75259 units and 127827 nodes, as shown in Fig. 8. The bearer was regarded as a constraint and the loading location is as shown in Fig. 9. As shown in Fig. 10 and Fig.11, the maximum displacement was 6.068 mm and the maximum stress was 467.418 MPa. Meanwhile, stress concentrations on bearer are significant, which is consistent with actual working conditions.

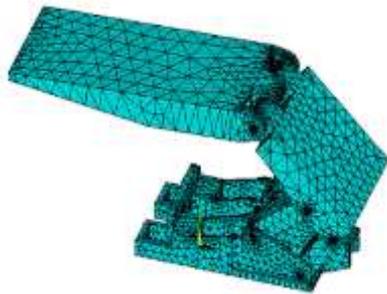


Fig.8 The meshing of the hydraulic support

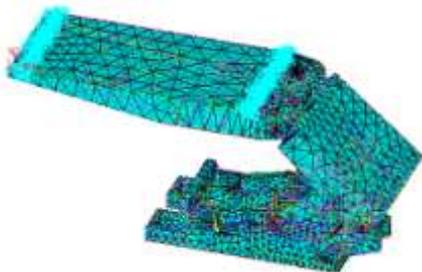


Fig.9 The loading position of two side of top beam

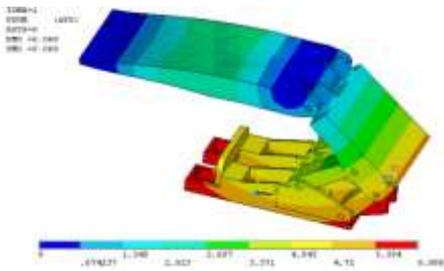


Fig.10 The displacement of the top beam

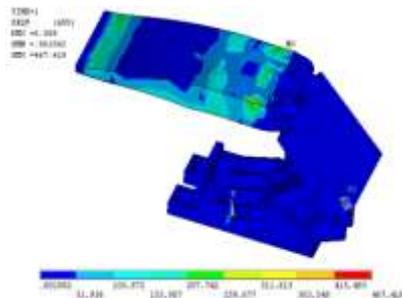


Fig.11 The stress of the top beam

D. Strength Analysis of Head Beam Torsion

The bearer was regarded as a constraint and its location is as shown in Fig. 12.

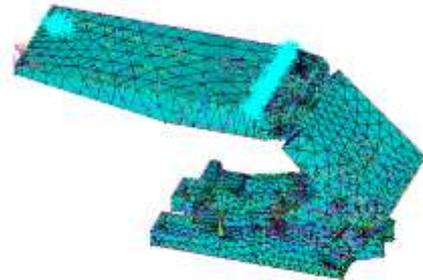


Fig.12 The position of the stepping-block

The DOFs of base bottom node in Y direction and the presser contacting with the head beam in X, Y, and Z directions along the axis were constrained, as shown in Fig. 13. Applying plane loads and the results obtained are as shown in Fig. 14 and Fig.15.

