

VI. ANALYSIS OF THE TOTAL FEED OF WHEEL

The total feed f_a can be found from the formula when spring grinding:

$$f_a = a_p + f_a' \quad (9)$$

Where a_p is grinding feed; f_a' is compensated feed which aims at overcome spring elastic potential energy.

Because spring has certain elasticity, wheel must produce enough positive pressure which applied on spring, by this way, abrasive grains with certain linear speed can cut spring metal matrix. Obviously, grinding feed a_p is based on compensated feed f_a' . When spring is grinded with critical grinding thickness a_{\min} of abrasive grains, the positive pressure between wheel and spring is defined as critical positive pressure. The critical grinding thickness a_{\min} of abrasive grains can refer to table 1. [6]

TABLE.1. CRITICAL GRINDING THICKNESS a_{\min}

Material	r_g	a_{\min}	$k_s = a_{\min}/r_g$
Hardened carbon steel	6	1.5	0.25
Cast-iron	6	3	0.5
Annealing carbon steel	6	4	0.67

Where r_g is the radius of micro blade of abrasive grains; k_s is a parameter which can characterize the cutting ability of material.

Grinding demand decides on selection of r_g , different granularity can corresponding to different harshness. In general, we use alumina grains for wheel when spring end grinding, and the keenness of alumina grains can be shown by r_g and tip angle of abrasive grains α , as follow in table 2

TABLE.2. THE KEENNESS OF ALUMINA GRAINS

Granularity	46#	60#	80#	W40	W28
$r_g/\mu\text{m}$	28	18	13	4	2.7
$\alpha/(\circ)$	110	108	106	98	90

When springs are grinded with critical grinding thickness of abrasive grains, the formula of grinding force:

$$\begin{aligned} F_a' &= 9.81a_{\min} \{C_F \cdot [b(\frac{l}{a} - 1)\sqrt{2al - l^2} \\ &+ ab \arcsin \frac{l-a}{a} + \frac{1}{2}\pi ab] \cdot N / v_2\} \tan \beta \\ &= 9.81r_g \cdot k_s \{C_F \cdot [b(\frac{l}{a} - 1)\sqrt{2al - l^2} \\ &+ ab \arcsin \frac{l-a}{a} + \frac{1}{2}\pi ab] \cdot N / v_2\} \tan \beta \end{aligned} \quad (10)$$

Positive pressure from pressure spring should meet the formula:

$$\begin{aligned} F_N &= K \cdot f_a' = F_a' / N \\ f_a' &= F_a' / (K \cdot N) \end{aligned} \quad (11)$$

Where F_N is elasticity of single spring; K is spring stiffness; N is the number of spring.

The relationship between total feed and grinding can be found from Eqs.(7)、Esq.(9) and Eqs.(11), it plays an important guiding significance in spring end grinding and can vastly improve the grinding efficiency and grinding quality.

VII. CONCLUSIONS

1. The process of spring end grinding is analyzed and the feasibility of controlled-force grinding using for spring end grinding is proved. The grinding force formula by analyzing geometric model of spring grinding is introduced to ensure the power of grinding head motor. These theories are of great help in designing spring grinder and confirming technology.

2. The process of spring grinding must have a constant grinding force. As the grinding depth increase, grinding area will increase and grinding feed will decrease.

3. Spring is considered as an elastomer and the grinding feed can be divided into two parts: one is grinding feed and other is compensated feed. The former is built on the latter, so we must consider both feed in spring end grinding.

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