Unsupervised Extrinsic Parameters Calibration for Multi-beam LIDARs

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Abstract—In this paper we present a technique of unsupervised extrinsic parameters calibration for a multi-beam LIDAR scanner. The proposed method decomposes extrinsic parameter calibration procedure into two parts: computing rotation matrix caused by pitch angle and roll angle through ground plane estimation; computing rotation matrix caused by navigation angle through matching pole-like obstacles in a series of poses. Experiment results demonstrate the efficacy of the calibration technique.

Keywords-component; unsupervised; calibration; extrinsic; decompose; multi-beam lidar;

I. INTRODUCTION

Light Detection and Ranging (LIDAR) sensors are important parts of robot systems. Traditional LIDAR sensors are equipped with only one rotating beam. However, with the progress of science and technology, applying multi-beam LIDAR sensors which are often referred as 3D LIDAR sensors configured with many simultaneous rotating beams at varying angles become a trend in robot navigation. One of these systems is the Velodyne HDL-64E S2(Fig. 1): it consists of 64 lasers located on a spinning head. Since 2007 DARPA urban challenge[1][2][3], Velodyne HDL-64E S2 has been widely applied in SLAM, 3D perception and other area of robotics.

Many work has been done in multi-beam LIDAR and camera calibration. In [4], author present mutual information (MI) based algorithm for automatic extrinsic calibration of a 3D laser scanner and optical camera system. [5] provides an approach for external calibration of a 3D laser scanner with an omni-directional camera system. [6] proposes a method to estimating the intrinsic parameters of a 3D LIDAR while at the same time computing its extrinsic calibration with respect to a rigidly connected camera. Some other work focuses on intrinsic parameters of multi-beam LIDAR, e.g. [7][8] use pattern planes to calibrate intrinsic parameters. [9] mentions both intrinsic parameters calibration and extrinsic parameters calibration.

As Fig 1 and Fig 2 present, a HDL64E S2 LIDAR has 64 laser emitters along the vertical direction. The angle interval between adjacent emitters is about 0.4 degree. The resolution of azimuth angle is 0.09 degree which is much higher than elevation angle's resolution. Due to the geometrical model of LIDAR system, data is sparse in vertical direction, especially

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at long distances. This effect makes 3D features unstable at the distance of 15m or more. However, 2D features in planes which parallel to horizon plane are more stable, such as polelike features, e.g. tree trunks, lampposts of streetlights.



Figure 1. geomertrical model of HDL64ES2 LIDAR: left figure is sideview of the LIDAR; right figure is top view of the LIDAR



Figure 2. data assembled by HDL64ES2: different color represents different laser beam

Given that the LIDAR is often mounted on a vehicle platform which also has an IMU and GPS system, we propose a two step unsupervised calibration method: computing rotation matrix caused by pitch angle and roll angle through estimating ground plane; computing rotation matrix caused by navigation angle through matching polelike obstacles in a series of the vehicle poses gotten from the IMU and GPS system.

The paper is organized as follows: section II describes system architecture of our vehicle platform; section III

introduces data preprocessing; section IV presents the calibration procedure; section VI provides the experiment results.

II. SYSTEM ARCHITECTURE

Our vehicle is shown in Fig 3. The Velodyne HDL-64E S2 LIDAR sensor is mounted on the top of the vehicle. The vehicle pose estimation system is comprised of IMU, GPS and a wheel encoder. It reliably provide ego-motion data.

The vehicle frame and the LIDAR frame are shown in Fig.4. We define yaw angle γ rotates around Z-axis, roll angle β rotates around Y-axis, pitch angle α rotates around X-axis.



Figure 4. Vehicle frame and LIDAR frame

III. DATA PREPROCESSING

The original sensor readings are in spherical coordinates, while we use 3D points in Cartesian coordinates. So the sensor readings are transformed into Cartesian coordinates first according to LIDAR geometrical model.

Denoting the *i* th laser beam's elevation angle with θ_i , rotation angle in time *t* is ϕ_t , the measurement is r_t , the computation of 3D points is as (1):

$$\begin{pmatrix} x_t \\ y_t \\ z_t \end{pmatrix} = r_t \begin{pmatrix} \cos(\theta_t)\cos(\phi_t) \\ \cos(\theta_t)\sin(\phi_t) \\ \sin(\theta) \end{pmatrix}$$
(1)

Due to the motion of the vehicle and the fact that the scanner takes a non-negligible amount of time(60ms~150ms) to complete one rotation, the point clouds will be distorted by vehicle motion. We use vehicle pose data to rectify the point clouds.

The vehicle pose information can be received at the instant of every frame ending. The pose information in one frame at time t is computed by linear interpolating the poses difference between the current frame and the last frame. Denoting LIDAR working at f Hz, the pitch angle difference of the concessive two frames is α . The pitch angle at time t is approximated by linear interpolation as $a(t) = f \cdot t \cdot a$, the other angles and translations components can be computed analogously.