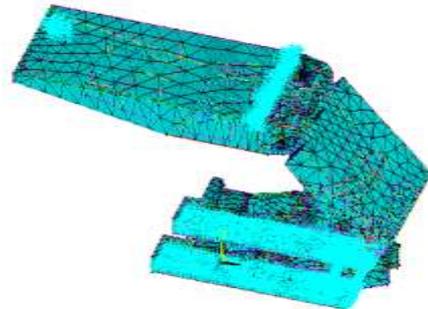


Fig.13 The loading restriction

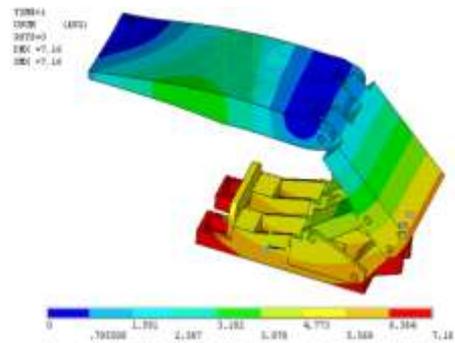


Fig.14 The torsion displacement of the top beam

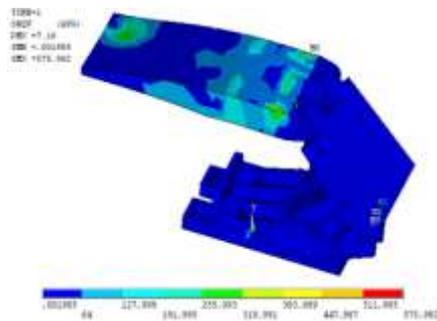


Fig.15 The torsion stress of the top beam

According to the displacement cloud chart, the maximum displacement in the presence of torsion loads on head beam was 7.16 mm. According to the stress cloud chart, the

maximum stress was 575.982 MPa and it appeared at the connection point of bearer and the head beam. Meanwhile, most severe stress concentrations were observed at the constraint bearer.

E. Strength Analysis of Load Concentrations on Base End Points

As shown in Fig. 16, the bearer was regarded as a constraint. The displacement cloud chart (Fig. 17), the geometric shapes before and after deformations (Fig. 18), and the stress cloud chart (Fig. 19) were obtained by finite element analysis. As observed, the maximum stress was 382.342 MPa.

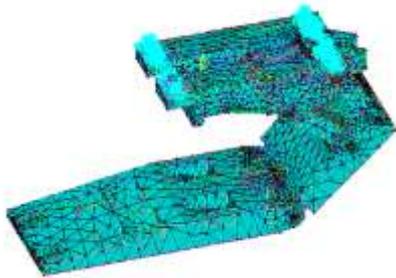


Fig.16 The position of stepping-block of the base

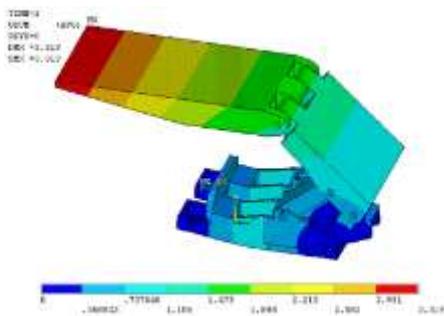


Fig.17 The displacement of concentrated loading of the base



Fig.18 The deformed nephogram of concentrated loading of the base

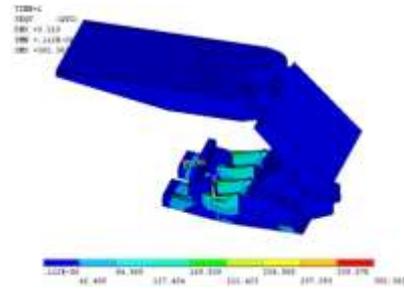


Fig.19 The stress of concentrated loading of the base

F. Strength Analysis of Base Torsion

Applying vertical constraints on the bearer and free gridding led to 85672 units and 143468 nodes, as shown in Fig. 20. By applying loads along the axial direction of the column, base torsion deformations (Fig. 21), torsion displacement cloud chart (Fig. 22), and stress cloud chart (Fig. 23) were obtained by analysis using the ANSYS software. As observed, the maximum displacement and stress of the support in the presence of base torsion loads were 5.004 mm and 648.723 MPa, respectively. The maximum stress observed was significantly higher than those in other cases mentioned above but is within the yield strength of the material.

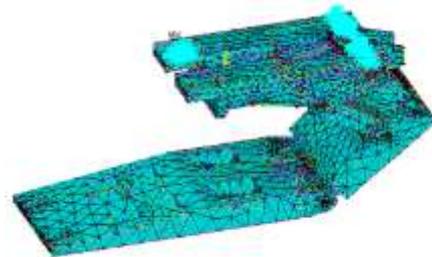


Fig.20 The position of the stepping-block of torsion loading of the base

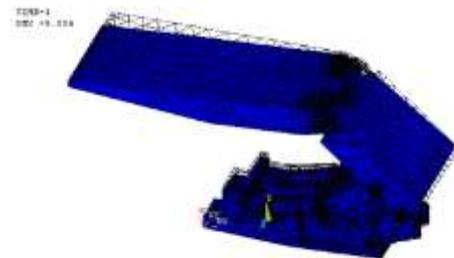


Fig.21 The deformed nephogram of torsion loading of the base

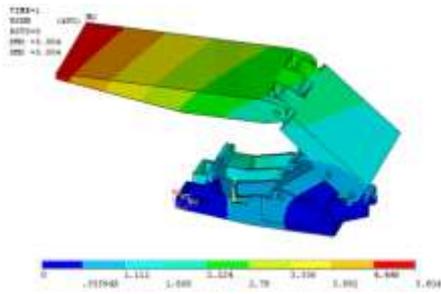


Fig.22 The displacement of torsion loading of the base

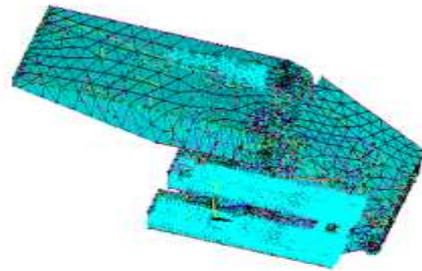


Fig.25 The one side loading restriction top of the beam

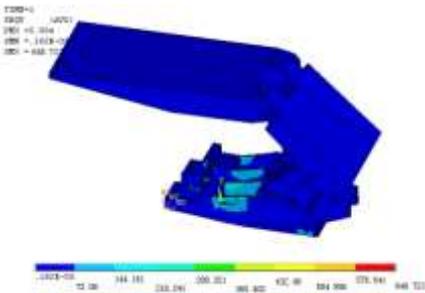


Fig.23 The stress of torsion loading of the base

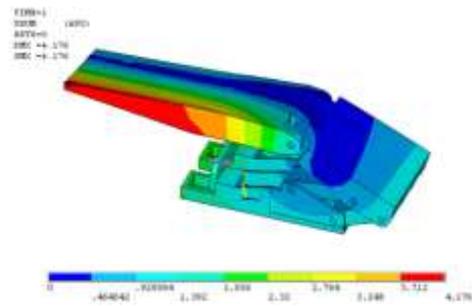


Fig.26 The displacement of one side loading of the top beam

G. Strength Analysis of Eccentric Loading on Beam

Fig. 24 shows the location of bearer in case of eccentric loading on beam. Free gridding of support led to 75135 units and 107464 nodes, as shown in Fig. 25. By applying loads along the axial direction of the column, cloud charts of displacements (Fig. 26) and stresses (Fig. 27) of the support in case of eccentric loading on beam were obtained by analysis using the ANSYS software. As observed, the maximum displacement and stress of the support in case of eccentric loading on beam were 4.176 mm and 672.886 MPa, respectively. Hence, eccentric loading on beam is one of the working conditions involving largest external loads and most severe stress concentrations.

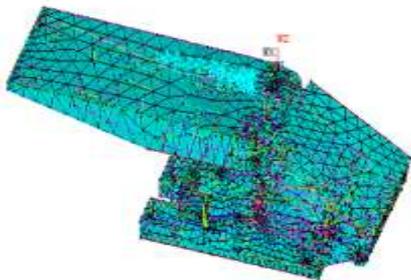


Fig.24 The stepping-block position of one side of the top beam

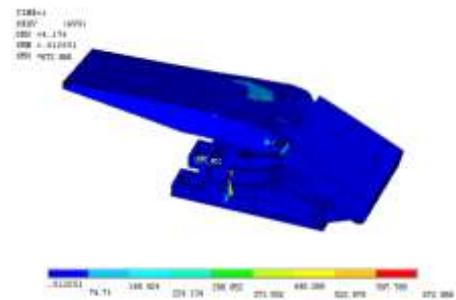


Fig.27 The stress of one side loading of the top beam

IV. MOTION SIMULATION OF HYDRAULIC SUPPORT

A. Establishment of Motion Model of Hydraulic Support

The motion model of hydraulic support was established (see Fig. 28) by 3D assembly modeling of its components involving motion pair and driver.