From these angles and translations, we can derive the rotation matrix and translation at time t.

$$\left(\frac{x_t}{y_t}\right) = R_t \begin{pmatrix} x_t \\ y_y \\ z_t \end{pmatrix} + T_t$$
(2)

IV. APPROACH

According to Euler-angles' definition, LIDAR frame to vehicle frame rotation matrix R and translation T can be decomposed into two parts as (3) shown:

rotation R_1 caused by pitch angle α , roll angle β and translation T_1 caused by z component;

rotation R_2 caused by yaw angle γ and translation T_2 caused by x and y component.

$$R = R_1 R_2, T = T_1 + T_2 \tag{3}$$

A. Ground extracting and R_1 , T_1 Computation

The vehicle is driven on a flat urban road. Ground plane is extracted by fit 3D points in region of interest through RANSAC.

The ground plane in LIDAR frame can be represented as (4):

$$Ax + By - z + c = 0 \tag{4}$$

Assuming yaw angle, x component and y component in translation are all zero. Sensor to vehicle's pitch angle, rotation angle and translation in z axis are computed as fig 5.



Figure 5. Tait-Bryan angles Z-Y-X

$$R_{1} = \begin{bmatrix} \cos\psi & \sin\psi & 0\\ -\sin\psi & \cos\psi & 0\\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0\\ 0 & \cos\theta & \sin\theta\\ 0 & -\sin\theta & \cos\theta \end{bmatrix} \begin{bmatrix} \cos\phi & \sin\phi & 0\\ -\sin\phi & \cos\phi & 0\\ 0 & 0 & 1 \end{bmatrix}$$
(5)

$$T_1 = \begin{bmatrix} 0\\0\\C \end{bmatrix}$$
(6)

B. Pole-like Obstacle labeling and R_2 , T_2 Computation

Similar to [10], we slice point clouds to get arc features and use arc curvature centers as labeled points for calibration.

Two group of points $P_{i,t}$, $P_{i,t+1}$ are labeled features in two consecutive data frame f_t , f_{t+1} , so $P_{i,t}$ and $P_{i,t+1}$ can be matched as :

$$R_{l,i,t}P_{i,t} + T_{l,i,t} = P_{i,t+1}$$
(7)

At time t+1, we can derive vehicle local pose difference $R_{s,t}$ and $T_{s,t}$ to its pose at time t. For LIDAR is rigidly connected to vehicle, rotation in LIDAR frame equals to rotation $R_{s,t}$, so $R_{l,i,t} = R_{s,t}$. Translation $T_{l,t}$ of LIDAR frame at time t is approximate by the average translation of all the match points at the time..

$$T_{l,t} = \frac{1}{n} \sum_{i=1}^{n} (P_{i,t+1} - R_{s,t} P_{i,t})$$
(8)

The relation of $T_{l,t}, T_{s,t}$ can be used to compute rotation and translation between the two system.

$$R_{p}T_{l,t} + T_{p} = R_{s,t}T + T_{s,t}$$
(9)

We compute R_p , T_p by solving least square formula (10)

$$E = \sum_{t=1}^{T} \left(R_p T_{l,t} + T_p - R_{s,t} T_p - T_{s,t} \right)^2$$
(10)

For the coefficients are linear in (10), it has the solution similar to (11), then it's easy to get R_2, T_2 :

$$X = (A^T A)^{-1} A^T B \tag{11}$$

$$R_2 = \begin{bmatrix} R_p & 0\\ 0 & 1 \end{bmatrix} T_2 = \begin{bmatrix} T_p\\ 0 \end{bmatrix}$$
(12)

V. EXPERIMENT AND RESULTS

The calibration algorithm is tested by our vehicle platform in real environment .

A. Ground Extraction and Pose estimation

The region of interest for ground estimation is set as: [-500cm, 800cm] in x-axis, [-2000cm, 3500cm] in y-axis, shows in fig.6;



Figure 6. Ground Plane Extraction: red area is the region of interest for RANSAC

The result of RANSAC ground plane is: -0.0004x + 0.0041y - z - 227.3088 = 0

 R_1, T_1 are computed by (5) (6).

B. Pole-like Feature Extraction and Pose Estimation

The vehicle is driven along the curved road at speed of 10km/h, the track is shown in fig.7.



Figure 7. Vehicle's Track

Every five frame, system extracts pole-like feature(see fig.8) and record vehicle pose from pose estimation system, Then use(8) – (12) to compute R_2 , T_2 .



Figure 8. Pole-like Feature Extraction

C. Performance Evaluation

We use supervised calibration which takes a lot of hand measurements as ground truth. After our unsupervised calibration, the error distances are dropping significantly. In fig.9, after calibration ground plane in LIDAR frame is very close to the ground in vehicle frame , most of error distances under 5 cm; in fig.10 calibration also reduces 3D points' error distance between LIDAR frame and vehicle frame.



Figure 9. Error distance to ground plane comparison



Figure 10. Error distance to 3D points comparison

VI. CONCLUSION

Multi-beam LIDAR's importance is increasing in the field of robotics. The powerful ability of 3D perception makes it irreplaceable in 3D-SLAM. It's sure that there are

still many of application can be developed in the huge amount of data provided by multi-beam LIDAR. For any sensor, calibration is one of the most important procedures before it generates valid data. The paper has presented an unsupervised method which shows how to simply and efficiently do calibration. We now aim to work on the calibration of LIDAR intrinsic parameters, possibly simultaneous calibration of LIDAR intrinsic parameters and extrinsic parameters.

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