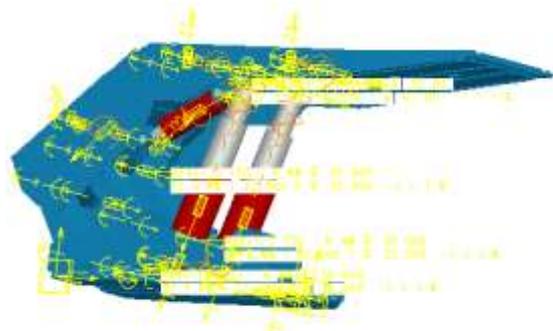


Fig.28 The movement assemble model of hydraulic support

B. Motion Simulation of Hydraulic Support

Once entering the Mechanism module, drivers are established and their motion orders are adjusted so that different parts have individual drivers to achieve motion of the entire system. Fig. 29 shows the motion simulation process of elevation of hydraulic support head beam and it allows intuitive understanding of dynamic characteristics of the system. The results indicated good rationality of hydraulic support structures and absence of motion interferences.

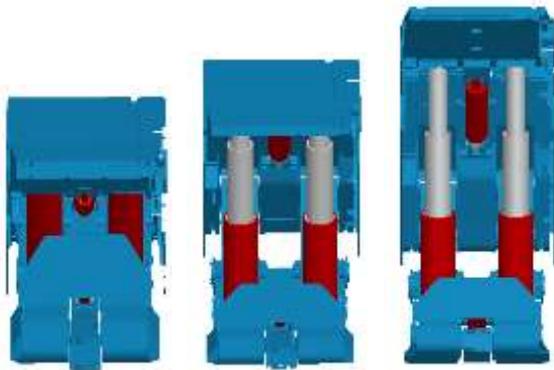


Fig.29 The risen process of hydraulic support

The elevating structure of the proposed hydraulic support is a four-link structure consisting of shield beam, pre and post connecting rods, and base. For the design of the four-link structure, the variation of end face distance shall be minimized during the elevation of supports within the working range so that the head beam can protect the roof. Fig. 30 shows end point displacements of hydraulic support head beam obtained by motion simulations. Fig. 31 shows end point displacements of head beam vs. time. As observed, the maximum horizontal displacement of end point of support head beam was 94 mm (2358-2264 mm), which was below 100 mm (the maximum horizontal displacement allowed), indicating good rationality of the four-link structure of hydraulic support in terms of size and other design requirements.



Fig.30 The double twist curve of the top beam's end

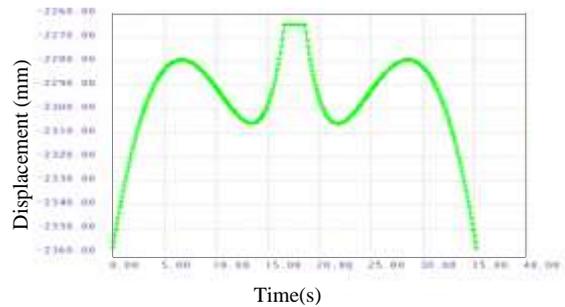


Fig.31 The displacement-time curve of the top beam's

V. CONCLUSIONS

To overcome limitations of current designs of hydraulic supports, a 3D numerical model was established for hydraulic supports by introducing virtual prototyping and static simulation and motion simulations of harsh environments in which hydraulic supports works were involved. The following conclusions can be drawn:

The locations of peril points and stress distribution in hydraulic supports were obtained and used for optimization of hydraulic support design.

Systematic motion simulations of hydraulic supports were involved and the results indicated absence of motion interferences and rationality of the four-link design of hydraulic supports.

The proposed virtual prototyping based hydraulic support is viable. Indeed, virtual prototyping can improve the design method and reduce the design period. This study provides references for industrial applications.

ACKNOWLEDGMENT

In this paper, the research was sponsored by the Natural Science Foundation of Shandong province, China (No. ZR2016EEM37), Key national research and development programs, China(No.2018YFC0604702)and key research and development project of Shangdong province, China (No. 2017GSF216004).

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